

# **Structure Geotechnical Report**

(In-House)

**US 52 over Elkhorn Creek**

**Bridge Replacement**

Proposed Structure Number: 071-0098

Existing Structure Number: 071-0070

Contract Number: 64H57

Route: US-50

Section: 16BR-1

County: Ogle

Project Number: P-92-029-12

Prepared For: Bridge Planning and Design Units

Prepared By: Foundations and Geotechnical Unit

Suhail Ibrahim

217-557-8239

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Report Date: 3/22/2017

## **1.0 Scope of Work**

This project consists of replacing the existing bridge carrying U.S. 52 over Elkhorn Creek. The site is located immediately Southeast of Brookville in Western Ogle County (see Site Location Map in Appendix A).

The existing structure is a 3-span bridge (SN: 071-0070) that is 124'-5" back to back abutments. It consists of stub abutments with two rows of metal shell piles (the front row is battered) and pile bent piers with HP 10X42 steel piles driven to rock.

The existing structure will be replaced by a proposed 3-span bridge with a total back to back length of 225', utilizing integral abutments. All substructures will be supported by H-piles driven to rock.

The proposed structure (SN: 071-0098) will be designed with the 2014 AASHTO LRFD Bridge Design Specifications, 7<sup>th</sup> Edition with 2015 and 2016 Interims. Preliminary factored loadings are as follows:

Estimated Factored Substructure Loads (kips)	W. Abut	Pier 1	Pier 2	E. Abut
	847	1540	1644	847

## **2.0 Subsurface Data**

Two borings were drilled in January and February of 2012 for subsurface exploration. Boring B-1, drilled near the West Abutment, is only 44 feet deep and does not reach rock. Boring B-2, drilled near the East Abutment, is 52 feet deep and shows a bedrock elevation of 711.80. Note that only one of the 2012 borings extends into rock. These borings shall be referenced as Boring B-1(2012) and Boring B-2(2012). To better ascertain the top of rock across the site, we have also employed the use of the two older borings that were drilled in November of 1979 for the existing bridge. Both borings extend into rock. These borings shall be referenced as Boring B-1(1979) and Boring B-2(1979).

Please see Appendix C for the Subsurface Data Plot and Appendix D for the borings. In addition, existing pile driving records are included in Appendix E.

## **3.0 Geotechnical Evaluation and Recommendation**

### **3.1 Settlement**

Approximately 2 feet of new fill will be required at the proposed West Abutment and 1.5 feet at the proposed East Abutment. The resulting settlement will be less than 0.4 inches in both abutments; therefore, no downdrag forces are anticipated at the abutments. See Appendix G for results.

## 3.2 Slope Stability Analysis

Based on our analysis, the slope stability is satisfactory. See Appendix G for results.

## 3.3 Scour

The raw scour depths from the 2016 Hydraulic Report are in the table below:

	Contraction Scour (ft)	Pier Scour (ft)	Total (ft)
<b>Q100</b>	13	5	18
<b>Q200</b>	15	5	20

Based on the abutments being protected with riprap in accordance with the ABD memo 14.2 and the raw scour depths being adjusted at the piers based on boring data, The Design Scour Elevations Table is as follows:

Event/Limit State	Design Scour Elevations (ft.)				Item 113
	W. Abut	Pier 1	Pier 2	E. Abut	
Q100	758.65	734.80	728.40	759.05	5
Q200	758.65	732.80	726.40	759.05	
Design	758.65	734.80	728.40	759.05	
Check	758.65	732.80	726.40	759.05	

## 3.4 Seismic Considerations

The LRFD seismic data for the structure is as follows:

Seismic Performance Zone (SPZ) = 1  
Design Spectral Acceleration at 1.0 sec. (SD1) = 0.057g  
Design Spectral Acceleration at 0.2 sec. (SDS) = 0.097g  
Soil Site Class = C

The above data is based on latitude= 42.047754, and longitude =-89.678776.

Because the site is located in SPZ 1, no liquefaction analysis is required.

## 4.0 Foundation Recommendations

### Abutments:

H-piles driven to their maximum nominal bearing in rock are recommended as the foundation choice for the abutments. Integral Abutments are feasible for this project and are the preferred option. As per the ABD memo 12.3, feasible H-pile types for the abutment are HP10X42 and larger. Please see Pile Design Tables on page 4 for Abutment piles.

Metal shell piles were not considered as a foundation type for the abutments due to the presence of rock relatively close to the surface.

**Piers:**

H-piles driven to their maximum nominal bearing in rock are recommended as the foundation choice for the piers; scour has been taken into consideration for their design. Please see Pile Design Tables on page 5 for Pier piles.

Metal shell piles were not considered as a foundation type for the piers due to the presence of rock relatively close to the surface.

Drilled shafts are a feasible foundation option at the piers, however, more rock cores will be required in order to provide any drilled shaft foundation design recommendations.

## Pile Design Tables for Abutments

### West Abutment (B-1 (2012) data) Pile cutoff elevation 760.65

Pile type	Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Pile Length (ft)
<b>HP 12 X 53</b>	419	230	52
<b>HP 12 X 74</b>	589	324	53
<b>HP 12 X 84</b>	664	365	53
<b>HP 14 X 73</b>	578	318	53
<b>HP 14 X 89</b>	705	388	53
<b>HP 14 X 102</b>	810	445	53
<b>HP 14 X 117</b>	929	511	54

### East Abutment (B-2 (2012) data) Pile cutoff elevation 761.05

Pile type	Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Pile Length (ft)
<b>HP 12 X 53</b>	419	230	51
<b>HP 12 X 74</b>	589	324	52
<b>HP 12 X 84</b>	664	365	53
<b>HP 14 X 73</b>	578	318	53
<b>HP 14 X 89</b>	705	388	53
<b>HP 14 X 102</b>	810	445	53
<b>HP 14 X 117</b>	929	511	54

## Pile Design Tables for Piers

### Pier 1 (B-2 (1979) data) Pile cutoff elevation 761.68

Pile type	Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Pile Length (ft)
<b>HP 12 X 53</b>	419	200	48
<b>HP 12 X 74</b>	589	293	49
<b>HP 12 X 84</b>	664	334	49
<b>HP 14 X 73</b>	578	282	50
<b>HP 14 X 89</b>	705	352	50
<b>HP 14 X 102</b>	810	409	50
<b>HP 14 X 117</b>	929	474	51

### Pier 2 (B-1 (1979) data) Pile cutoff elevation 761.84

Pile type	Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Pile Length (ft)
<b>HP 12 X 53</b>	419	202	58
<b>HP 12 X 74</b>	589	296	59
<b>HP 12 X 84</b>	664	336	60
<b>HP 14 X 73</b>	578	285	60
<b>HP 14 X 89</b>	705	355	60
<b>HP 14 X 102</b>	810	413	60
<b>HP 14 X 117</b>	929	477	61

**Pile Shoes:**

Pile shoes are recommended for all piles since they are to be driven into hard rock.

**Test Piles:**

We recommend one test pile at each one of the four elements of the structure.

**Lateral Load Analysis**

No formal lateral load analyses were required. Based on the structure being integral with fixed piers, along with what appears to be sufficient pier pile embedment remaining upon a scour event occurring (thereby providing fixity) and the structure being located in SPZ 1, lateral loading should not be a concern.

## **5.0 Construction Considerations**

### **5.1 Cofferdam and Sealcoat**

A Cofferdam with Sealcoat will be required at Pier 2. Therefore, a Cofferdam Type 2 with Sealcoat needs to be indicated on the plans. Pier 1 will not require a Cofferdam.

### **5.2 Temporary Soil Retention**

The TSL is showing that the traffic will be detoured; therefore no soil retention will be needed for Stage Construction.

