STRUCTURE GEOTECHNICAL REPORT PAULINA STREET BRIDGE OVER INTERSTATE 290 AND THE CTA SN 016-0098 CHICAGO, COOK COUNTY, ILLINOIS

For Collins Engineers 550 West Jackson Blvd., Suite 1200 Chicago, IL. 60661

Submitted by
Wang Engineering, Inc.
1145 North Main Street
Lombard, IL 60148

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replaced and the existing v indicate the existing abutm loading from conventional abutment walls and decreas with lightweight cellular c and a standard IDOT 30-fc piers will remain with recc abutment length of 274.9 geotechnical recommendate. The lithological succession hard silty clay to silty clay feet. Beneath the fill, borin loam to very dense silt t encountered refusal at the Groundwater was observed. We estimate the new apprelightweight concrete cellul	beams along Paulina Street bridge over aulted abutments will remain and will be ent piles cannot support additional later fill materials. Therefore, to reduce the see foundation soil settlements the abutme concrete. We understand the existing apport approach slab with the sleeper slab constructed bearing seats. The four-span feet and will have an out-to-out widths ons for the design of the proposed improvement of the p	re backfilled to the top. Evaluations ral pressure or increased settlement lateral pressure on the back of the ent vaults should be filled to the top proach pile bents will be removed will be constructed. The main-span bridge will have a back-to-back of of 88.3 feet. This report provides overnents. ploration revealed medium stiff to to an elevation of about 585 to 590 lty clay followed by hard silty clay 195.8 and 508.3 feet, the borings good quality dolostone bedrock. The bearing pressure of 550 psf. The aximum density of 35 pcf and will						
	esistance of 1,500 psf. Under the new lowe estimate total settlements of about 1.0							

12. Path to archived file



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STRUCTURE GEOTECHNICAL REPORT PAULINA STREET BRIDGE OVER INTERSTATE 290 AND THE CTA CHICAGO, COOK COUNTY, ILLINOIS SN 016-0098 FOR COLLINS ENGINEERS

1.0 Introduction

This report presents the results of our subsurface investigation, laboratory testing, geotechnical evaluations, and recommendations to support the design of the proposed improvements along Paulina Street Bridge over Interstate 290 (I-290) in Chicago, Cook County, Illinois. A *Site Location Map* is presented as Exhibit 1.

The purpose of this investigation was to characterize the site soil and groundwater conditions, perform geotechnical engineering analyses, and provide recommendations for the design of the proposed improvements.

1.1 Existing and Proposed Structure

Based on the *General Plan and Elevation (GPE)* drawing attached as Appendix B and provided by Collins Engineers, Wang Engineering, Inc. (Wang) understands that the existing 1954 bridge is a four-span, non-composite, continuous wide flange steel beam structure with concrete closed vaulted wall abutments and three reinforced concrete multi-column piers all supported on metal shell cast-in-place concrete piles.

The existing four span deck and steel beams along Paulina Street Bridge over Interstate 290 will be removed and replaced with shallower beams to increase vertical clearance over I-290. The existing bridge has vaulted abutments that will remain in place; however, the proposed work includes removing the pile bents supporting the existing approach slabs, filling the vaults behind the abutments to the base of the proposed pavement and approach slabs, and construct the typical 30 feet approach slab with the typical IDOT approach sleeper slab. The piers will remain with reconstructed bearing seats. The new bridge deck will have a back-to-back of abutment length of 274.9 feet and will have an out-to-out width of 88.3 feet. The profile grade along Paulina Street will remain the same.



2.0 Investigation Methods

The following sections outline the subsurface and laboratory investigations performed by Wang.

2.1 Field Investigation

The subsurface investigation consisted of three structure borings, designated as PAU-01 to PAU-03, drilled by Wang in May and June 2024. The borings were drilled at elevations of 592.6 to 602.8 feet and were advanced to depths of 69.3 to 104.5 feet bgs. The as-drilled northings, eastings, and elevations were acquired by Wang with a mapping-grade GPS unit. Boring location data are presented in the *Boring Logs* (Appendix A) and the locations are shown in the *Boring Location Plan* (Exhibit 2).

A truck-mounted drilling rig, equipped with hollow stem augers and mud rotary equipment, was used to advance and maintain open boreholes. Soil sampling was performed according to AASHTO T206, "Penetration Test and Split Barrel Sampling of Soils." The soil was sampled at 2.5-foot intervals to a depth of 30.0 feet bgs and at 5-foot intervals thereafter to the boring termination depths. Soil samples collected from each interval were placed in sealed jars and transferred to the laboratory for further examination and testing. The bedrock was cored at the boring location in a 10-foot run with an NWD4-sized core barrel.

Field boring logs, prepared and maintained by Wang field engineers, include lithological descriptions, visual-manual soil (IDH Textural) Classifications, results of Rimac and pocket penetrometer unconfined compressive strength tests, and results of Standard Penetration Tests (SPT) recorded as blows per 6 inches of penetration.

Groundwater observations were made in boreholes during and at end of drilling operations. Boreholes were grouted upon completion and, where necessary, the pavement surface was restored as much as possible to its original condition.

2.2 Laboratory Testing

Soil samples were tested in the laboratory for moisture content. Field visual descriptions of the soil samples were verified in the laboratory and the tested samples were classified in accordance with the IDH Soil Classification System. Laboratory test results are shown in the *Boring Logs* (Appendix A).



3.0 INVESTIGATION RESULTS

Detailed descriptions of the soil conditions encountered during the subsurface investigation are presented in the attached *Boring Logs* (Appendix A) and in the *Soil Profile* (Exhibit 3). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

3.1 Lithological Profile

Along the surface of Paulina Street, the borings encountered a 2- to 3-inch-thick asphalt overlay on top of 5.5- to 12-inch-thick concrete and an aggregate base. In descending order, the general lithologic succession encountered beneath the surface includes: 1) man-made ground (fill); 2) very soft to medium stiff silty clay; 3) very stiff silty clay; 4) hard silty clay loam to very dense silt to silty loam; and 5) Strong, good quality dolostone.

1) Man-made ground (fill)

Beneath the pavement, the borings revealed an embankment consisting of medium stiff to hard silty clay to silty clay loam fill extending down to an elevation of about 585 to 590 feet. The cohesive fill has unconfined compressive strength (Qu) values of 0.5 to 4.5 tsf and moisture content values of 4 to 21%.

2) Very soft to soft silty clay

Beneath the fill, the borings encountered a very soft to soft silty clay extending down to an elevation of about 554 to 566 feet. The cohesive fill has unconfined compressive strength (Qu) values of 0.16 to 0.41 tsf and moisture content values of 20 to 28%.

3) Very stiff silty clay

Beneath the soft clay, the borings advanced very stiff, gray silty clay with Q_u values of 1.5 to 4.0 and moisture contents of 17 to 26%. This soil unit continues to elevations of about 539 to 548 feet.

4) Hard silty clay loam to very dense silt to silty loam

At elevations of 539 to 548 feet, the borings advanced through hard silty clay loam. This unit has unconfined compressive strength (Q_u) values of 2.8 to 8.5 tsf; N-value of 50 blows per foot of penetration and moisture content values of 8 to 23%.



