

STRUCTURE GEOTECHNICAL REPORT

Proposed Structure No. 058-0137

Existing SN: 058-0029

IL Route 148 over Mosquito Creek
FAP Route 714 (IL 148)
Section (128BR-1) B-1
Macon County
Sta. 382+15.80

P-97-019-09
Contract No. 74368

May 12, 2020 (revised)
February 7, 2020

Prepared By: Scott A. Kassel, P.E.
IDOT Region 4 District 7
Geotechnical Unit
scott.kassel@illinois.gov
(217) 342-8233

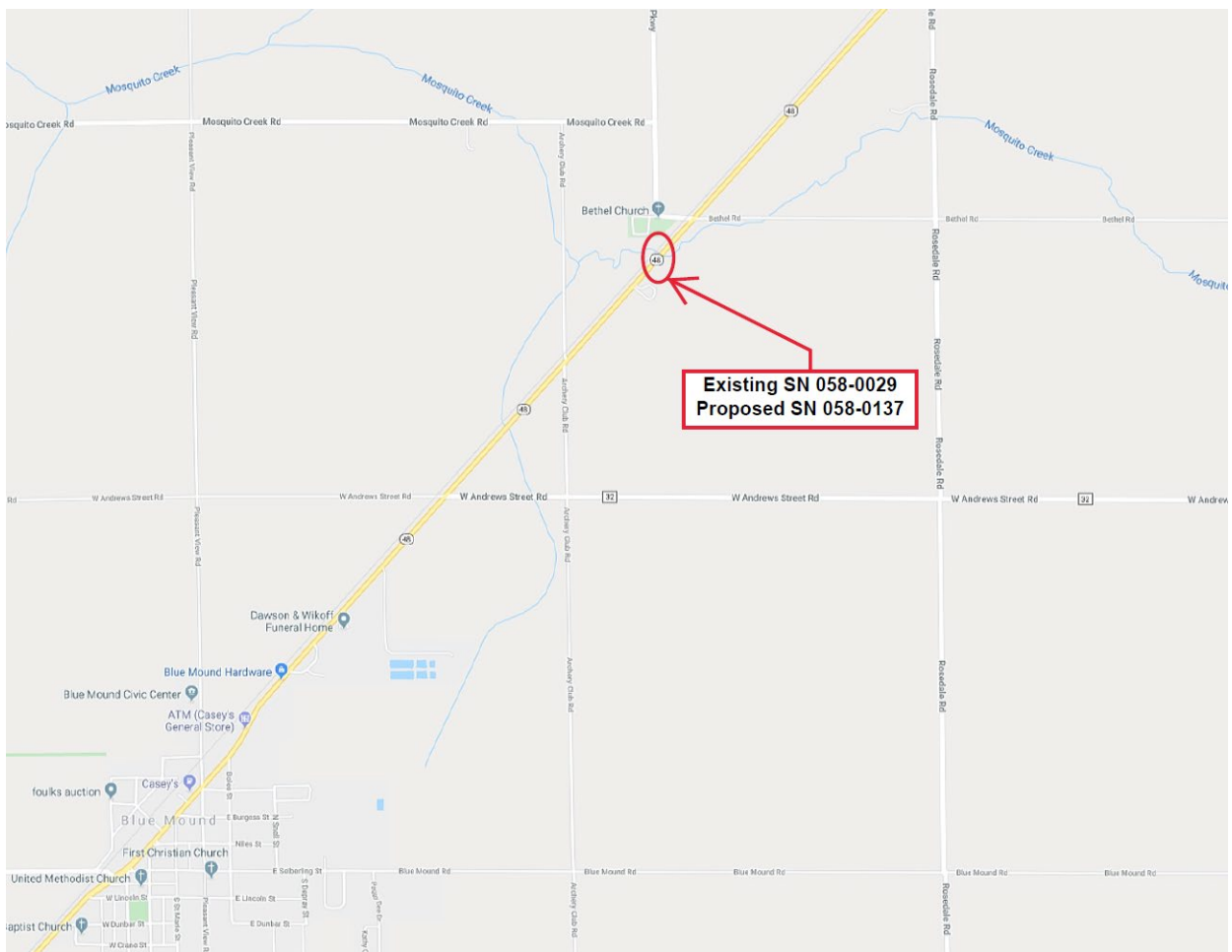
Approved by: Bradly Hessing, P.E.
Bureau of Bridges & Structures
Foundation & Geotechnical Unit
bradly.hessing@illinois.gov
(217) 782-7773

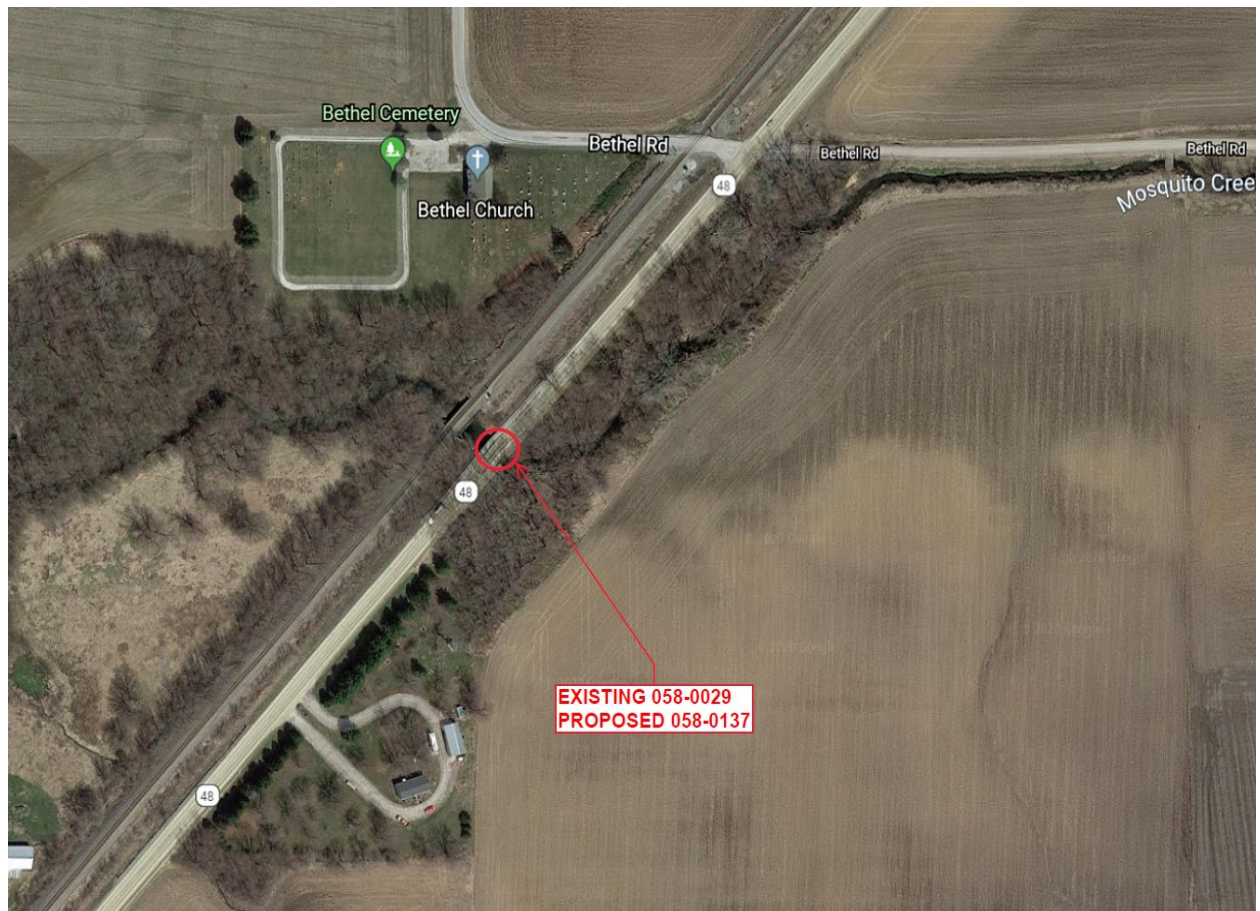
Prepared For: Illinois Department of Transportation
Bureau of Bridges and Structures
Bridge Planning Unit and
Bridge Design Section