## **6.0 Appendices**

Appendix A: Location Map

Appendix B: Preliminary Type, Size, and Location

Appendix C: Subsurface Data Plot

Appendix D: Boring Logs

Appendix E: Existing Pile Driving Records (1983)

Appendix F: Existing General Plan and Elevation

Appendix G: Spreadsheets (Settlement, Seismic Site Class Determination, and Estimating Pile Length) and Computer Outputs (*SLIDE* Slope Stability)

## **Appendix A**

### **Location map**



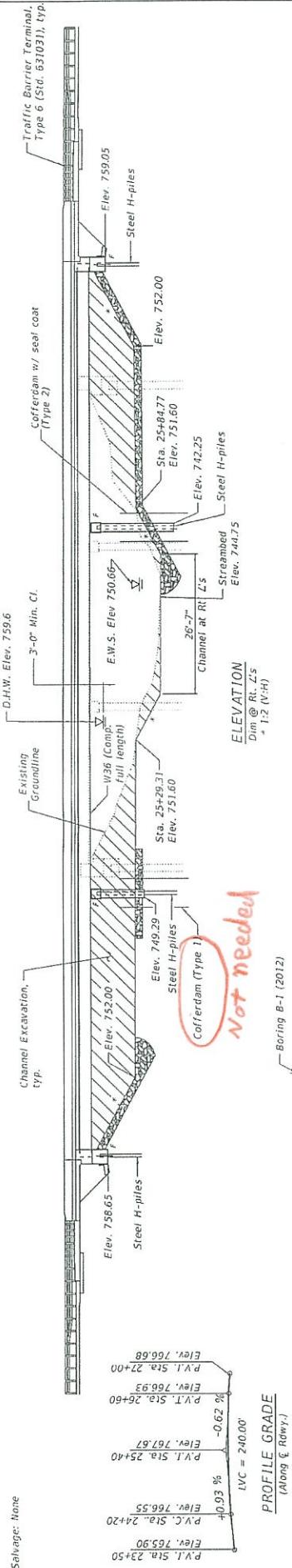
## **Appendix B**

### **Preliminary Type, Size, and Location**

Bench mark: Chiseled "T" in top of NE wingwall. Station 26+11.8640/17.1214 Lt. Elevation = 764.64.

**Existing Structure:** Structure No. 071-070 is a 3 span PPC deck beam bridge, originally built in 1993 as F.A.S. 2079 (US Rule 52), Section 6-BR at station 97+150.04. Both abutments are open stay abutments supported on concrete piles and the two bent type piers are supported on H-piles. The back to back abutment length is 124'-4¾", the out to out deck width is 31'-2" with a clear roadway width of 28'-6" and a 20° right-forward skew. Existing structure is to be demolished and replaced. Traffic will be detoured.

CONTINUOUS



PROFILE GRADE  
*(Along & Rowby.)*

DESIGN SPECIFICATIONS

2014 AASHTO LRFD Bridge Design  
Specifications, 7th Edition with 2015 and 2016 Interims

<u>DESIGN STRESSES</u>	<u>FIELD UNITS</u>
$f_c = 3,500 \text{ psi}$	
$f_c = 4,000 \text{ psi}$ (Superstructure Concrete)	
$f_c = 60,000 \text{ psi}$ (Reinforcement)	

F.A.S. Rte. 2079 -U.S. Rte. 52

SEISMIC DATA

Seismic Performance Zone ( $SPZ_1$ ) =  $SPZ_1$   
 Design Spectral Acceleration at 1.0 sec. ( $SDI_1$ ) = 0.0579  
 Design Spectral Acceleration at 0.2 sec. ( $SDS_1$ ) = 0.0979  
 $S_{0.2} / S_{1.0}$  Class = C

F.A.S. A/E. 2019 = SEC. 18BA-1

STATION 25+36.51  
STRUCTURE NO. 071-0098

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卷之三

TOTAL SHEET

CONTRACT NO.