5) Dolostone Bedrock

At elevations of 495.8 and 508.3 feet, the borings encountered refusal at the top of bedrock. Bedrock coring at Boring PAU-03 recovered strong, light and dark gray, good quality dolostone. The dolostone has a Rock Quality Designation (RQD) of 90% and a recovery of 96%.

3.2 Groundwater Conditions

Groundwater was not observed while drilling in any of the borings. We estimate that groundwater on site is deep-seated and will not impact the proposed improvement. It should be noted, however, that fluctuations in groundwater level may occur due to variations in the rainfall, other climatic conditions, or other factors not evident at the time measurements were made and reported herein.

4.0 ANALYSIS AND RECOMMENDATIONS

Geotechnical evaluations and recommendations for the proposed improvements are included in the following sections. The existing profile grade along Paulina Street will not be significantly altered. The designed plan is to replace the existing, pile-bent supported approach slabs by filling the existing vault area and placing typical IDOT 30-feet long approach slabs. Thus, the existing void spaces within the vaults and behind the abutments are proposed to be backfilled. However, evaluations estimate the existing abutment piles cannot support the additional lateral soil pressure and the proposed settlement of the very soft to soft silty clay will induce additional vertical loads on the piles. To reduce the lateral loading and limit the proposed foundation soil settlements we recommend filling the vaults with Class I or Class II lightweight cellular concrete with a maximum density of 35 pcf.

4.1 Seismic Design Considerations

The seismic hazard for the site was evaluated in accordance with IDOT (2020) and AASHTO (2022). The Seismic Soil Site Class was determined per the requirements of *All Geotechnical Manual Users* (AGMU) Memo 9.1, *Design Guide for Seismic Site Class Determination*, and the accompanying spreadsheet. A global Site Class Definition was determined for this project, and was found to be Soil Site Class D. The project location belongs to the Seismic Performance Zone 1. The seismic spectral acceleration parameters recommended for design in accordance with the *AASHTO LRFD Bridge Design Specifications* (AASHTO 2020) are summarized in Table 3. According to the IDOT *Bridge Manual* (IDOT 2023), liquefaction analysis is not required for structures located in Seismic Performance Zone 1.



Table 1: Recommended Seismic Design Parameters

Spectral	Spectral Acceleration	-	Design Spectrum for
Acceleration Period	Coefficient1)	Site Factors	Site Class D
(sec)	(% g)		(% g)
0.0	PGA= 4.2	$F_{pga}=1.6$	$A_s=6.7$
0.2	$S_s = 9.0$	$F_a = 1.6$	S _{DS} = 14.5
1.0	$S_1 = 3.6$	$F_v = 2.4$	$S_{D1}=8.6$

¹⁾ Spectral acceleration coefficients based on Site Class D

4.2 Approach Slab and New Embankments

Wang has evaluated the bearing capacity and potential settlement of the approach slabs and vault fill. The existing pavement elevation along Paulina Street is approximately 592 to 602 feet.

4.2.1 Bearing Capacity

Based on the information provided, we understand new approach slabs will be supported on lightweight cellular concrete fill. We estimate the new approach slabs will apply a maximum service bearing pressure of 550 psf, which includes an 18-inch-thick approach slab, 6-inches of subbase and 250 psf live load surcharge. According to the cellular concrete manufacturer, the lightweight concrete cellular fill has a maximum bearing resistance of 1,500 psf (https://www.texasce.org/tce-news/lightweight-cellular-concrete-2/.)

4.2.2 Approach Slab and New Embankment Settlement

The vault areas behind the existing abutments should be filled with lightweight cellular concrete from the existing surface to the base elevations of the proposed approach slabs. The existing granular fill within the abutments can remain. Constructing the new embankment with approximately 15 feet of lightweight material will reduce the load transferred to the bottom of the embankment and the lateral loading on the existing abutment walls. We estimate the 18-inch-thick slab, 6-inch-thick subbase, 15-foot-thick cellular concrete of 35 pcf unit weight, and live load of 250 psf, will induce an approach slab settlement of about 1 inch.

4.2.4 Lateral Design Pressure

The lateral earth pressure on the existing abutment walls induced by the 35 pcf maximum density

²⁾ Site Class D Spectrum to be included on plans; $A_s = PGA*F_{pga}; S_{DS} = S_s*F_a; S_{DI} = S_1*F_v$



lightweight cellular concrete should be evaluated for the walls in the short-term (undrained) and long-term (drained) conditions using the soil parameters recommended in Tables 2 and 3. Additional lateral surcharge pressures of 250 psf should be included in the analysis (AASHTO 2020).

Table 2: Undrained Geotechnical Parameters for Wall Design

Soil Type (Layer)	Unit Weight, γ (pcf)	Undrained Shear Strength, c _u (psf)	Estimated Friction Angle, Φ (°)	Active Pressure Coefficient, K _a (Horizontal)	Passive Pressure Coefficient, K _p (Horizontal)
Lightweight Concrete Fill EL 598 to 575.4 feet	35	0	35(1)	0.27	3.69
Existing Granular Fill EL 575.4 to 570 feet	120	0	30	0.33	3.00
V Soft to Soft Silty Clay EL 570 to 554 feet	110	320	0	1.00	1.00
V Stiff Silty Clay EL 554 to 540 feet	120	2,500	0	1.00	1.00
Hard Silty Clay Loam EL 540 to 525 feet	125	5,000	0	1.00	1.00
V Dense Silt to Silty Loam EL 525 to 500 feet	63 (submerged)	0	36	0.26	3.85

¹⁾ Based on results determined from direct shear test (Tiwari et al., 2017)

Table 3: Drained Geotechnical Parameters for Wall Design

Soil Type (Layer)	Unit Weight, γ (pcf)	Undrained Shear Strength, c _u (psf)	Estimated Friction Angle, Φ (°)	Active Pressure Coefficient, K _a (Horizontal)	Passive Pressure Coefficient, K _p (Horizontal)
Lightweight Concrete Fill EL 598 to 575.4 feet	35	0	35(1)	0.27	3.69
Existing Granular Fill EL 575.4 to 570 feet	120	0	30	0.33	3.00
V Soft to Soft Silty Clay EL 570 to 554 feet	110	50	26	0.39	2.56
V Stiff Silty Clay EL 554 to 540 feet	120	100	30	0.33	3.00
Hard Silty Clay Loam EL 540 to 525 feet	125	100	31	0.32	3.12
V Dense Silt to Silty Loam EL 525 to 500 feet	63 (submerged)	0	36	0.26	3.85

¹⁾ Based on results determined from direct shear test (Tiwari et al., 2017)



5.0 CONSTRUCTION CONSIDERATIONS

5.1 Site Preparation

Pavement and debris should be cleared and stripped where the structure and structural fill will be placed. The exposed subgrade should be observed and evaluated by a qualified engineer. If unstable or unsuitable materials are exposed during excavation, they should be removed and replaced with compacted structural fill as described in Section 5.2.