Attachments: Boring Logs
Subsurface Data Profile Plot
Slope Stability Analysis
Approved TSL
IDOT Static Method of
Estimating Pile Lengths

1. Project Description and Scope

This project consists of complete replacement of existing structure 058-0029 with proposed structure 058-0137. The existing structure consists of a single span, deck beam bridge. It measures 52 ft 9- $\frac{1}{8}$ in total length (back to back abutments) and a clear width of 35 ft-4 in (out to out deck) and is set at a zero-degree skew. The proposed structure will consist of a single span concrete deck on steel beams supported on integral abutments and will also be set at a zero-degree skew. The planned length is 84 ft-8 in (back to back abutments) and planned width of 42 ft-10 in (out to out deck). According to the BCR, replacement has been recommended due to the excessive leaking at the keyways and 30 plus years of deck beam service. The location of the existing and proposed structure is at IL 48 over Mosquito Creek in Macon County. Specifically, this is in the Northwest $\frac{1}{4}$ of the Southeast $\frac{1}{4}$, Section 28, Township 15N, Range 1E. The maps below show the location of the structure to be approximately 1 $\frac{1}{2}$ miles Northeast of Blue Mound.





2. Subsurface Conditions

Generalized subsurface conditions, based on borings B-1 and B-2, mainly consist of a mixture of Clay and Silty Clay overlaying a Sandy Loam and Sandy Clay Loam (Till). The hard glacial (Till) unconfined compressive strengths (Q_u) range from 3.93 – 11.52 tsf with SPT (N Value) ranging from 21 to 100 blows per 12" of penetration. Boring B-1 was advanced to auger refusal at elevation 565.77 feet.

Groundwater was first encountered at elevations of 581.8 feet in boring B-1 and 579.8 feet in boring B-2 at the time of field exploration. Upon completion of drilling, the groundwater was measured at an elevation 589.3 feet in both borings. When checked 24 hours after drilling, groundwater in both borings was measured at an elevation of 592.3 feet. These observations represent groundwater conditions at the time of the field exploration, and may not be indicative of other times, or at other locations. Groundwater levels can be expected to fluctuate with varying seasonal and weather conditions.

3. Settlement

Approximately 1½ feet of fill will be placed at the north and south abutments. The soil profile is composed of medium to hard, cohesive soils. It is estimated that less than 1-in of settlement should occur in the cohesive portion of the existing soils. Most of this settlement, if any, will likely occur in the top 5 feet below the ground surface. Remedial methods used to accelerate or limit settlement should not be necessary.

4. Slope Stability

Due to lengthening of the structure, soil will be excavated to a distance approximately 42' behind the existing north and south abutments, to the proposed north and south abutment locations. A 1:2 (V:H) cut slope will be constructed in front of the proposed north and south abutments. The estimated slope stability factor of safety for the new slopes at the abutments is 5.9, which exceeds the minimum requirement of 1.7 for cut slopes. Therefore, there is no stability concern at either slope wall and remedial measures are not necessary.

5. Scour

Based on pictures and descriptions in the BCR, there is no scour concern at the existing abutments. Pictures in the BCR do not indicate that any of the substructure footings have been undermined by scour. There is no documented history of scour or erosion occurring at the existing substructure. The proposed bridge opening will be

widened, and the abutments will be protected by a 1:2 (V:H) riprap slope. Based upon the new substructure configuration, the Q100, the Q200, Design and the Check Scour Elevations for both abutments are to be set at the bottom of abutment elevation.

Event/Limit State	Design Scour Elevations (ft.)		
	North Abutment	South Abutment	Item 113
Q100	600.68	600.68	8
Q200	600.68	600.68	
Design	600.68	600.68	
Check	600.68	600.68	

6. Seismic Considerations

Based on the proposed structure location and boring data, we recommend that the seismic data to be shown on the TSL as follows:

Seismic Performance Zone (SPZ) = 2
Design Spectral Acceleration at 1.0 sec. (SD1) = 0.114
Design Spectral Acceleration at 0.2 sec. (SDS) = 0.227
Soil Site Class = C

There is a granular layer shown in boring B-1 at approximate elevation 581 feet, which is submerged by the water table. Liquefaction is not probable due to the location of this sand layer, its relation to the water table, and due to the stiff cohesive soils in the

profile. The design of this structure will not likely be impacted by seismic considerations.

7. Foundation Recommendations

Preliminary maximum factored loads, provided by the structure designer, are estimated to be approximately 1277 kips vertical at the abutments. The draft TS&L proposes an integral abutment substructure system for this structure. Driven piling is the preferred foundation for integral abutments, therefore drilled shafts and spread footings were not evaluated as alternatives to driven pile foundations.

Piles: Based on the “*Integral Abutment Feasibility Analysis*”, it appears that friction H-piles or steel shell piles are feasible. The analysis included steel H-piles, 14” metal shell piles and 16” metal shell piles. H-pile lengths are very difficult to predict when bedrock is not encountered in the boring logs, therefore metal shell piles were the preferred pile type at this location. However, based upon the hard till conditions and our analysis, it would be difficult for metal shell piles to be driven into the hard till material without incurring damage to the pile. Therefore, it is recommended that steel H-piles driven to their maximum nominal bearing be used. Because of the limitations of the drill rig and crew, the borings were only able to be advanced to an auger refusal depth of 41 feet without encountering rock. A review of steel H-pile driving records from structures constructed in the vicinity of this structure indicate that H-piles can be successfully driven into hard till conditions without encountering bedrock. The Pile Design Table (below) lists steel H-Piles, their maximum nominal required bearings, and the corresponding factored resistances. Pile capacities on the pile data sheets were calculated assuming no pre-coring thorough the existing embankment material and the hard till material extended to the maximum depth of the pile. Since settlement at the embankments under the weight of new fill should be minimal, we do not feel that pre-coring is necessary. Lateral loading to the piles should not be a concern in this situation. A structure with pile configurations as shown on the TSL should not require a lateral load pile analysis.