卷之三

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

PLAN

225'-1" Back-to-back Abutments

GENERAL PLAN AND ELEVATION

U.S. ROUTE 52 OVER

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ELKHORN CREEK

RTE 2079 - SEC 16

OGI/E COUNTY

STATION 25436 51

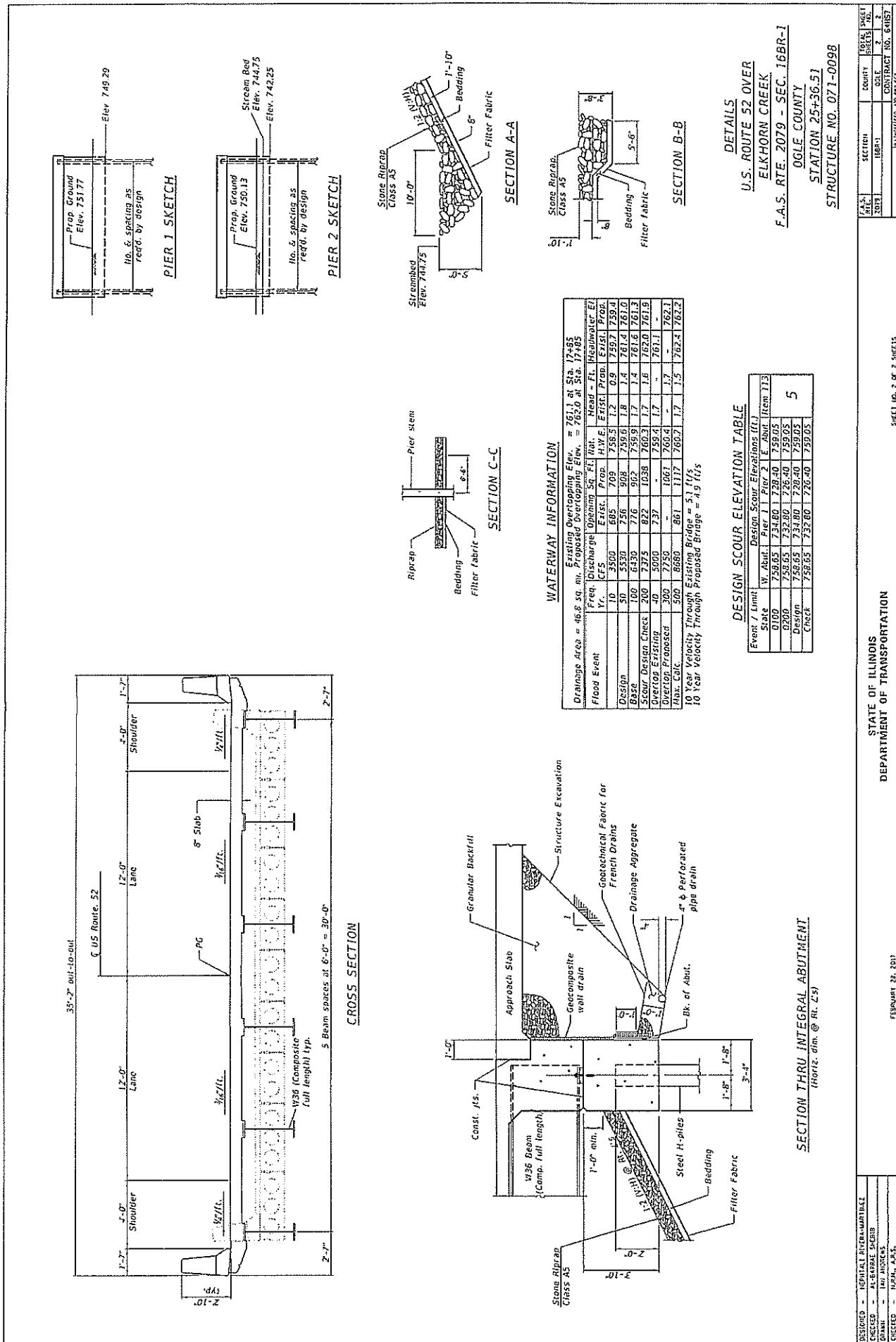
STRUCTURE AND

WECI 06.01-00

SECTION | COUNTY |

CONTRACT

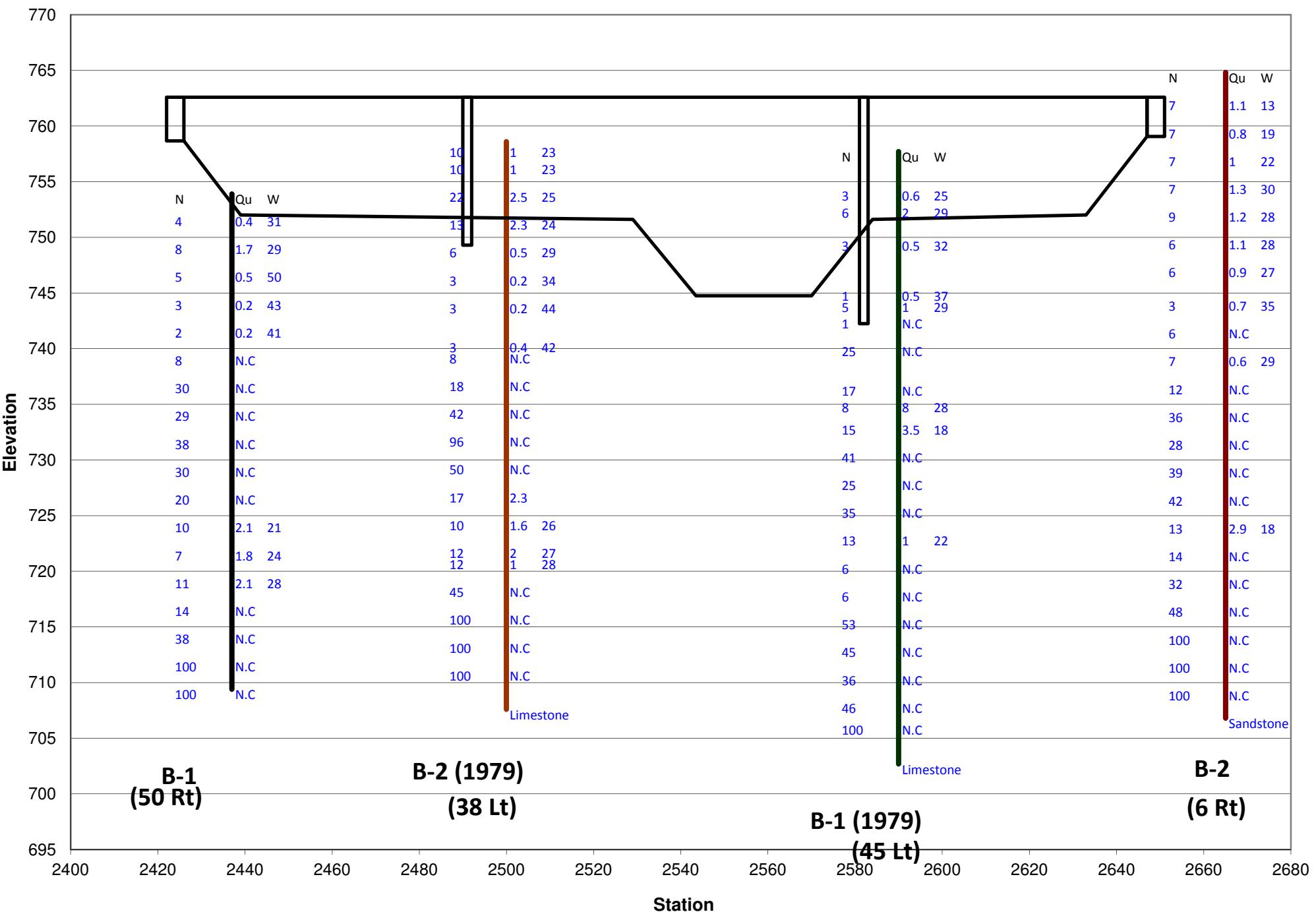
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# **Appendix C**

## **Subsurface Data Plot**

071-0098



# **Appendix D**

## **Boring logs**

### **(Including 2012 Borings and Existing 1979 Borings)**



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# SOIL BORING LOG

Page 1 of 2

Date 2/17/12

ROUTE US 52 DESCRIPTION 071-0070 P92-029-12 Bridge, US 52, 5 m. S. of IL 64 over Elkhorn Creek LOGGED BY W. Garza

**SECTION** \_\_\_\_\_ **LOCATION** Brookville Twp. - 27NW, SEC., TWP. 24N, RNG. 7E

COUNTY      Ogle      DRILLING METHOD      Hollow Stem Auger      HAMMER TYPE      CME-45 Automatic

COUNTY Ogle DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer). The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206).

BBS, from 137 (Rev. 8-99)



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## SOIL BORING LOG

Page 2 of 2

Date 2/17/12

ROUTE US 52 DESCRIPTION 071-0070 P92-029-12 Bridge, US 52, .5 m. S. of IL 64 over Elkhorn Creek LOGGED BY W. Garza

SECTION \_\_\_\_\_ LOCATION Brookville Twp. - 27NW, SEC. , TWP. 24N, RNG. 7E

COUNTY Ogle DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

STRUCT. NO.	071-0070	D	B	U	M	Surface Water Elev.	ft
Station		E	L	C	O	Stream Bed Elev.	ft
BORING NO.	B-1	P	O	S	I	Groundwater Elev.:	
Station	970+38	T	W	Qu	S	First Encounter	739.4 ft <input checked="" type="checkbox"/>
Offset	50.00ft Lt CL	H	S			Upon Completion	Wash ft
Ground Surface Elev.	753.9 ft	(ft)	(16")	(tsf)	(%)	After Hrs.	ft
Wash			100/7'				
VERY DENSE white fine SAND (continued)	712.90						
Wash			100/3'				
VERY DENSE white fine SAND							
End of Boring	709.90						
		-45					
		-50					
		-55					
		-60					

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)



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# SOIL BORING LOG

Page 1 of 2

Date 3/5/12

ROUTE US 52 DESCRIPTION 071-0070 P92-029-12 Bridge, US 52, .5 m. S. of IL 64 over Elkhorn Creek LOGGED BY W. Garza

SECTION LOCATION Brookville Twp. - 27NW, SEC. , TWP. 24N, RNG. 7E

COUNTY Ogle DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

STRUCT. NO.	071-0070				D	B	U	M	Surface Water Elev. _____ ft				D	B	U	M
Station					E	L	C	O	Stream Bed Elev. _____ ft	E	L	C	O			
BORING NO.	B-2				P	O	S	I	Groundwater Elev.: _____ ft	P	O	S	I			
Station	972+57				T	W	Qu	S	First Encounter 742.3 ft ▼	T	W	Qu	S			
Offset	6.00ft R1 CL				H	S			Upon Completion Wash ft	H	S	Qu	S			
Ground Surface Elev.	764.81 ft				(ft)	(16")	(tsf)	(%)	After _____ Hrs. ft	(ft)	(16")	(tsf)	(%)			
STIFF gray LOAM									LOOSE gray moist fine SAND					2		
														2		
														4		
														742.81		
MEDIUM gray SILTY CLAY LOAM		762.31			3				MEDIUM gray SILTY LOAM with SAND lens					▼		
					3		0.8	19						1		
		760.81			4		P							2	0.6	29
														5	P	
STIFF gray SANDY LOAM		-5			1				MEDIUM tan SANDY GRAVEL					-25		
					3		1.0	22						6		
		758.31			4		P							4		
														8		
STIFF gray SILTY LOAM					2				DENSE tan weathered LIMESTONE					740.31		
					3		1.3	30						13		
		755.81			4		B							16		
														20		
STIFF gray SILTY LOAM		-10			2				MEDIUM tan weathered LIMESTONE					-30		
					4		1.2	28						17		
		753.31			5		B							14		
														14		
STIFF gray SILTY CLAY LOAM					2				DENSE tan weathered LIMESTONE					-35		
					2		1.1							16		
		750.81			4		P							20		
														19		
MEDIUM gray SILTY LOAM with ORGANICS		-15			2				DENSE tan weathered LIMESTONE					-35		
					3		0.9	27						20		
		748.31			3		B							20		
														22		
MEDIUM gray SILTY LOAM with SAND lens					2				VERY STIFF gray CLAY LOAM TILL					727.81		
					1		0.7	35						4		
		745.31			2		B							5	2.9	18
														8	B	
					-20									-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)