5.2 Excavation, Dewatering, and Utilities

Excavations should be performed in accordance with local, state, and federal regulations including current OSHA regulations. The potential effect of ground movements upon nearby utilities should be considered during construction. Temporary excavations should be sloped at no steeper than 1:2 (V:H). Excavated material should not be stockpiled immediately adjacent to the top of slopes, nor should equipment be allowed to operate too closely to open excavations.

Groundwater was not observed while drilling in any of the borings. The groundwater will not affect the proposed improvements.

5.3 Filling and Backfilling

Fill material used to attain final design elevations outside of the lightweight cellular concrete sections should be pre-approved, compacted, cohesive or granular soil conforming to IDOT Section 205, *Embankment* (2022). The fill material should be free of organic matter and debris and should be placed in lifts and compacted according to the standard. Backfill material must be preapproved by the Resident Engineer and should be placed and compacted in accordance with the specification (IDOT 2022).

The lightweight cellular concrete placed behind the existing vaults should be Class I or Class II in accordance with IDOT Guide Bridge Special Provision (GBSP) No. 87, *Lightweight Cellular Concrete Fill* (2016). The fill should be mixed and installed in accordance with the GBSP.

5.4 Earthwork Operations

The required earthwork can be accomplished with conventional construction equipment. Moisture and traffic will cause deterioration of exposed subgrade soils. Precautions should be taken by the Contractor to prevent water erosion of the exposed subgrade. A compacted subgrade will minimize

Wang No KE235325 Paulina Street Bridge over I-290 January 20, 2025 Wang Engineering

A Ferracon Company

water runoff erosion.

Earth moving operations should be scheduled to not coincide with excessive cold or wet weather (early spring, late fall or winter). Any soil allowed to freeze or soften due to the standing water should be removed. Wet weather can cause problems with subgrade compaction.

It is recommended that an experienced geotechnical engineer be retained to inspect the exposed subgrade, monitor earthwork operations, and provide material inspection services during the construction phase of this project.

6.0 QUALIFICATIONS

The analysis and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 2. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. In the event that any changes in the design and/or location of the structure are planned, we should be timely informed so that our recommendations can be adjusted accordingly.

It has been a pleasure to assist Collins Engineers and the Illinois Department of Transportation on this project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

Wang Engineering, Inc. (A Terracon Company)

Ehab Shaheen, Ph.D, P.E. Senior Geotechnical Engineer

Mickey Snider, P.E. Senior Geotechnical Engineer

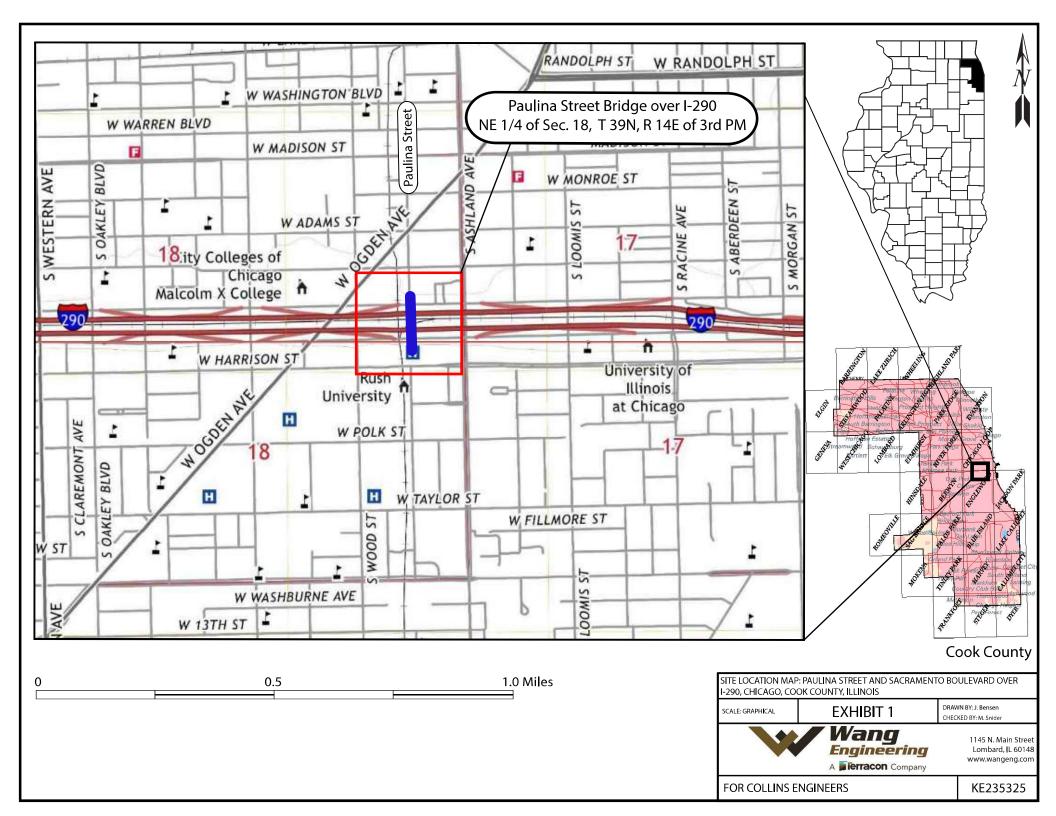


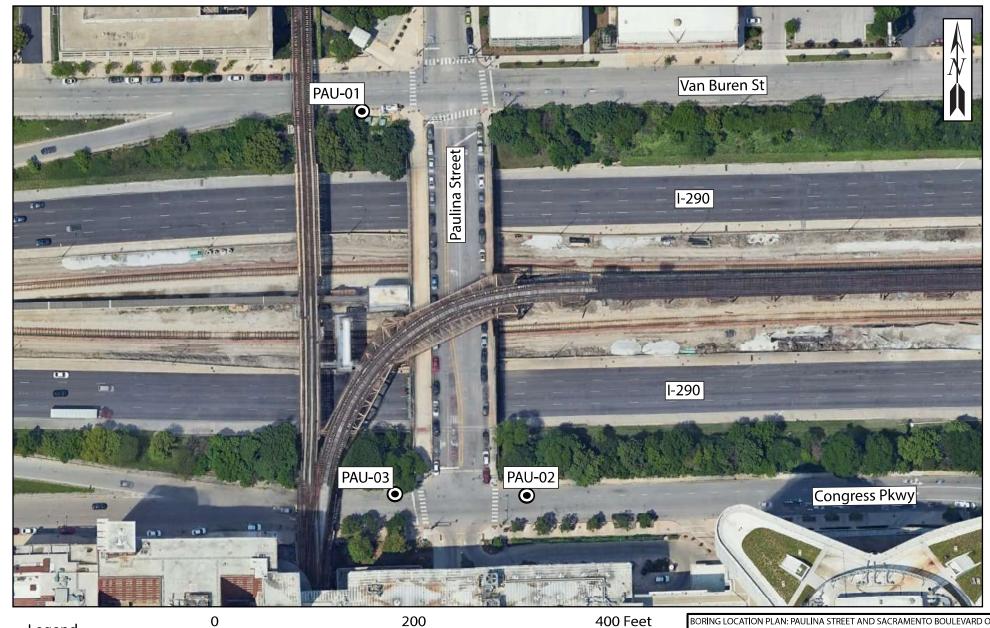
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EXHIBITS