Pile Design Table for Steel H-Piles SN: 058-0137				
Pile Location	Pile Size	Maximum Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Pile Length* (Ft)
North Abutment Boring B-1	HP 12x53	419	230	50
	HP 12x63	497	273	56
	HP 12x74	589	324	67
South Abutment Boring B-2	HP 12x53	419	230	48
	HP 12x63	497	273	54
	HP 12x74	589	324	62

*Estimated pile length is based on assuming the pile embedment depth: 2.0 ft., bottom of abutment elevation: 600.68 ft, and ground elevation at beginning of pile driving: 600.68 ft.
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One test pile should be driven at the North Abutment to verify the estimated lengths determined in design.

8. Construction Considerations:

Stage Construction: The new structure will be built under staged construction. Based on the design charts, “Temporary Sheet Piling” appears only to be feasible at the North Abutment. A Temporary Soil Retention System will be required to be used on the South Abutment.

EWSE/Cofferdams: The estimated water surface elevation (EWSE) is approximately 593 feet. The bottom of abutment elevation is 601 feet. Therefore, there is no need for cofferdams.

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Date 8/30/18

9" Asphalt Pavement.	606.02				Medium, moist, grey, SILTY CLAY LOAM. <i>(continued)</i>	1 1	0.6 B	25
9" Concrete Pavement.	605.27							
Moist, dark grey, CLAY with Silt.					584.77			
					Medium, moist, grey, SANDY LOAM with Silt.	0 1 1		22
					<i>Soft, wet.</i>			
<i>Stiff, with organics.</i>	-5	3			▼-25	1		
		3 4	1.3 B	31	580.87	4 8	0.3 B	21
					Grey, GRAVELLY SAND.			
		3			579.77			
		3 4	1.2 B	29	Very stiff, moist, grey, SANDY CLAY LOAM.	10 10 11		
					SANDY LOAM with gravel		2.9 B	9
					SANDY CLAY LOAM TILL			
597.27	-10	2				20		
Medium, moist, dark grey, SILTY CLAY.		2 3	1.0 B	28	Hard, moist, grey.	31 50	6.9 S	8
						5-3/4"		
		1			<i>Very dense, augers locked in place.</i>			
593.67		2 3	2.1 B	28				
592.27	-15	1				42		
Medium, moist, dark grey, SILTY CLAY.		2 2	0.7 B	28		50 5-1/4"	6.9 S	6
						50 4-1/2"		
589.77								
Medium, moist, grey, SILTY CLAY LOAM.	▽	1 2 2		25				
			0.9 B					
	-20	0				50		

SOIL BORING 058-0029 SOIL 2018.GPJ IL DOT.GDT 2/6/20

BBS. form 137 (Rev. 8-99)

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Date 8/30/18

This image shows a completely blank white rectangular area enclosed within a thin black frame. There are no markings, text, or illustrations present.

BBS, form 137 (Rev. 8-99)

SOIL BORING 058-0029 SOIL 2018.GPJ IL_DOT.GDT 2/6/20

Page 1 of 2

Date 8/30/18

	1 1	1.2 B	28
8	0		
	1 1	0.3 B	22
-25	5		
	8 14	0.2 S	15
▼	12		
	10 13	3.9 S	8
-30	29		
	50 5-15/16" 50 4-1/8"	11.5 S	7
-35	40		
	50 5-5/8" 50 4-3/8"	5.7 S	6
-40	50		

BBS, form 137 (Rev. 8-99)

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Date 8/30/18

Groundwater Elev.:		
First Encounter	<u>579.8</u>	ft ▼
Upon Completion	<u>589.3</u>	ft ▼
After 24 Hrs.	<u>592.3</u>	ft ▼

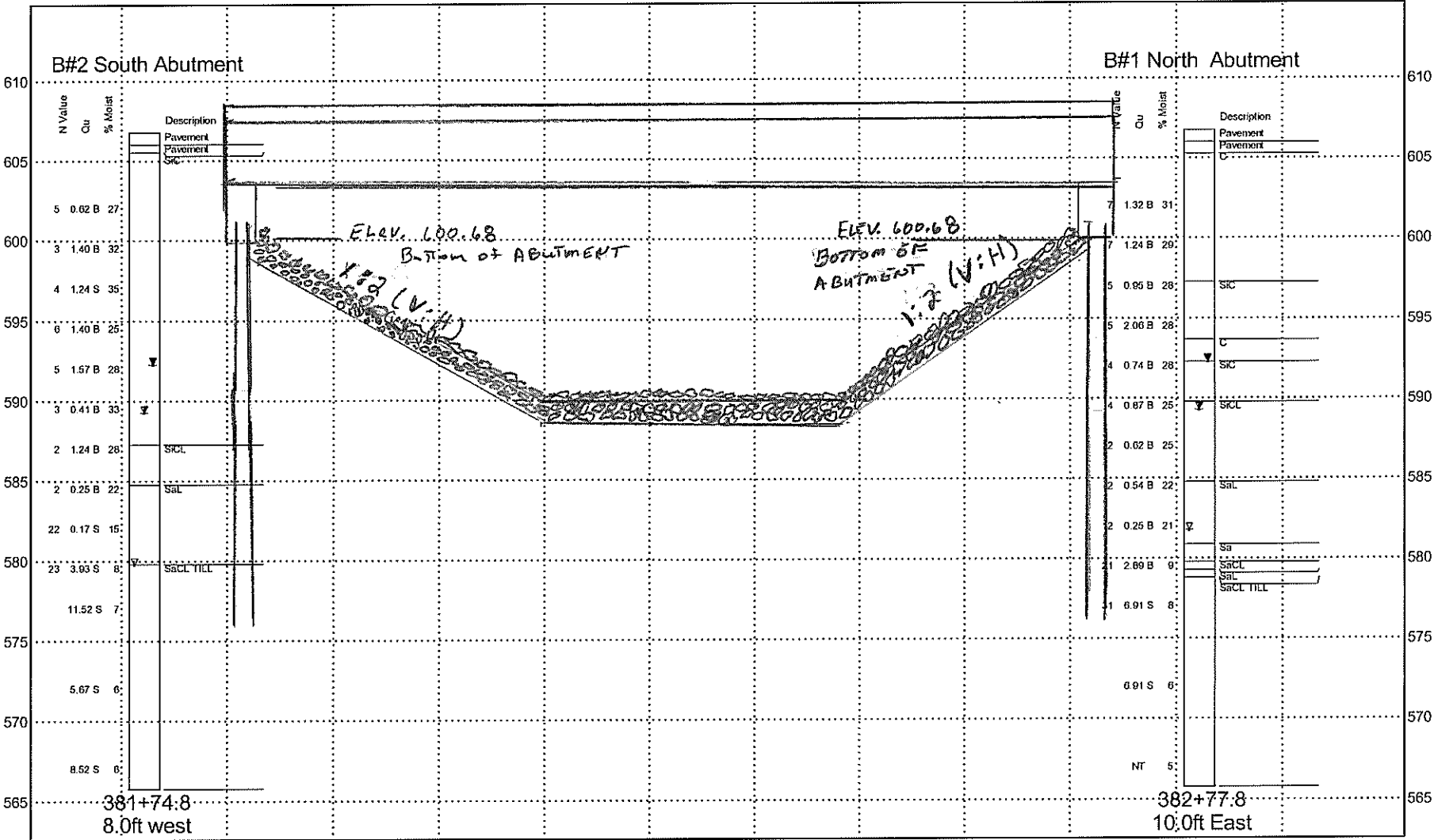
565.78	4-1/2" 50	8.5 S	6	
Extent of exploration.	4-1/4" 50			
Benchmark: BM 100 brass disk in NE Headwall of Str. No. 058-0029, Sta. 382+46, 18.6' RT. End of Boring	3-1/2"			
-45				
-50				
-55				
-60				