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# SOIL BORING LOG

Page 2 of 2

Date 3/5/12

ROUTE US 52 DESCRIPTION 071-0070 P92-029-12 Bridge, US 52, .5 m. S. of IL 64 over Elkhorn Creek LOGGED BY W. Garza

SECTION \_\_\_\_\_ LOCATION Brookville Twp. - 27NW, SEC., TWP. 24N, RNG. 7E

COUNTY Ogle DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

STRUCT. NO.	071-0070	D	B	U	M	Surface Water Elev.	ft
Station		E	L	C	O	Stream Bed Elev.	ft
BORING NO.	B-2	P	O	S	I	Groundwater Elev.:	
Station	972+57	T	W	Qu	S	First Encounter	742.3 ft <input checked="" type="checkbox"/>
Offset	6.00ft Rt CL	H	S			Upon Completion	Wash ft
Ground Surface Elev.	764.81 ft	(ft)	(1/6")	(tsf)	(%)	After Hrs.	ft
MEDIUM tan fine SAND							
			9				
			10				
			4				
			723.31				
Wash							
DENSE tan fine SAND							
			11				
			15				
			17				
			720.81				
DENSE tan fine SAND							
			10				
			14				
			34				
			718.31				
VERY DENSE tan fine SAND							
			100/9'				
			715.81				
Wash							
VERY DENSE off-white fine SAND							
			100/3'				
			713.31				
VERY DENSE white fine SAND							
	711.81		100/4'				
Borehole continued with rock coring.							
			-55				
			-60				

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)



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## ROCK CORE LOG

Page 1 of 1

Date 3/5/12

ROUTE US 52 DESCRIPTION 071-0070 P92-029-12 Bridge, US 52, .5 m. S. of IL 64 over Elkhorn Creek LOGGED BY W. Garza

SECTION LOCATION Brookville Twp. - 27NW, SEC. , TWP. 24N, RNG. 7E

COUNTY	Ogle	CORING METHOD	R	E	R	CORE	S	T
STRUCT. NO.	071-0070	CORING BARREL TYPE & SIZE	D	C	T	R	E	N
Station		Core Diameter 2 in	E	O	I	M	E	G
BORING NO.	B-2	Top of Rock Elev. 717.31 ft	P	R	D	E	T	H
Station	972+57	Begin Core Elev. 711.81 ft	T	E	R	Y		
Offset	6.00ft Rt CL		H	(#)	(%)	(%)	(min/ft)	(tsf)
Ground Surface Elev.	764.81 ft							
Sandstone: tan-white, fine to medium grained, crumbly and soft, mostly washed out, 711.81 no testable segments retrieved.					1	40	0	1.6
					-55			
					-50			
					-45			
					-40			
					-35			
					-30			
					-25			
					-20			
					-15			
					-10			
					-5			
					706.81			
Sandstone: as above.					2	30	0	1.4
					-60			
					-55			
					-50			
					-45			
					-40			
					-35			
					-30			
					-25			
					-20			
					-15			
					-10			
					701.81			
End of Boring					-65			
					-60			
					-55			
					-50			
					-45			
					-40			
					-35			
					-30			
					-25			
					-20			
					-15			
					-10			

Color pictures of the cores \_\_\_\_\_

Cores will be stored for examination until \_\_\_\_\_

The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)



NW<sub>4</sub>, Section 27, T 24 N, R 7 E; 4th PM

24 N., R 7 E.; 4th PM

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Near Ctr. W $\frac{1}{2}$ , SE $\frac{1}{4}$ , NW $\frac{1}{4}$ ,  
27-24N-7E

## **Bridge Foundation Boring Log**

Sh. 1 of 2 Sh.

PROJECT P-92-061-78 BRIDGE Elkhorn Creek Date 11-8-79

ROUTE PAS-2079 (U.S.52) 071-0032 Bored By Crofton & Wildman

SEC 16-BR STA 971+50 (ins. to SE) Checked By R. Wildman

N-Standard Penetration Test-  
Blows per foot to drive 2"  
O.D. Split Spoon Sampler 12" with  
140 No. hammer falling 30".

## Qu-Unconfined Compressive Strength - t/sf

w - Water Content - percentage  
of oven dry weight-%.

Type failure:  
B - Bulge Failure  
S - Shear Failure  
E - Estimated Value  
P - Penetrometer

**BRIDGE FOUNDATION BORING LOG**

P-92-061-78

FAS 2079

16BR

Ogle County

Boring B-7 1

	Elevation	N	Qntr/s.t.	w (%)		Elevation	N	Qntr/s.t.	w (%)
Dense Sand & Gravel Coarse Sand Predominant	-45					-75			
Same As Above	-46	36				-80			
Very Dense Limestone with Gravel	-50					-85			
Auger Refusal	-55	100	6" pene.			-90			
	-60					-95			
	-65					-100			
	-70					-105			



Bridge Foundation  
Boring Log

Sh.1 of 2 Sh.

PROJECT P-92-061-78 BRIDGE Elkhorn Creek Date 11-15-79  
 ROUTE FAS 2079 (U.S.52) 071-0032 Bored By R. Wildman  
 SEC. 16BR STA. 971+50 Checked By R. Wildman

COUNTY	Elevation	Surface Water El.				Elevation	N	Qu t/s.f.	W (%)
		Groundwater El. at Completion	Wash	After Hours					
Ogle									
Boring No. B-2									
Station 970+92									
Offset 38'L									
Ground Surface (758.6±)	262.1	0							
Medium Silty Clay Loam Brown	10	1.0	23	Dense Sand & Gravel		42			
Very Stiff, Silty Clay Black	22	2.5	25	Very Dense Limestone & Sand & Gravel		96			
Same As Above	13	2.3	24	Dense Limestone - Yellow		50			
Soft Silty Clay Gray	6	0.5	29	Very Stiff Silt, Gray to Brown Mottled		17	2.3		
Very Soft Silty Clay Loam, Gray with Sand Lenses	3	0.2	34	Stiff Silty Clay Gray		10	1.6	26	
Very Soft Silt Gray, Sand Lenses	3	0.2	44	Very Stiff Silty Clay Gray		12	2.0	27	
Soft Silt Gray with Gravel	3	0.4	42	Stiff, Same As Above		12	1.0	28	
Loose Sand & Gravel Yellow-Brown	8			Loose Sand Yellow Coarse		45			
Medium Sand & Gravel Limestone with Granite Particles Also	18			Dense Highly Fractured Limestone with Sand Coarse		100	6"	bene	
N-Standard Penetration Test- Blows per foot to drive 2" O.D. Split Spoon Sampler 12" with 140 lb hammer falling 30"				Very Dense Fractured Limestone with Gray Clay Matrix					
Qu-Unconfined Compressive Strength - t/sf				Type failure					
w - Water Content - percentage of oven dry weight-%				B - Bulge Failure					
				S - Shear Failure					
				E - Estimated Value					
				P - Penetrometer					

N-Standard Penetration Test- Blows per foot to drive 2" O.D. Split Spoon Sampler 12" with 140 lb hammer falling 30"