Legend

Soil Borings

BORING LOCATION PLAN: PAULINA STREET AND SACRAMENTO BOULEVARD OVER I-290, CHICAGO, COOK COUNTY, ILLINOIS

SCALE: GRAPHICAL

EXHIBIT 2

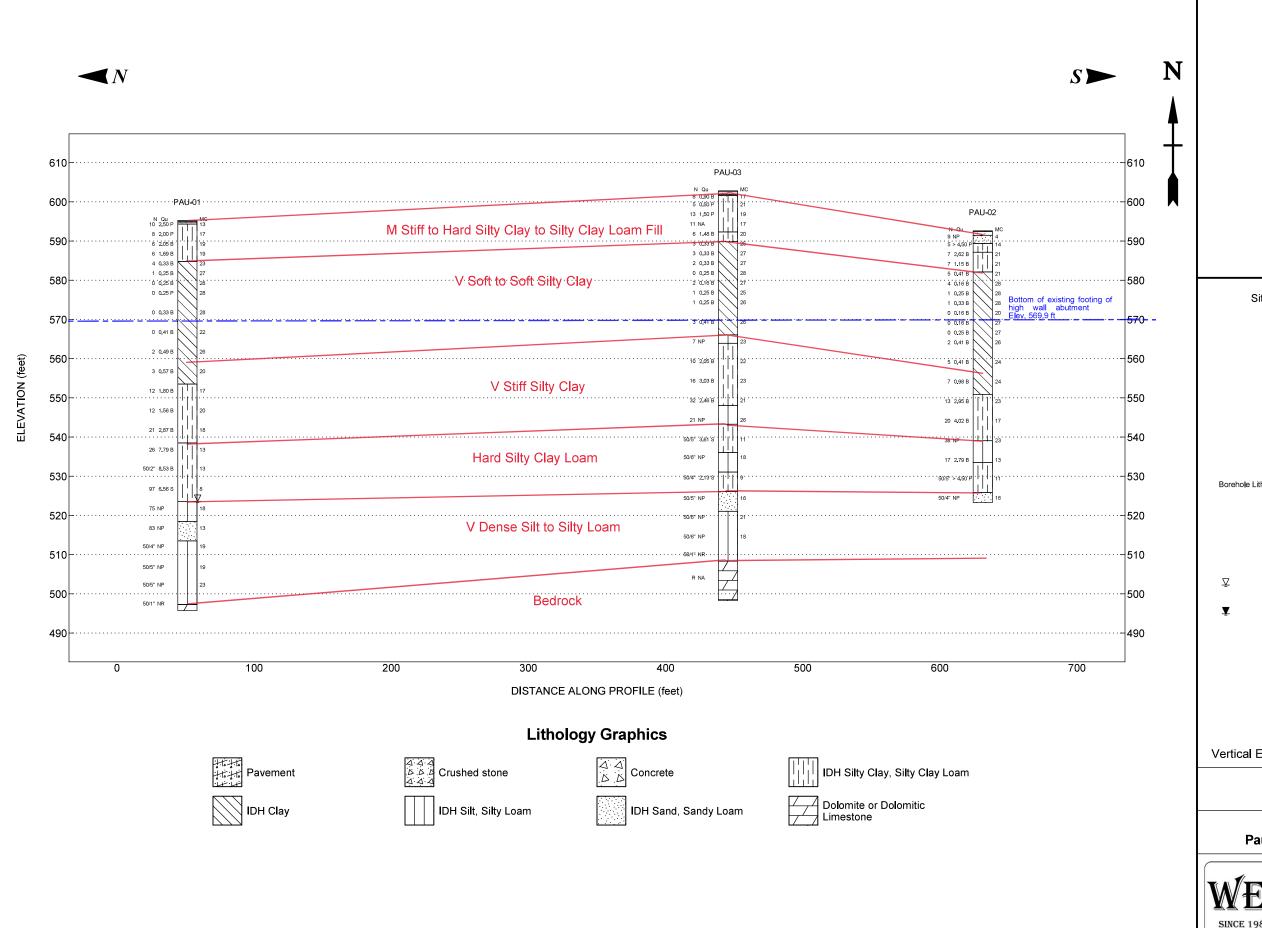
DRAWN BY: J. Bensen CHECKED BY: M. Snider

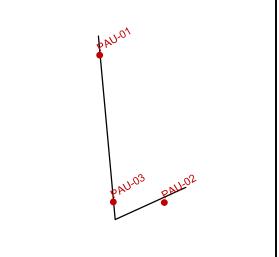


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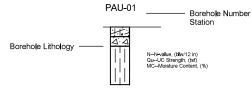
KE235325





Site Map Scale 1 inch equals 255 feet

Explanation:



Water Level Reading at time of drilling. Water Level Reading end of drilling



Vertical Exaggeration: 3x

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Subsurface Data Profile Paulina Street Bridge over I-290



Paulina Street and Sacramento Blvd over Interstate 290 Chicago, Cook County, IL

JOB NUMBER PLATE NUMBER KE235325 EXHIBIT 3



APPENDIX A



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BORING LOG PAU-01

WEI Job No.: KE235325

Collins Engineers

Proj Raulina Street and Sacramento Blvd over Interstate 290 Station: Location Chicago, Cook County, IL

Datum: NAVD88 Elevation: 595.26 ft North: 1898199.16 ft East: 1165040.73 ft

Profile	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery Sample No.	SPT (blw/6 in) RQD (%)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft) Sample Type Recovery Sample Type Robert Sample No. SPT (blw/6 in) RQD (%)	(tsf) Moisture Content (%)
	595, 12.5-inch thick ASPHALT 594, 33-inch thick, brown SANDY GRAVEL 5.5-inch thick CONCRETEPAVEMENT		1	12 5 5	2.50 P	13			
	Stiff to very stiff, brown, gray and black SILTY CLAY LOAM to SILTY CLAY, trace gravelFILLRDR 2		2	3 4 4	2.00 P	17		1	.41 22 B
	 	1	3	2 2 4	2.05 B	19			
	584.8	10	4	2 3 3	1.69 B	19			.49 26 B
	Soft to medium stiff, gray CLA' to SILTY CLAY, trace gravel RDR 1	7	5	1 2 2	0.33 B	23			
		15	6	0 0 1	0.25 B	27			.57 20 B
		1	7	0 0 0	0.25 B	28		553.5 Stiff to very stiff, gray SILTY CLAY, trace gravelRDR 2	
		20	8	0 0 0	0.25 P	28		13 3 1	.80 17 B
DT 6/25/24		-							
MANGENGINC KE235325.GPJ WANGENG.GDT		25/	9	0 0 0	0.33 B	28		50 7 7	.56 20 B
325.G	GENERA 05 00 0004		WATER LEVEL DATA						
E235	egin Drilling 05-22-2024	Comp	While Drilling ☐ Dry to 10' [24] While Drilling ☐ Dry to 10'						
N N	rilling Contractor Wang Testing \$ riller RH&JD Logger								
D G	rilling Method 2,25" ID HSA to 10		illed Depth to Water ▼ NA						
WANC	upon completion		TI 1 CC C F 10 10 1 1 1						