SOIL BORING 058-0029 SOIL 2018.GPJ IL_DOT.GDT 2/6/20

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

Structure Number 058-0029 (E) 058-0137 (P) Abutments
Located in the Mosquito Creek of Section 14, Township 15N, Range 1E of the 3 P.M.



NOT TO HORIZONTAL SCALE

VARIATIONS IN SUBSURFACE
CONDITIONS MAY EXIST
BETWEEN BORINGS

Groundwater
First Encounter
Completion
after (refer to log) hours

Abbreviations
WOH - Sampler Advanced by Weight
of Hammer, WOP - Weight of Pipe
B.S. - Before Sealing

SUBSURFACE DATA PROFILE

Route: FAP 714
Section: (12BR-1)B-1
County: Macon



**Illinois Department
of Transportation**
Division of Highways
IDOT

Slide Analysis Information

Abutment

Project Summary

File Name: Abutment.slmd
 Last saved with Slide version: 8.013
 Project Title: SN 058-0137 Mosquito Creek
 Analysis: Slope Stability for Abutments
 Author: Scott Kassel, P.E.
 Company: IDOT District 7
 Date Created: February 6, 2020

Analysis Options

Slices Type: Vertical

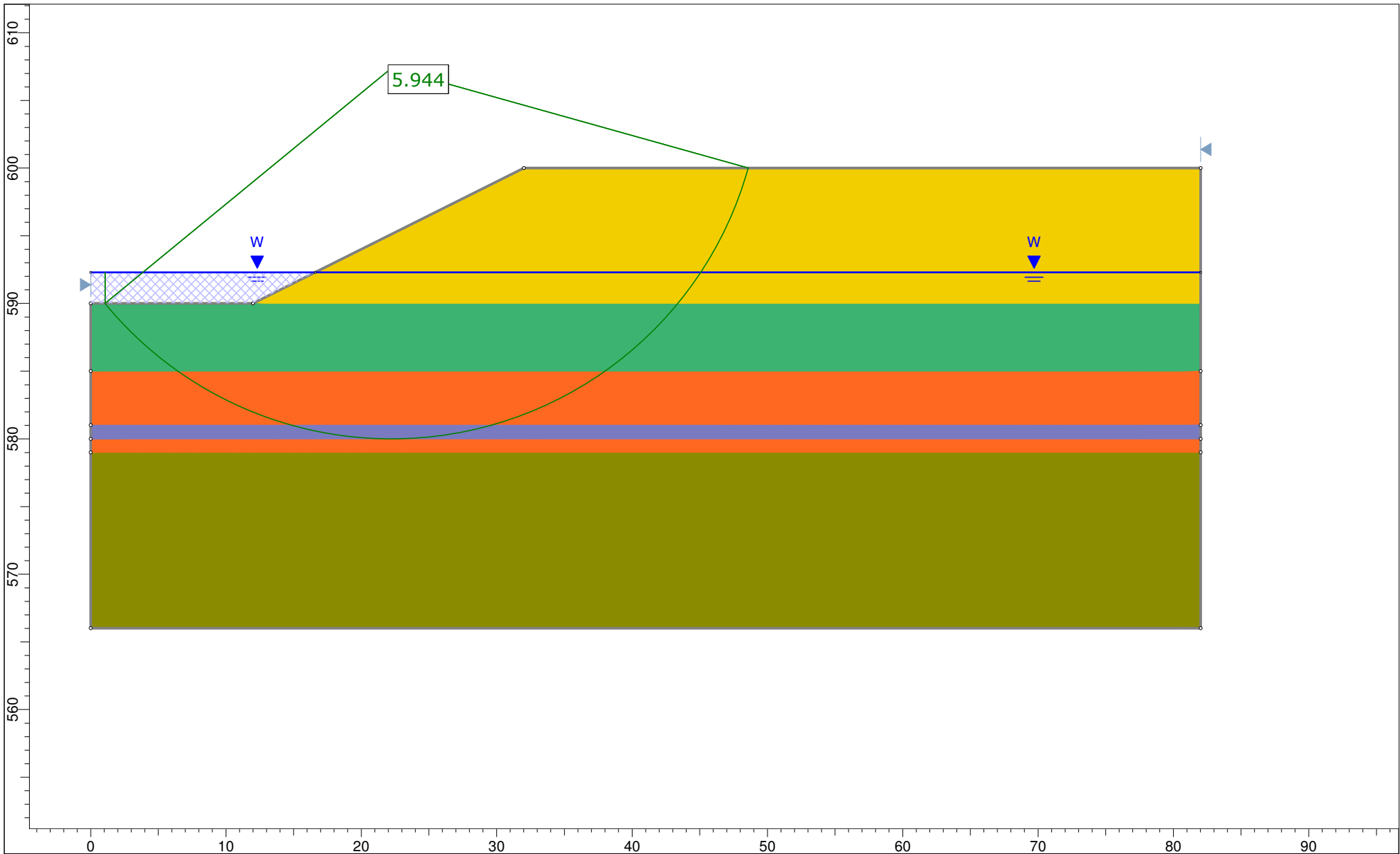
Analysis Methods Used

Bishop simplified
 Janbu simplified

Number of slices: 50
 Tolerance: 0.005
 Maximum number of iterations: 75
 Check malpha < 0.2: Yes
 Create Interslice boundaries at intersections with water tables and piezos: Yes
 Initial trial value of FS: 1
 Steffensen Iteration: Yes