Qu-Unconfined Compressive Strength - t/sf

w - Water Content - percentage of oven dry weight-%

Type failure

B - Bulge Failure

S - Shear Failure

E - Estimated Value

P - Penetrometer

## BRIDGE FOUNDATION BORING LOG

FAS 2079 16-BR Ogle County P-92-061-78 Boring B-2	Elevation	%	Qu t/l.f.	W (%)	Elevation	%	Qu t/l.f.	W (%)
	-45							
Very Dense Sand White Medium	100	6"	pene.					
Same As Above with Limestone Gravel	100	6"	pene.					
End of Boring	-50							
	-55							
	-60							
	-65							
	-70							
	-75							
	-80							
	-85							
	-90							
	-95							
	-100							

## **Appendix E**

### **Existing Pile Driving Records**

## PILING DIAGRAM

County Ogle

Section 16 BR

Route FAS-2079

**District 2**

Contract No. 36446

Job No. C92-110-83

Project BR-2-2079 (1oz)

Station 972 + 12.20 (EAST ABUT)

Type Of Piling METAL SHELL

Plan Length 35'

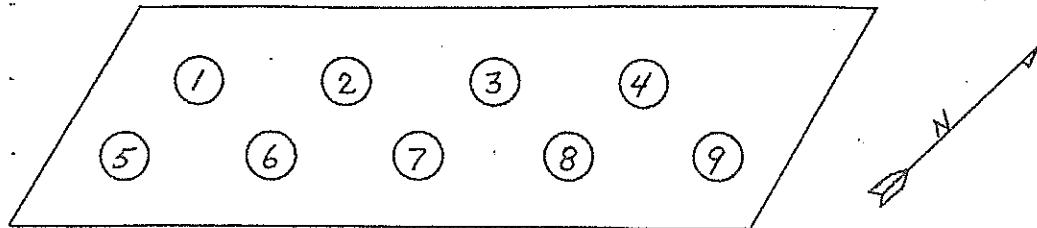
Ordered Length 33'

Date Driven 9-6-83

Hammer Make & Model DELMAG 15

Test Pile Length \_\_\_\_\_ No. \_\_\_\_\_

Location \_\_\_\_\_  
Page \_\_\_\_\_ of \_\_\_\_\_



## PILING DIAGRAM

County Ogle

Section 16 BR

Route FAS - 2079

District 2

District -  
Contract No. 36446

Job No. C92-110-83

Project BR-2-2079 (102)

Station 971 + 30.14 (Pier #1)

Type Of Piling Steel HP 10 x 42

Plan Length 57

Ordered Length 5/

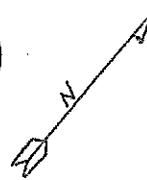
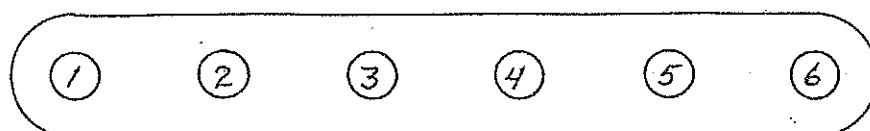
Date Driven 8-27-83

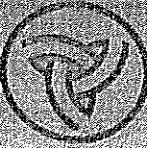
Hammer Make & Model Delmag 15

Test Pile Length \_\_\_\_\_ No. \_\_\_\_\_

Location \_\_\_\_\_

Res. Eng. J. Westervelt





# Illinois Department of Transportation

## Memorandum

To: Carl Thunman  
From: Ralph C. Wehner  
Subject: Piling Diagrams  
Date: August 9, 1984

ROUTE FAS 2079  
SECTION 16-BR  
COUNTY Ogle  
PROJECT BR-S-2079(102)  
JOB NO. C-92-110-83  
CONTRACT NO. 36446  
CONTRACTOR Belvidere Construction Company

RECEIVED  
BUREAU OF BRIDGES  
AND STRUCTURES

AUG 13 1984

ITR  
RPH  
OMI  
RGH  
PPM  
INFO.

DISC.  
Sgn.  
FAC  
CIRC.

## PILING DIAGRAM

County Ogle

Section 16 BR

Route FAS - 2079

**District**

Contract No. 36446

Job No. C92-110-83

Project BR-2-2079 (102)

Station 970 + 87, 74 (West Abut.)

Type Of Piling METAL SHELL

Plan Length 30

Ordered Length 33'

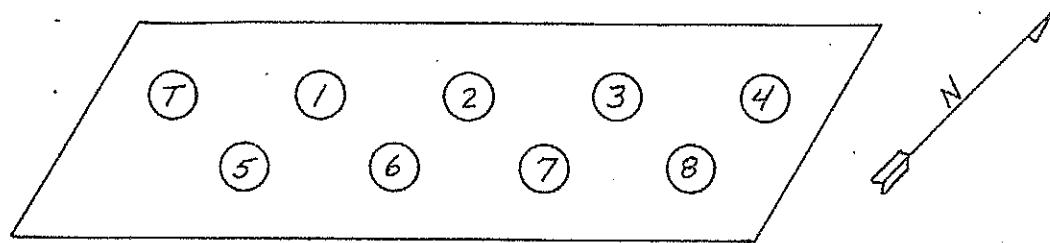
Date Driven 9-12-83

Hammer Make & Model DELATAG 15

Test Ple Length 30.67 No. T

Location 970 + 87.74

Res. Eng. J. Westervelt



## PILEING DIAGRAM

Section 16 BR

Section 16, BR

Route FAS-2079

**District Z**

Contract No. 36446

Job No. C92-110-83

Project B.B. 2.2078 (102)

Project BR-2-2079 (102)

Station 971 + 69.93 (Pier # 2)