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BORING LOG PAU-01

WEI Job No.: KE235325

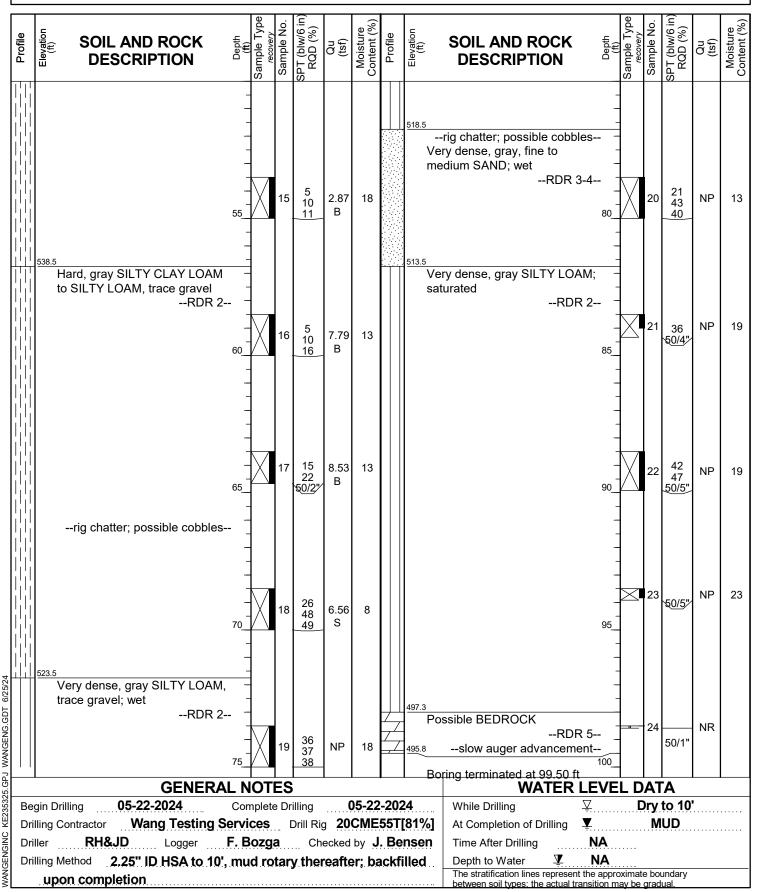
Client Collins Engineers

ProjRaulina Street and Sacramento Blvd over Interstate 290

on Chicago, Cook County, IL

Datum: NAVD88 Elevation: 595.26 ft North: 1898199.16 ft East: 1165040.73 ft

Station: Offset:





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BORING LOG PAU-02

WEI Job No.: KE235325

Collins Engineers

Proj Raulina Street and Sacramento Blvd over Interstate 290 Station: Chicago, Cook County, IL

Datum: NAVD88 Elevation: 592.63 ft North: 1897805.11 ft East: 1165213.66 ft

Profile	SOIL AND ROCK defection DESCRIPTION	Sample Type	Sample No.	SPT (blw/6 in RQD (%)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCI	Cepth (#)	Sample Type	SPT (blw/6 in RQD (%)	Qu (tsf)	Moisture Content (%)
100	592.52-inch thick ASPHALT 591.512-inch thick CONCRETEPAVEMENT Loose, brown and white, fine SAND, trace gravel; damp 589.4FILL		1	4 5 4	NP	4				- - - -	11		0.25 B	27
	Hard, brown SILTY CLAY LOAM, little to some gravel; moist 5_587.11 inch asphalt on bottom of		2	13 3 2	> 4.50 P	14				30_	12	0 1 1	0.41 B	26
	Stiff to very stiff, brown and gray SILTY CLAY, trace gravel; moist		3	2 3 4	2.62 B	21				- - -				
	FILL RDR 2 - 10_		4	3 3 4	1.15 B	21				- - - 35_	13	3 0 2 3	0.41 B	24
	Very soft to medium stiff, gray CLAY to SILTY CLAY, trace gravel; moistRDR 2		5	2 2 3	0.41 B	21				- - - -	- - - - -			
	15_		6	0 2 2	0.16 B	28				40_	14	2 3 4	0.98 B	24
			7	0 0 1	0.25 B	28			ry stiff to hard, gray SIL AY, trace gravel; moist	-				
	20_		8	0 0 1	0.33 B	28			R	DR 2 - - - 45_	15	5 6 7	2.95 B	23
6/25/24	-		9	0 0 0	0.16 B	20				- - - -				
WANGENGINC KE235325.GPJ WANGENG.GDT	- - - 25_		10	0 0 0	0.16 B	27				- - 50_	16	6 7 13	4.02 B	17
.GPJ	GENERAL N		WATF	R LEVE	L DA	TA								
3532£ Be	Begin Drilling 06-05-2024 Complete Drilling 06-05-2024								While Drilling	<u> </u>		to 10	•	
Ž Dr	Illing Contractor Wang Testing Serv	At Completion of Drilling MUD												
S Dr	Driller KS> Logger A. Scifers Checked by J. Bensen								Time After Drilling NA					
틸 Dr	lling Method 2.25" ID HSA to 10', mu	ıd ro	tary	/ the	eafte	er; ba	ackf	illed	Depth to Water 🛂 NA					
\ \ \ \	upon completion	The stratification lines represent the approximate boundary between soil types: the actual transition may be gradual.												



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Fax:

BORING LOG PAU-02

WEI Job No.: KE235325

Collins Engineers

Proj Raulina Street and Sacramento Blvd over Interstate 290 Station: Chicago, Cook County, IL