Materials

Property	Embankment	Silty Clay Loam	Sandy Loam	Gravelly Sand	Till
Color					
Strength Type	Mohr-Coulomb	Mohr-Coulomb	Mohr-Coulomb	Mohr-Coulomb	Mohr-Coulomb
Unit Weight [lbs/ft3]	125	120	110	120	106
Cohesion [psf]	1800	1500	1000	0	2000
Friction Angle [°]	0	0	0	26	0
Water Surface	Water Table	Water Table	Water Table	Water Table	Water Table
Hu Value	1	1	1	1	1
Unsat. Shear Strength Phi b [°]	0	0	0	0	0
Unsat. Shear Strength Air Entry Value [psf]	0	0	0	0	0



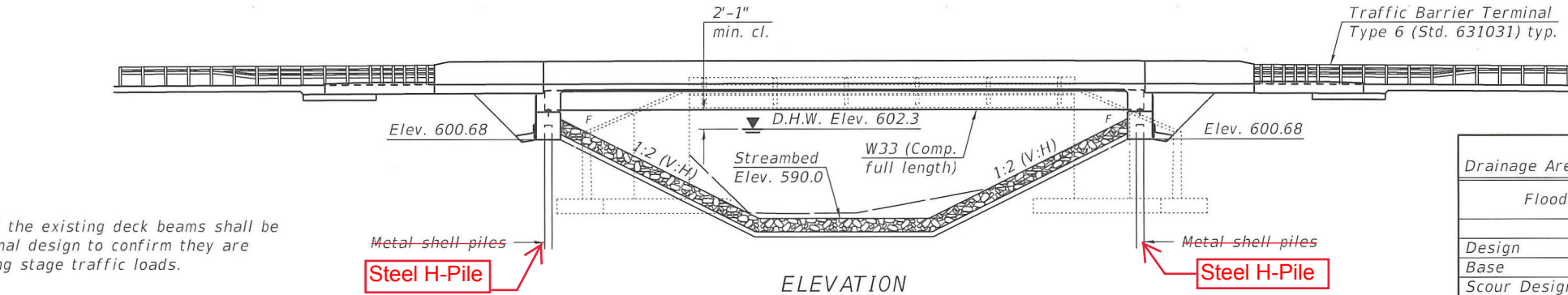
	Project			SN 058-0137 Mosquito Creek	
	Analysis Description			Slope Stability for Abutments	
	Drawn By	Scott Kassel, P.E.	Scale	1:118	Company
	Date	February 6, 2020	File Name	Abutment.slmd	
				IDOT District 7	

Benchmark: Brass disk in NE wingwall of SN 058-0029; Elev. 606.90, Sta. 382+46, Offset 18.6' Rt.

Existing Structure: Structure No. 058-0029 was originally constructed in 1928 as F.A.P. Route 714, Section 128-8. The original structure was a single span, 52'-9½" reinforced concrete deck girder superstructure supported on closed abutments with wingwalls on untreated timber pile foundation. In 1951, the structure was widened from 22 ft. to 36 ft. with new concrete wingwalls as Section 128-B-1; S.B.I. Route 48. In 1983, the concrete deck girder superstructure was removed and replaced with PPC deck beams and a bituminous wearing surface overlying a waterproofing membrane system as Section 128 BR-1. Existing structure will be removed and replaced utilizing stage construction.

No salvage.

Note:
The condition of the existing deck beams shall be verified during final design to confirm they are capable of carrying stage traffic loads.



DESIGN SCOUR ELEVATION TABLE

Event / Limit	Design Scour Elevations (ft.)		
	State	S. Abut.	N. Abut.
Q100		600.68	600.68
Q200		600.68	600.68
Design		600.68	600.68
Check		600.68	600.68

WATERWAY INFORMATION

Drainage Area = 12.4 sq. mi.		Existing Overtopping Elev. = 606.74 at Sta. 381+00							
		Proposed Overtopping Elev. = 606.87 at Sta. 385+50							
Flood	Freq. Yr.	Q C.F.S.	Opening Ft ²		Nat. H.W.E.	Head - Ft.		Headwater El.	
			Exist.	Prop.		Exist.	Prop.	Exist.	Prop.
	10	1720	397	495	600.9	0.3	0.2	601.2	601.1
Design	50	2820	468	594	602.3	0.5	0.3	602.8	602.6
Base	100	3310	497	636	602.9	0.5	0.3	603.4	603.2
Scour Design Check	200	3830	527	682	603.5	0.6	0.3	604.1	603.8
Overtop Existing	N/A	-	-	-	-	-	-	-	-
Overtop Proposed	N/A	-	-	-	-	-	-	-	-
Max. Calc.	500	4540	566	743	604.3	1.2	0.8	605.5	605.1

10 Year velocity through existing structure = 4.3 ft./sec.
10 Year velocity through proposed structure = 3.5 ft./sec.

DESIGN SPECIFICATIONS

2017 AASHTO LRFD Bridge Design Specifications, 8th Edition

DESIGN STRESSES

FIELD UNITS

f'c = 3,500 psi
f'c = 4,000 psi (Superstructure Concrete)
fy = 60,000 psi (Reinforcement)
fy = 50,000 psi (M270 Grade 50)

HIGHWAY CLASSIFICATION

IL Rte. 48 - F.A.P. Rte. 714
Functional Class: Minor Arterial
ADT: 5,200 (2020); 6,200 (2040)
ADTT: 750 (2020); 894 (2040)
DHV: 572 (2020); 682 (2040)
Design Speed: 60 m.p.h.
Posted Speed: 55 m.p.h.
Two-Way Traffic
Directional Distribution: 50:50

LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

SEISMIC DATA

Seismic Performance Zone (SPZ) = 2
Design Spectral Acceleration at 1.0 sec. (SD1) = 0.114
Design Spectral Acceleration at 0.2 sec. (SDS) = 0.227
Soil Site Class = C