Type Of Piling Steel HP 10 x 42

Plan Length 51 ft

Ordered Length 51 ft

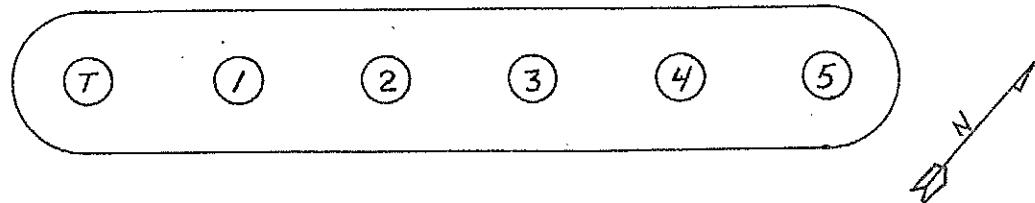
Date Driven 8-25-83

Hammer Make & Model DeWalt 15

Test Pile Length 48.66 ft

Location 971 + 69.93 16° 3" LT

Res. Eng. J. Westervelt

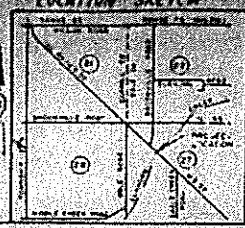


## **Appendix F**

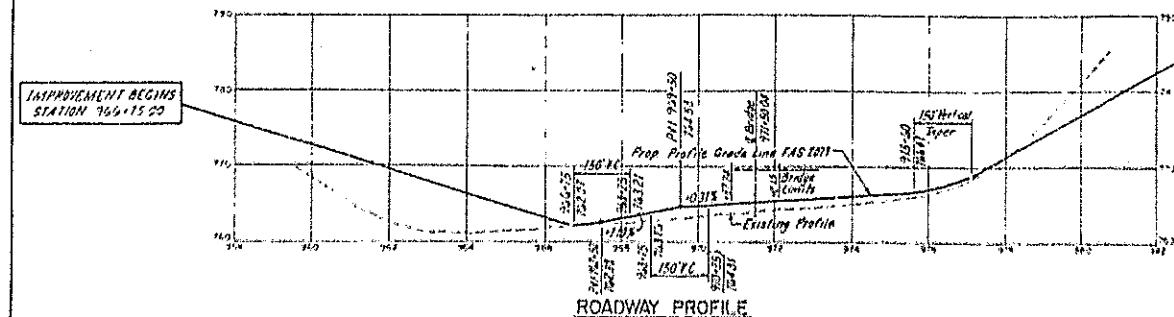
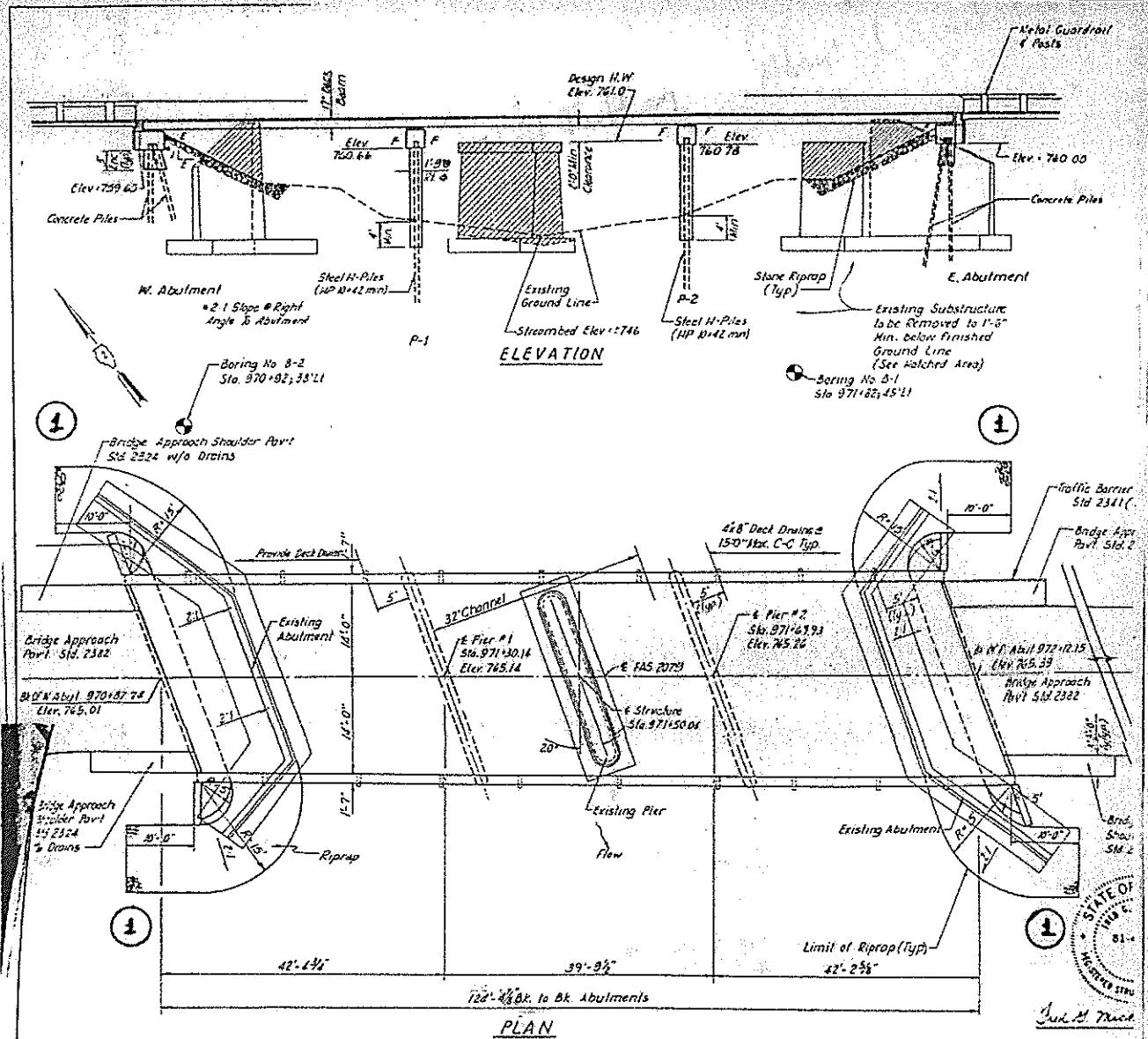
### **Existing General Plan and Elevation**

Flow	Ft/s	Q CFS	Open Channel		H.W.		Impermeable		Permeable	
			Elev	Prop	Elev	Prop	Elev	Prop	Elev	Prop
Design	30	5440	660	862	761.0	2.40	763.4	762.80		
Safe	100	3070	660	939	761.6	2.34	763.94	763.51		
Overshooting	80	6735	660	921	761.4	1.81			763.21	
Max. Calc.	300									

### LOCATION SKETCH



GENERAL



PROPERTY OWNER  
① DAVID L. INTYRE  
BOX 85  
POLO, IL

(015) 946-2695

# **Appendix G**

## **Spreadsheets and Computer Outputs**

(Settlement, Seismic Site Class Determination, Estimating  
Pile Length, and *SLIDE* Slope Stability)

# COHESIVE SOIL SETTLEMENT ESTIMATE

I.D.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

Modified on 12/9/14

LOCATION AND BORING USED ===== [East Abutment B-2 \(2012\)](#)

TYPE OF SURCHARGE ===== 1 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)

DEPTH TO WATER TABLE (below top of existing embankment) ===

7 FT

NEW EMBANKMENT:

NEW EMBANKMENT FILL UNIT WEIGHT ===== 120 PCF

NEW EMBANKMENT FILL HEIGHT ===== 1.5 FT

PROPOSED WIDTH AT TOP ===== 32 FT

PROPOSED WIDTH AT BOTTOM ===== 38 FT (which is a 2.0:1 slope)

## ASSUMPTIONS:

Soil Deposit is Normally Consolidated

Cohesive Layers are Saturated

Soils have a Low Sensitivity

Liquid Limit (LL)=Moist. Content (MC%)

Initial Void Ratio ( $E_0$ )=2.7\*(MC%)/100

Comp. Index ( $C_c$ )=0.009\*(LL-10)

Neglecting Granular & Secondary Settlem't

EXISTING EMBANKMENT (IF ANY):

EXISTING EMBANKMENT UNIT WEIGHT ===== PCF

EXISTING EMBANKMENT HEIGHT ===== FT

EXISTING WIDTH AT TOP ===== FT

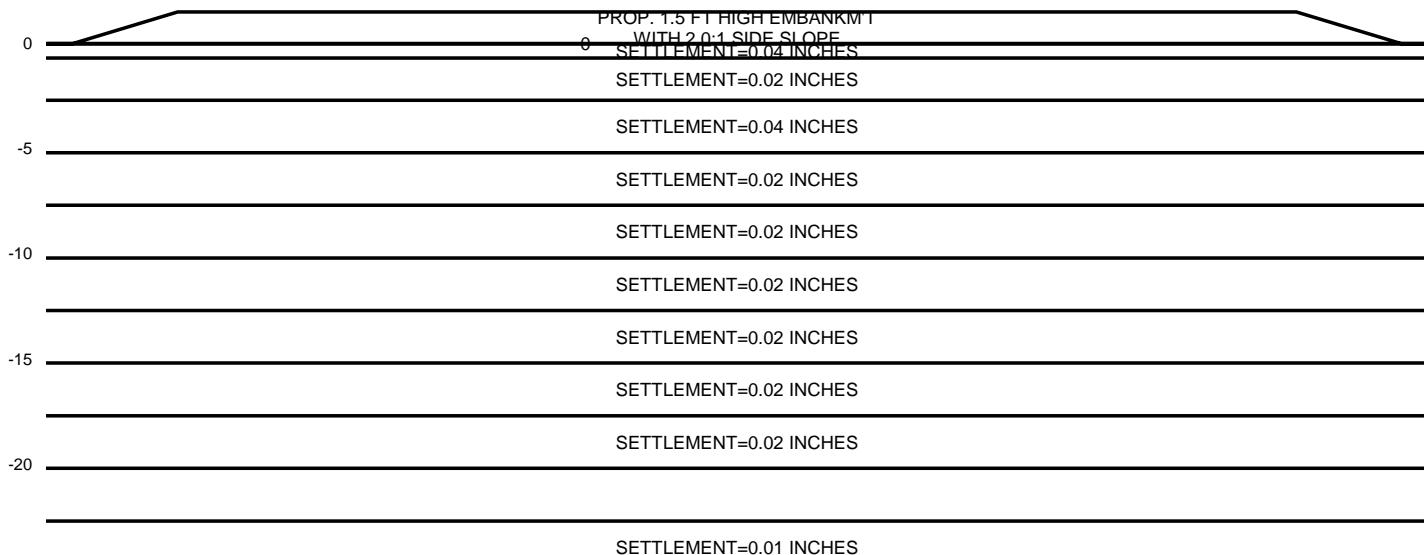
EXISTING WIDTH AT BASE ===== FT (which is a 0.0:1 slope)