Datum: NAVD88 Elevation: 592.63 ft North: 1897805.11 ft East: 1165213.66 ft

Medium dense to dense, gray Sil. TY LOAM, trace gravel; Sil. TY LOAM, trace gravel; Sil. TY LOAM, trace gravel; Sil. TY LOAM to Sil. TY LOAM, solution of Sil. Ty LoAM, soluti	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type	Sample No.	SPT (blw/6 in) RQD (%)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (#)	Sample Type	Sample No.	SPT (blw/6 in) RQD (%)	Qu (tsf)	Moisture Content (%)
CLÁY LOAM to SILTÝ LOAM, 60 11 11 B little gravel; moist		N 5	SILTY LOAM, trace gravel; moist	55_			13 14	NP	23									
GENERAL NOTES Begin Drilling 06-05-2024 Complete Drilling Contractor Wang Testing Services Drill Rig 20CME55T[81%] 19		\	CLAY LOAM to SILTY LOAM, ittle gravel; moist RDR 2-3-	<u> </u>		18	10 6 11		13									
From 63.5' to 68.5' Very dense, gray SANDY LOAM, trace gravel; moist S23.3 Boring terminated at 69.33 ft To GENERAL NOTES Begin Drilling 06-05-2024 Complete Drilling Drilling Contractor Wang Testing Services Drill Rig 20 37 NP 16 WATER LEVEL DATA While Drilling At Completion of Drilling MUD		525.9	63.5'-	- - 65_ -		19			11									
GENERAL NOTES WATER LEVEL DATA Begin Drilling 06-05-2024 Complete Drilling 06-05-2024 While Drilling Drilling Contractor Wang Testing Services Drill Rig 20CME55T[81%] At Completion of Drilling MUD		523.3	from 63.5' to 68.5'- Very dense, gray SANDY LOAM, trace gravel; moist RDR 4-	 - - -				NP	16									
Drilling Contractor Wang Testing Services Drill Rig 20CME55T[81%] At Completion of Drilling WUD			GENERA		OT	ES						WATE	R LEVE) 	Ā		
Drilling Contractor Wang Testing Services Drill Rig 20CME55T[81%] At Completion of Drilling ▼ MUD Driller KS> Logger A. Scifers Checked by J. Bensen Time After Drilling NA Drilling Method 2.25" JD HSA to 10', mud rotary thereafter: backfilled Depth to Water ▼ NA	ı													-		•		
upon completion The stratification lines represent the approximate boundary between soil types: the actual transition may be gradual.	Dri Dri Dri	Driller KS> Logger A. Scifers Checked by J. Bensen Drilling Method 2.25" ID HSA to 10', mud rotary thereafter; backfilled								Time After Drilling Depth to Water	NA NA				••••			



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WANGENGINC KE235325.GPJ WANGENG.GDT 6/25/24

BORING LOG PAU-03

WEI Job No.: KE235325

Collins Engineers

Proj Raulina Street and Sacramento Blvd over Interstate 290 Station: Location Chicago, Cook County, IL

Datum: NAVD88 Elevation: 602.83 ft North: 1897806.69 ft East: 1165077.27 ft

Profile	uoitin SOIL AND ROCK the decision of the decis	Sample Type	SPT (blw/6 in) RQD (%)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft) Sample Type	sample No.	SPT (blw/6 in) RQD (%)	Qu (tsf)	Moisture Content (%)
	602.63-inch thick ASPHALT 601.89-inch thick CONCRETEPAVEMENT/ 3-inch thick GRAVELBASE COURSE		1 2 3 3	0.90 B	17					11		0.25 B	25
	Medium stiff to stiff, black, brown, and gray SILTY CLAY, trace gravel; moistFILL 5moved 2' north due to		2 3 2 3	0.50 P	21				30	12	0 0 1	0.25 B	26
	unknown concrete structure, _ possilble storm sewer about 3 ft _ bgs - -		3 5 6 7	1.50 P	19								
	592.3 Stiff, gray SILTY CLAY, trace		4 5 5 6	NA	17				35	13	0 1 2	0.41 B	26
	gravel; moistRDR 2<1-inch thick sand seam 589.8 Very soft to soft, gray CLAY to		5 2 3 3	1.48 B	20		566.1 Lo	ose, gray SILT; moist to wet RDR 2					
	SILTY CLAY, trace gravel; moistRDR 2		6 2 2 1	0.33 B	25			ery stiff, gray SILTY CLAY to _AY, trace gravel; moist RDR 2	40 7	/ 14	5 4 3	NP	23
			7 0 1 2	0.33 B	27								
		X t	8 0 1 1	0.33 B	27				45	/ 15	6 4 6	2.05 B	22
	- - - - -		9 0 0 0	0.25 B	28								
	25_ GENERAL N		10 0 1 1	0.16 B	27			WATER L	50	16	9	3.03 B	23
i Ra	gin Drilling 06-04-2024 Com	While Drilling			to 10	•							
ÝΙ	illing Contractor Wang Testing Service	At Completion of Drilling			IUD								
	iller KS> Logger A. Se	· · · · · · · · · · · · · · · · · · ·	NA	!7	·~.~								
41	illing Method 2.25" ID HSA to 10', mu		NA										
	upon completion		-					The stratification lines represent the between soil types: the actual trans	e approxim	ate bo	oundary dual.		



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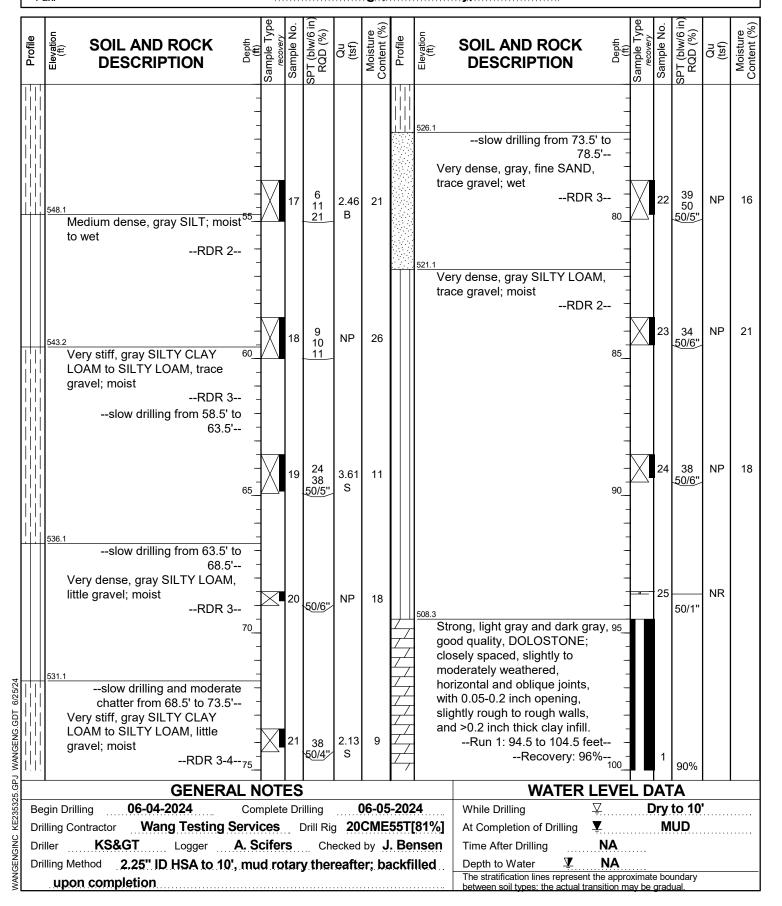
BORING LOG PAU-03

WEI Job No.: KE235325

Collins Engineers

Proj Raulina Street and Sacramento Blvd over Interstate 290 Station: Chicago, Cook County, IL