GENERAL PLAN & ELEVATION

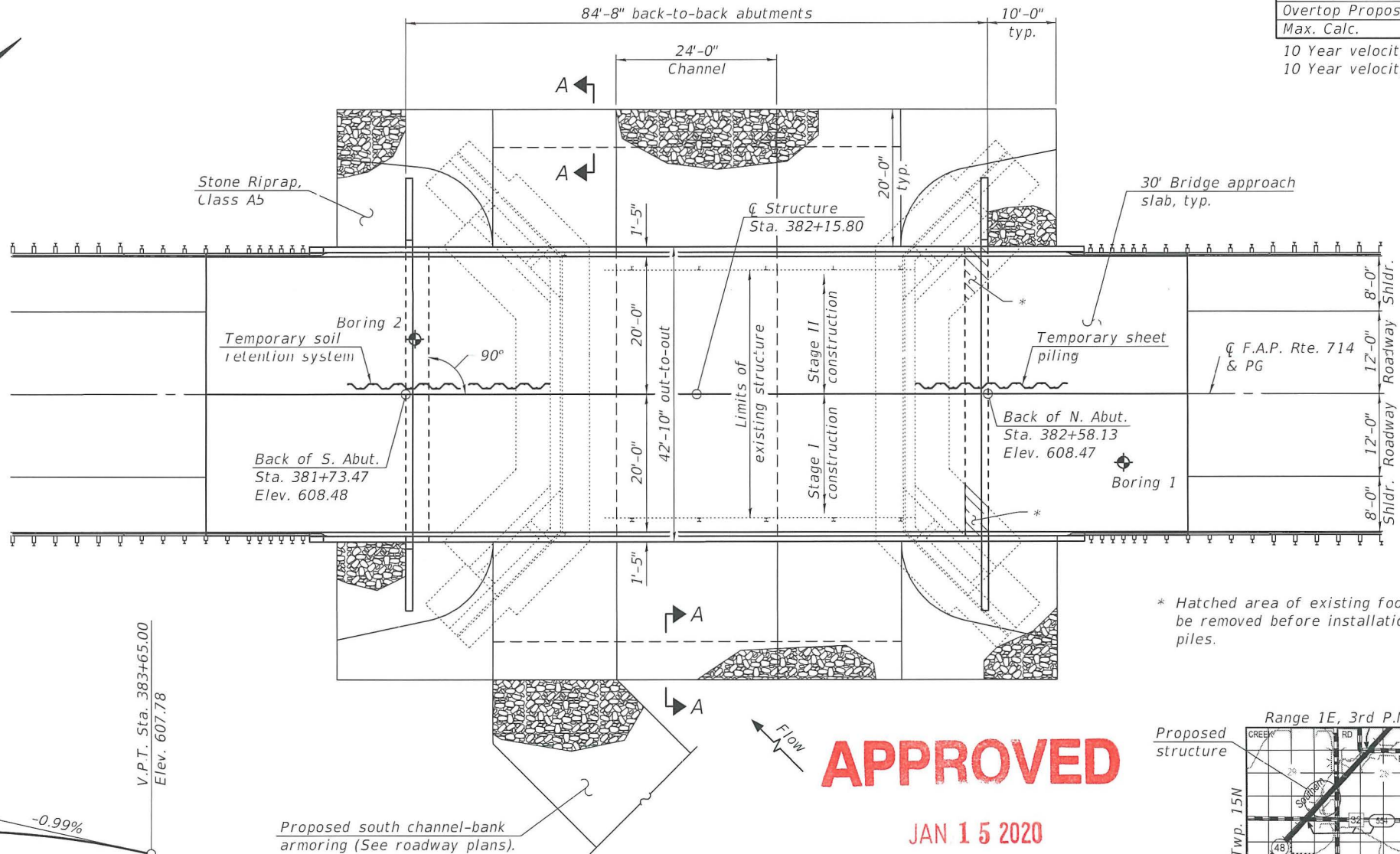
ILLINOIS ROUTE 48 OVER MOSQUITO CREEK

F.A.P. RTE. 714 - SEC. (128BR-1)B-1

MACON COUNTY

STATION 382+15.80

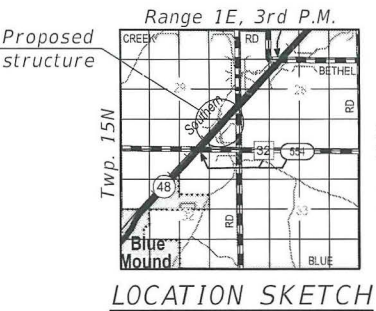
STRUCTURE NO. 058-0137



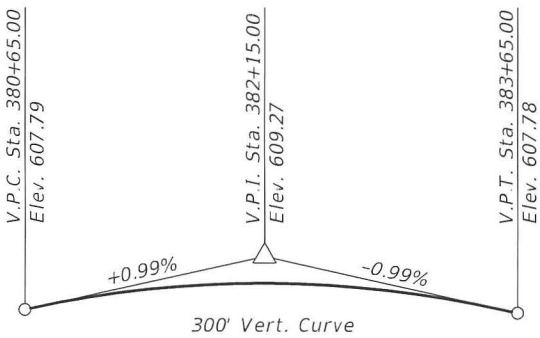
APPROVED

JAN 15 2020

AS A BASIS FOR
PREPARATION OF DETAILED PLANS

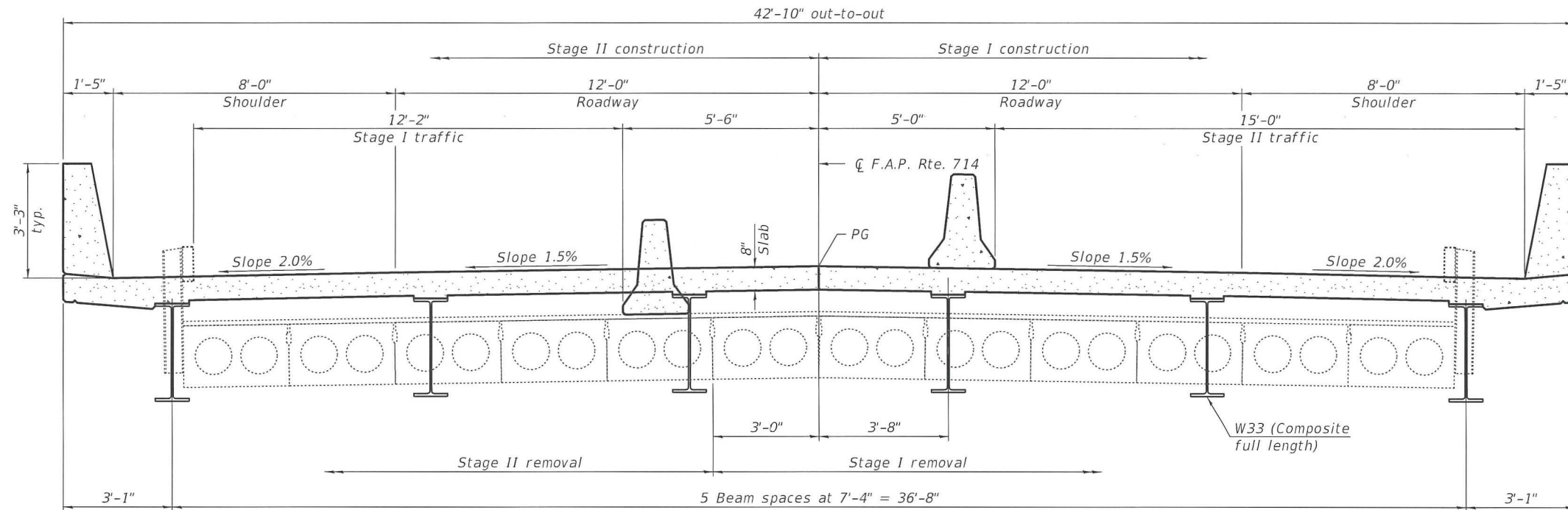


PROFILE GRADE
(Along Q F.A.P. Rte. 714)