LAYER THICK	TOTAL UNIT WT. (PCF)	UNCONF. COMP. STRENGTH (Qu) (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
0.7	120	1.00	15	0.041	0.173	0.405	0.045	0.200	0.04
2.0	120	1.10	13	0.203	0.151	0.351	0.027	0.184	0.02
2.5	120	0.80	19	0.473	0.127	0.513	0.081	0.242	0.04
2.5	120	1.00	22	0.773	0.113	0.594	0.108	0.200	0.02
2.5	120	1.30	30	0.952	0.105	0.810	0.180	0.160	0.02
2.5	120	1.20	28	1.096	0.098	0.756	0.162	0.171	0.02
2.5	120	1.10	28	1.240	0.091	0.756	0.162	0.184	0.02
2.5	120	0.90	27	1.384	0.086	0.729	0.153	0.219	0.02
2.5	120	0.70	35	1.528	0.080	0.945	0.225	0.271	0.02
2.5	120	0.00		1.672	0.075			1.000	
2.5	120	0.60	29	1.816	0.071	0.783	0.171	0.309	Granular 0.01

**TOTAL SETTLEMENT UNDER CENTER OF BRIDGE CONE = 0.23 IN.**

## EMBANKMENT AND SOIL PROFILE

5



-30

# COHESIVE SOIL SETTLEMENT ESTIMATE

I.D.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

Modified on 12/9/14

LOCATION AND BORING USED ===== West Abutment/ B-1 (2012)

TYPE OF SURCHARGE ===== 1 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)

DEPTH TO WATER TABLE (below top of existing embankment) == 19 FT

**NEW EMBANKMENT:**

NEW EMBANKMENT FILL UNIT WEIGHT ===== 120 PCF

NEW EMBANKMENT FILL HEIGHT ===== 2 FT

PROPOSED WIDTH AT TOP ===== 32 FT

PROPOSED WIDTH AT BOTTOM ===== 40 FT (which is a 2.0:1 slope)

**ASSUMPTIONS:**

Soil Deposit is Normally Consolidated

Cohesive Layers are Saturated

Soils have a Low Sensitivity

Liquid Limit (LL)=Moist. Content (MC%)

Initial Void Ratio ( $E_0$ )=2.7\*(MC%)/100

Comp. Index ( $C_c$ )=0.009\*(LL-10)

Neglecting Granular & Secondary Settlem't

**EXISTING EMBANKMENT (IF ANY):**

EXISTING EMBANKMENT UNIT WEIGHT ===== PCF

EXISTING EMBANKMENT HEIGHT ===== FT

EXISTING WIDTH AT TOP ===== FT

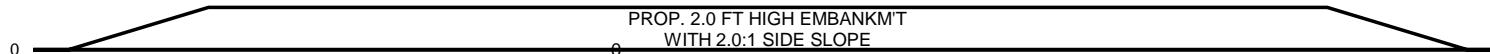
EXISTING WIDTH AT BASE ===== FT (which is a 0.0:1 slope)

LAYER THICK	TOTAL UNIT WT. (PCF)	UNCONF. COMP. STRENGTH (Qu) (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
10.9	120	1.00	15	0.654	0.167	0.405	0.045	0.200	0.08
2.0	120	0.40	31	1.428	0.135	0.837	0.189	0.436	0.04
2.5	120	1.70	29	1.698	0.127	0.783	0.171	0.127	0.01
2.5	120	0.50	50	1.998	0.119	1.350	0.360	0.361	0.04
2.5	120	0.20	43	2.289	0.111	1.161	0.297	0.700	0.06
2.5	120	0.20	41	2.433	0.104	1.107	0.279	0.700	0.05

**TOTAL SETTLEMENT UNDER CENTER OF BRIDGE CONE = 0.29 IN.**

**EMBANKMENT AND SOIL PROFILE**

5



-5

SETTLEMENT=0.08 INCHES

-10

SETTLEMENT=0.04 INCHES

-15

SETTLEMENT=0.01 INCHES

-20

SETTLEMENT=0.04 INCHES

SETTLEMENT=0.06 INCHES

SETTLEMENT=0.05 INCHES

-25

TOTAL SETTLEMENT=0.29 INCHES

-30

### **Global Site Class Definition: Substructures 1 through 4**

N (bar): 28 (Blows/ft.) Soil Site Class D  
 N<sub>ch</sub> (bar): 57 (Blows/ft.) Soil Site Class C <----Controls  
 s<sub>u</sub> (bar): 2.91 (ksf) Soil Site Class C

# IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

I.D.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

Modified 10/18/2011

SUBSTRUCTURE=====		east abutment	MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses				
REFERENCE BORING =====		B-2	LRFD	Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
PILE CUTOFF ELEV.	761.00	ft	759.00	ft	578 KIPS	578 KIPS	318 KIPS
GROUND SURFACE ELEV. AGAINST PILE DURING DRILLING	None		424.00	ft			51 FT.
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD)	None		434.00	ft			
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====							
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====							

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1245 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)==== 34.00 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 292.94 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 109.85 KIPS

PILE TYPE AND SIZE ===== Steel HP 14 X 73

Plugged Pile Perimeter===== 4.700 FT. Unplugged Pile Perimeter===== 6.975 FT.