Datum: NAVD88 Elevation: 602.83 ft North: 1897806.69 ft East: 1165077.27 ft





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BORING LOG PAU-03

WEI Job No.: KE235325

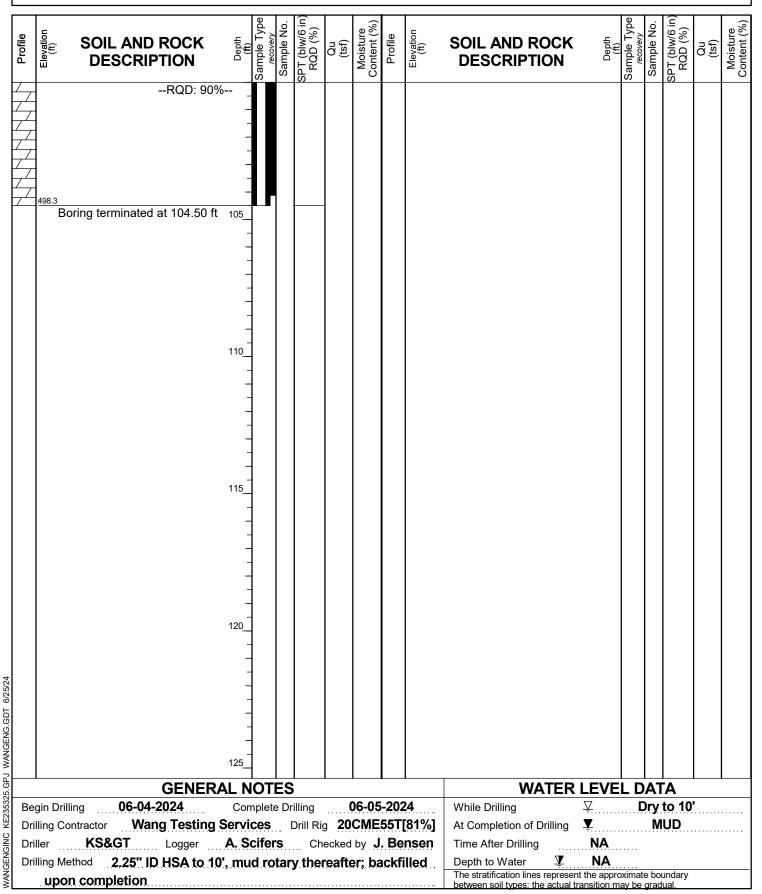
Client Collins Engineers

Proj**₽aulina Street and Sacramento Blvd over Interstate 290**

Chicago, Cook County, IL

Datum: NAVD88 Elevation: 602.83 ft North: 1897806.69 ft East: 1165077.27 ft

Station: Offset:



Run #1



Boring PAU-03: Run #1, 94.5 to 104.5 feet, RECOVERY=96%, RQD=90% BEDROCK CORE PHOTOS: PAULINA STREET AND SACRAMENTO BOULEVARD OVER I-290, CHICAGO, COOK COUNTY, ILLINOIS

SCALE: GRAPHICAL

APPENDIX A

DRAWN BY: J. Bensen CHECKED BY: M. Snider



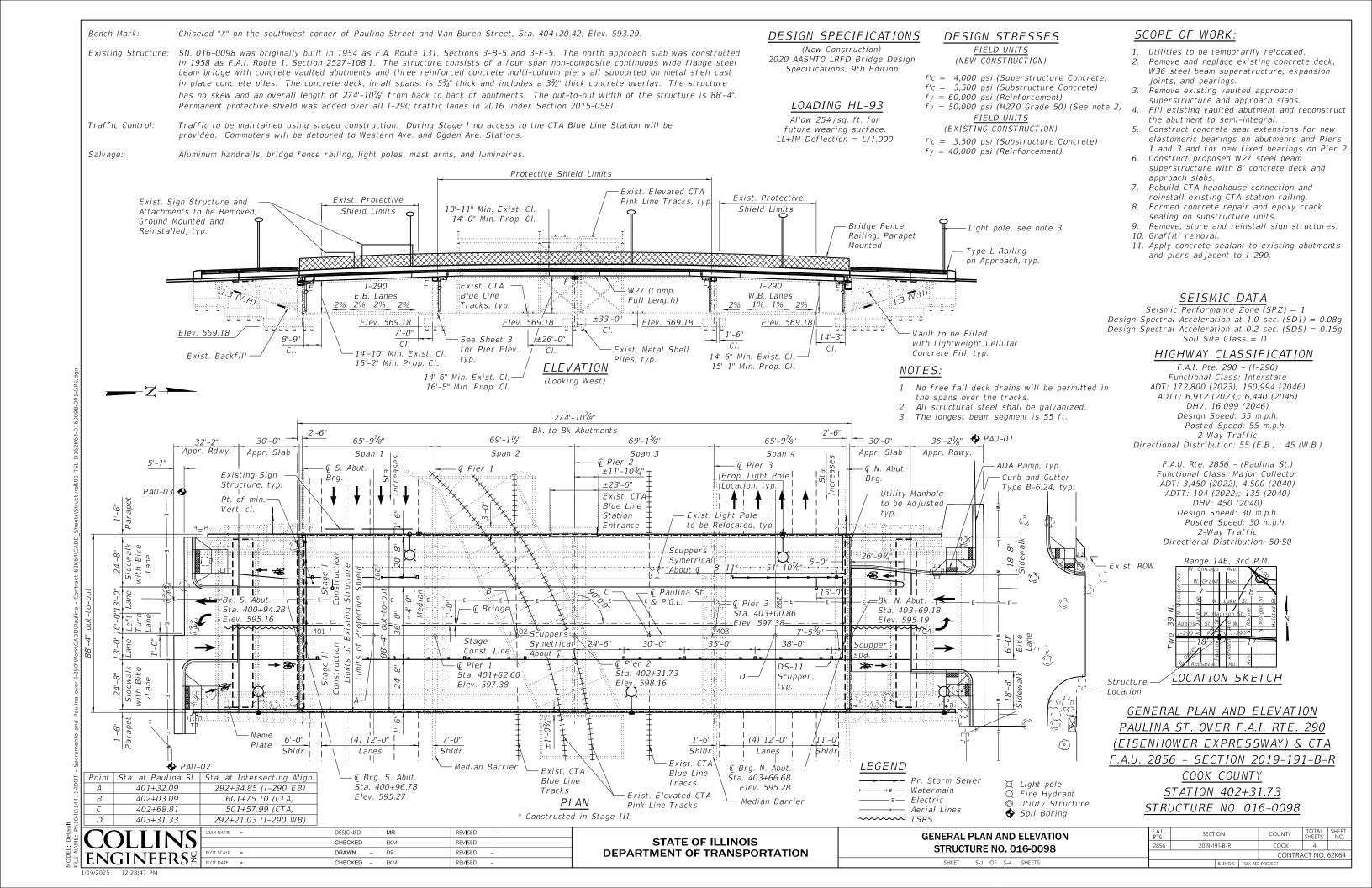
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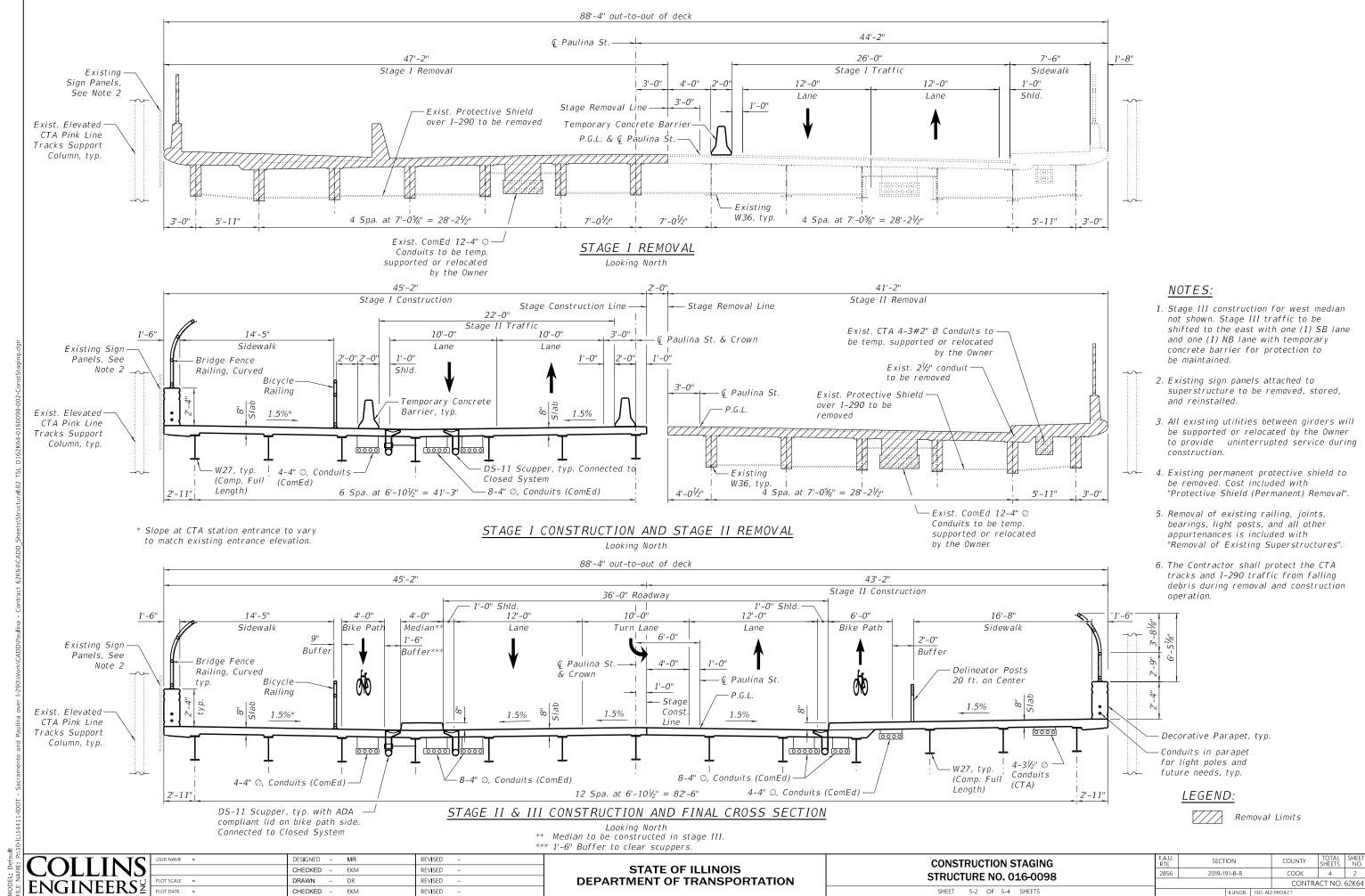
FOR COLLINS ENGINEERS