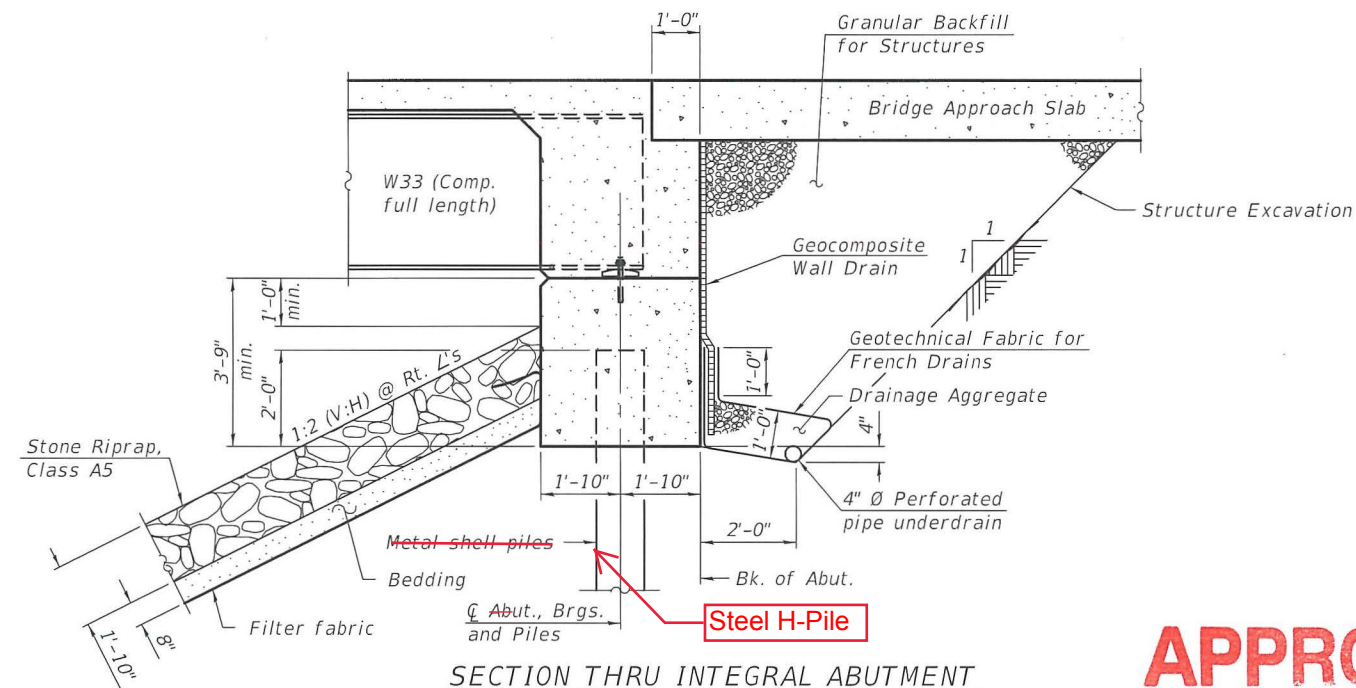


STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

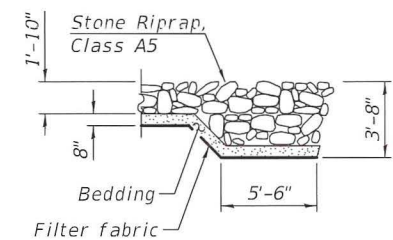
F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
714	(128BR-1)B-1	MACON	—	—
CONTRACT NO. 74368				



CROSS SECTION
(Looking North)



SECTION THRU INTEGRAL ABUTMENT



SECTION A-A

APPROVED

JAN 15 2020

**AS A BASIS FOR
PREPARATION OF DETAILED PLANS**

DETAILS

ILLINOIS ROUTE 48 OVER MOSQUITO CREEK

F.A.P. RTE. 714 - SEC. (128BR-1)B-1

MACON COUNTY

STATION 382+15.80

STRUCTURE NO. 058-0137

**STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION**

SHEET 2 OF 2 SHEETS

F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
714	(128BR-1)B-1	MACON	—	—
CONTRACT NO. 74368				
ILLINOIS FED. AID PROJECT				

DESIGNED -	JUSTIN T. BELUE
CHECKED -	RICHARD J. CHAPUT
DRAWN -	MICHAEL B. MOSSMAN
CHECKED -	J.T.B. / R.J.C.

Pile Design Table for North Abutment utilizing Boring #B-1

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
Metal Shell 12"Φ w/.25" walls			Steel HP 10 X 42			Steel HP 12 X 84		
82	45	21	161	88	31	145	80	26
376	207	23	212	117	36	209	115	31
Metal Shell 14"Φ w/.25" walls			259	142	41	271	149	36
101	55	21	305	168	46	328	180	41
Metal Shell 14"Φ w/.312" walls			Steel HP 10 X 57			385	212	46
101	55	21	114	63	26	442	243	51
497	273	23	167	92	31	499	274	56
Metal Shell 16"Φ w/.312" walls			218	120	36	547	301	61
120	66	21	265	146	41	586	323	66
634	349	23	312	172	46	626	344	71
Metal Shell 16"Φ w/.375" walls			357	197	51	Steel HP 14 X 73		
120	66	21	390	214	56	160	88	26
634	349	23	422	232	61	235	129	31
Steel HP 8 X 36			Steel HP 12 X 53			309	170	36
130	71	31	130	72	26	376	207	41
171	94	36	193	106	31	442	243	46
208	114	41	254	140	36	509	280	51
241	132	46	310	170	41	576	317	56
266	147	51	365	201	46	Steel HP 14 X 89		
			Steel HP 12 X 63			135	74	23
			135	75	26	167	92	26
			199	109	31	243	134	31
			261	143	36	317	174	36
			317	174	41	384	211	41
			374	205	46	452	248	46
			430	237	51	519	286	51
			486	268	56	587	323	56
			Steel HP 12 X 74			654	360	61
			140	77	26	Steel HP 14 X 102		
			204	112	31	140	77	23
			266	146	36	173	95	26
			323	177	41	249	137	31
			379	209	46	323	177	36
			436	240	51	390	215	41
			493	271	56	458	252	46
			538	296	61	526	289	51
			577	317	66	593	326	56
						661	363	61
						723	398	66
						769	423	71
						Steel HP 14 X 117		
						145	80	23
						180	99	26
						256	141	31
						330	182	36
						399	219	41
						467	257	46
						535	294	51
						603	332	56
						671	369	61
						734	403	66
						780	429	71
						Precast 14"x 14"		
						128	70	21

SUBSTRUCTURE===== **North Abutment**
 REFERENCE BORING ===== **B-1**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **602.68** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **600.68** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
418 KIPS	365 KIPS	201 KIPS	46 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1277** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **42.83** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 238.52 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 89.45 KIPS