KE235325

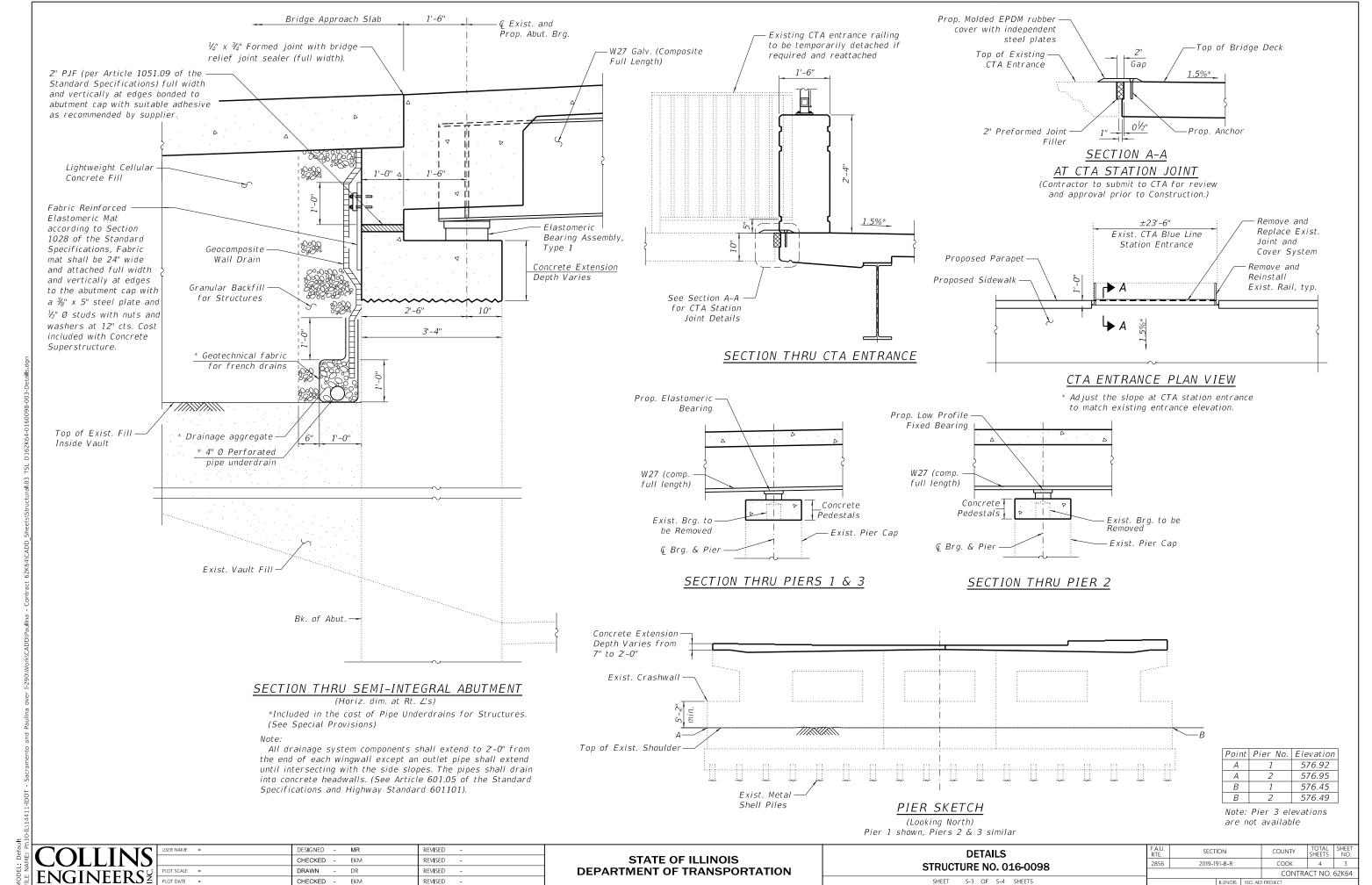


APPENDIX B





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