PILE TYPE AND SIZE ===== **Steel HP 12 X 53**

Plugged Pile Perimeter===== 3.967 FT. Unplugged Pile Perimeter===== 5.800 FT.
 Plugged Pile End Bearing Area===== 0.983 SQFT. Unplugged Pile End Bearing Area===== 0.108 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
599.28	1.40	1.20			4.6		18.3	6.7		8.2	8	0	0	4	3
596.78	2.50	1.00			7.0	13.8	40.5	10.3	1.5	20.1	20	0	0	11	6
594.28	2.50	2.10			11.9	28.9	33.1	17.4	3.2	35.4	33	0	0	18	8
591.78	2.50	0.70			5.2	9.6	41.1	7.6	1.1	43.4	41	0	0	23	11
589.28	2.50	0.90			6.5	12.4	43.5	9.5	1.4	52.4	43	0	0	24	13
586.78	2.50	0.60			4.6	8.3	46.6	6.7	0.9	58.9	47	0	0	26	16
584.28	2.50	0.50			3.9	6.9	47.7	5.7	0.8	64.2	48	0	0	26	18
581.78	2.50	0.30			2.4	4.1	86.0	3.5	0.5	71.7	72	0	0	39	21
579.28	2.50	2.90			14.8	40.0	209.7	21.7	4.4	105.2	105	0	0	58	23
576.78	2.50		81	Hard Till	14.4	148.8	259.0	21.1	16.3	130.1	130	0	0	72	26
571.78	5.00		100	Hard Till	42.7	183.7	301.7	62.5	20.1	192.6	193	0	0	106	31
566.78	5.00		100	Hard Till	42.7	183.7	333.4	62.5	20.1	253.9	254	0	0	140	36
561.78	5.00		94	Hard Till	38.0	172.7	371.5	55.6	18.9	309.5	310	0	0	170	41
556.78	5.00		94	Hard Till	38.0	172.7	409.5	55.6	18.9	365.1	365	0	0	201	46
551.78	5.00		94	Hard Till	38.0	172.7	447.5	55.6	18.9	420.7	424	0	0	234	54
546.78	5.00		94	Hard Till	38.0	172.7	485.5	55.6	18.9	476.3	476	0	0	262	56
541.78	5.00		94	Hard Till	38.0	172.7	523.6	55.6	18.9	531.9	524	0	0	288	64
536.78	5.00		94	Hard Till	38.0	172.7	561.6	55.6	18.9	587.5	562	0	0	309	66
531.78	5.00		94	Hard Till	38.0	172.7	599.6	55.6	18.9	643.1	600	0	0	330	74
526.78	5.00		94	Hard Till		172.7			18.9						

Pile Design Table for South Abutment utilizing Boring #B-2

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
Metal Shell 12"Φ w/.25" walls			Steel HP 10 X 42			Steel HP 12 X 84		
144	79	21	130	71	28	107	59	23
Metal Shell 14"Φ w/.25" walls			182	100	33	171	94	28
69	38	18	234	129	38	235	129	33
185	102	21	287	158	43	299	164	38
Metal Shell 14"Φ w/.312" walls			Steel HP 10 X 57			363	200	43
69	38	18	136	75	28	427	235	48
185	102	21	189	104	33	491	270	53
Metal Shell 16"Φ w/.312" walls			241	133	38	555	305	58
79	43	18	294	162	43	602	331	63
230	127	21	347	191	48	Steel HP 14 X 73		
Metal Shell 16"Φ w/.375" walls			392	216	53	116	64	23
79	43	18	429	236	58	191	105	28
230	127	21	Steel HP 12 X 53			266	146	33
751	413	23	156	86	28	341	188	38
Steel HP 8 X 36			218	120	33	416	229	43
147	81	33	281	154	38	492	270	48
189	104	38	343	189	43	567	312	53
231	127	43	406	223	48	Steel HP 14 X 89		
264	145	48	Steel HP 12 X 63			123	67	23
			162	89	28	198	109	28
			225	124	33	274	151	33
			288	159	38	350	193	38
			352	193	43	426	234	43
			415	228	48	502	276	48
			479	263	53	577	318	53
			Steel HP 12 X 74			653	359	58
			103	57	23	Steel HP 14 X 102		
			167	92	28	128	70	23
			230	127	33	204	112	28
			294	162	38	280	154	33
			358	197	43	356	196	38
			421	232	48	432	238	43
			485	267	53	508	280	48
			548	302	58	584	321	53
						660	363	58
						737	405	63
						Steel HP 14 X 117		
						134	74	23
						211	116	28
						288	158	33
						365	201	38
						441	243	43
						518	285	48
						595	327	53
						671	369	58
						748	411	63
						Precast 14"x 14"		
						88	48	18
						235	129	21

SUBSTRUCTURE===== **South Abutment**
 REFERENCE BORING ===== **B-2**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **602.68** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **600.68** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
497 KIPS	479 KIPS	263 KIPS	53 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1277** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **42.83** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 238.52 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 89.45 KIPS

PILE TYPE AND SIZE ===== **Steel HP 12 X 63**

Plugged Pile Perimeter===== 4.000 FT. Unplugged Pile Perimeter===== 5.883 FT.
 Plugged Pile End Bearing Area===== 1.000 SQFT. Unplugged Pile End Bearing Area===== 0.128 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
599.28	1.40	1.40			5.1		22.0	7.6		9.7	10	0	0	5	3
596.78	2.50	1.20			8.2	16.8	32.9	12.1	2.1	22.1	22	0	0	12	6
594.28	2.50	1.40			9.2	19.6	44.9	13.5	2.5	36.0	36	0	0	20	8
591.78	2.50	1.60			10.1	22.4	38.2	14.8	2.9	48.6	38	0	0	21	11
589.28	2.50	0.40			3.2	5.6	52.5	4.7	0.7	54.7	53	0	0	29	13
586.78	2.50	1.20			8.2	16.8	48.1	12.1	2.1	65.1	48	0	0	26	16
584.28	2.50	0.30			2.4	4.2	49.1	3.6	0.5	68.5	49	0	0	27	18
581.78	2.50	0.20			1.6	2.8	91.0	2.4	0.4	76.1	76	0	0	42	21
579.28	2.50		23	Hard Till	2.5	43.0	237.3	3.7	5.5	98.1	98	0	0	54	23
574.28	5.00		100	Hard Till	43.1	186.8	280.4	63.4	23.9	161.6	162	0	0	89	28
569.28	5.00		100	Hard Till	43.1	186.8	323.6	63.4	23.9	225.0	225	0	0	124	33
564.28	5.00		100	Hard Till	43.1	186.8	366.7	63.4	23.9	288.4	288	0	0	159	38
559.28	5.00		100	Hard Till	43.1	186.8	409.8	63.4	23.9	351.8	352	0	0	193	43
554.28	5.00		100	Hard Till	43.1	186.8	452.9	63.4	23.9	415.2	415	0	0	228	48
549.28	5.00		100	Hard Till	43.1	186.8	496.0	63.4	23.9	478.6	479	0	0	263	53
544.28	5.00		100	Hard Till	43.1	186.8	539.1	63.4	23.9	542.0	539	0	0	297	58
539.28	5.00		100	Hard Till	43.1	186.8	582.2	63.4	23.9	605.4	582	0	0	320	63
534.28	5.00		100	Hard Till		186.8			23.9						