Plugged Pile End Bearing Area===== 1.379 SQFT. Unplugged Pile End Bearing Area===== 0.149 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
757.81	1.19	1.30			4.9	30.0	7.2	9.9	10	0	0	0	5	3	
755.31	2.50	1.30			10.2	25.1	38.3	15.2	2.7	24.9	25	0	0	14	6
752.81	2.50	1.20			9.6	23.2	46.0	14.3	2.5	39.0	39	0	0	21	8
750.31	2.50	1.10			9.0	21.3	51.1	13.4	2.3	51.9	51	0	0	28	11
747.81	2.50	0.90			7.7	17.4	54.9	11.4	1.9	62.9	55	0	0	30	13
744.81	3.00	0.70			7.4	13.5	69.4	11.0	1.5	74.6	69	0	0	38	16
742.31	2.50		6	Fine Sand	1.2	20.6	61.6	1.8	2.2	75.5	62	0	0	34	19
739.81	2.50	0.60			5.4	11.6	96.6	8.0	1.2	86.7	87	0	0	48	21
737.31	2.50		12	Sandy Gravel	3.3	41.2	151.5	4.9	4.4	97.1	97	0	0	53	24
735.31	2.00		36	Hard Till	3.8	92.8	134.6	5.6	10.0	100.5	100	0	0	55	26
732.81	2.50		28	Hard Till	3.6	72.1	166.5	5.3	7.8	108.8	109	0	0	60	28
730.31	2.50		39	Hard Till	5.2	100.5	179.5	7.7	10.8	117.4	117	0	0	65	31
727.31	3.00		42	Hard Till	6.9	108.2	134.2	10.3	11.7	122.1	122	0	0	67	34
724.81	2.50		2.90		17.5	56.0	143.8	26.0	6.0	147.3	144	0	0	79	36
722.81	2.00		14	Fine Sand	2.3	48.1	207.9	3.3	5.2	157.3	157	0	0	87	38
720.31	2.50		32	Fine Sand	6.6	109.9	269.5	9.8	11.8	173.0	173	0	0	95	41
717.81	2.50		48	Fine Sand	12.6	164.9	460.8	18.8	17.8	211.0	211	0	0	116	43
715.31	2.50		100	Fine Sand	42.1	343.5	502.8	62.4	37.0	273.4	273	0	0	150	46
711.31	4.00		100	Fine Sand	67.3	343.5	505.7	99.9	37.0	366.3	366	0	0	201	50
710.81	0.50			Sandstone	48.8	279.1	554.5	72.4	30.1	438.8	439	0	0	241	50.2
710.31	0.50			Sandstone	48.8	279.1	603.3	72.4	30.1	511.2	511	0	0	281	50.7
709.81	0.50			Sandstone	48.8	279.1	652.1	72.4	30.1	583.6	584	0	0	324	51.2
709.31	0.50			Sandstone	48.8	279.1	700.9	72.4	30.1	656.0	656	0	0	361	51.7
708.81	0.50			Sandstone	48.8	279.1	749.7	72.4	30.1	728.4	728	0	0	404	52.2
708.31	0.50			Sandstone	48.8	279.1	798.5	72.4	30.1	800.8	798	0	0	439	52.7
707.81	0.50			Sandstone	48.8	279.1	847.2	72.4	30.1	873.2	847	0	0	466	53.2
707.31	0.50			Sandstone	48.8	279.1	896.0	72.4	30.1	945.6	896	0	0	493	53.7
706.81	0.50			Sandstone	48.8	279.1	944.8	72.4	30.1	1018.0	945	0	0	520	54.2
706.31	0.50			Sandstone	48.8	279.1	993.6	72.4	30.1	1090.4	994	0	0	546	54.7
705.81	0.50			Sandstone	48.8	279.1	1042.4	72.4	30.1	1162.8	1042	0	0	573	55.2
705.31	0.50			Sandstone	48.8	279.1	1091.2	72.4	30.1	1235.2	1091	0	0	600	55.7
704.81	0.50			Sandstone	48.8	279.1	1140.0	72.4	30.1	1307.6	1140	0	0	627	56.2
704.31	0.50			Sandstone	48.8	279.1	1188.8	72.4	30.1	1380.1	1189	0	0	654	56.7
703.81	0.50			Sandstone	48.8	279.1	1237.6	72.4	30.1	1452.5	1238	0	0	681	57.2
703.31	0.50			Sandstone		279.1			30.1						

# IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

I.D.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

Modified 10/18/2011

SUBSTRUCTURE=====	pier 1	MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses			
REFERENCE BORING =====	B-2 (1970s)				
LRFD or ASD or SEISMIC =====	LRFD	Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
PILE CUTOFF ELEV. =====	761.68 ft				
GROUND SURFACE ELEV. AGAINST PILE DURING DR	749.50 ft	<b>664 KIPS</b>	<b>610 KIPS</b>	<b>304 KIPS</b>	<b>49 FT.</b>
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD)	Scour				
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====	732.00 ft				
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====	434.00 ft				

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1540 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)==== 40.00 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE : 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 307.96 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 115.48 KIPS

PILE TYPE AND SIZE ===== Steel HP 12 X 84

Plugged Pile Perimeter===== 4.100 FT. Unplugged Pile Perimeter===== 5.942 FT.

Plugged Pile End Bearing Area===== 1.051 SQFT. Unplugged Pile End Bearing Area===== 0.171 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
749.10	0.40	0.50			0.6		3.6	0.9		1.4	1	0	0	0	13
746.60	2.50	0.20			1.7	2.9	5.3	2.4	0.5	3.8	4	1	0	1	15
744.10	2.50	0.20			1.7	2.9	9.9	2.4	0.5	6.8	7	2	0	2	18
740.60	3.50	0.40			4.6	5.9	139.4	6.6	1.0	33.7	34	5	0	14	21
732.00	8.60		50	Medium Sand	48.0	130.9	190.1	69.6	21.3	103.7	104	31	0	26	30
729.10	2.90		51	Medium Sand	16.8	133.5	<b>107.3</b>	24.4	21.7	111.9	107	31	0	28	33
726.60	2.50	2.30			13.1	33.9	<b>110.0</b>	18.9	5.5	129.1	110	31	0	29	35
724.10	2.50	1.60			10.3	23.6	<b>126.2</b>	14.9	3.8	145.0	126	31	0	38	38
721.60	2.50	2.00			11.9	29.4	<b>123.4</b>	17.3	4.8	159.9	123	31	0	37	40
719.60	2.00	1.00			5.8	14.7	234.9	8.4	2.4	<b>185.5</b>	186	31	0	71	42
715.10	4.50		46	Medium Sand	21.5	120.4	397.7	31.1	19.6	<b>239.6</b>	240	31	0	101	47
714.60	0.50			Limestone	51.1	261.8	448.8	74.0	42.6	<b>313.6</b>	314	31	0	141	47.1
714.10	0.50			Limestone	51.1	261.8	499.9	74.0	42.6	<b>387.6</b>	388	31	0	182	47.6
713.60	0.50			Limestone	51.1	261.8	551.0	74.0	42.6	<b>461.7</b>	462	31	0	223	48.1
713.10	0.50			Limestone	51.1	261.8	602.0	74.0	42.6	<b>535.7</b>	536	31	0	264	48.6
712.60	0.50			Limestone	51.1	261.8	653.1	74.0	42.6	<b>609.7</b>	610	31	0	304	49.1
712.10	0.50			Limestone	51.1	261.8	704.2	74.0	42.6	<b>683.7</b>	684	31	0	345	49.6
711.60	0.50			Limestone	51.1	261.8	<b>755.3</b>	74.0	42.6	757.7	755	31	0	384	50.1
711.10	0.50			Limestone	51.1	261.8	<b>806.3</b>	74.0	42.6	831.7	806	31	0	412	50.6
710.60	0.50			Limestone	51.1	261.8	<b>857.4</b>	74.0	42.6	905.8	857	31	0	440	51.1
710.10	0.50			Limestone	51.1	261.8	<b>908.5</b>	74.0	42.6	979.8	908	31	0	469	51.6
709.60	0.50			Limestone	51.1	261.8	<b>959.5</b>	74.0	42.6	1053.8	960	31	0	497	52.1
709.10	0.50			Limestone			261.8								

# IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

I.D.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

Modified 10/18/2011

SUBSTRUCTURE=====		Pier 2	MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses			
REFERENCE BORING =====		B-1 (1970s)				
LRFD or ASD or SEISMIC =====		LRFD	Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
PILE CUTOFF ELEV. =====		761.84 ft	578 KIPS	550 KIPS	270 KIPS	59 FT.
GROUND SURFACE ELEV. AGAINST PILE DURING DRILLING =====		742.25 ft				
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====		Scour				
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====		726.40 ft				
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====		434.00 ft				

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1644 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)==== 34.00 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE = 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 386.82 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 145.06 KIPS

PILE TYPE AND SIZE ===== Steel HP 14 X 73

Plugged Pile Perimeter===== 4.700 FT. Unplugged Pile Perimeter===== 6.975 FT.

Plugged Pile End Bearing Area===== 1.379 SQFT. Unplugged Pile End Bearing Area===== 0.149 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
739.70	2.55	25	25	Medium Sand	5.5	33.2	8.1	11.1	11	3	0	3	22		
736.70	3.00	17	17	Medium Sand	4.4	27.8	67.8	6.5	3.0	20.8	21	5	6	25	
735.20	1.50	3.00	3.00	Medium Sand	10.8	58.0	88.2	16.0	6.2	37.9	38	11	9	27	
733.20	2.00	3.50	15	Medium Sand	16.1	67.6	36.7	23.9	7.3	54.5	37	20	0	29	
730.20	3.00			Medium Sand	0.0	0.0	177.6	0.0	0.0	69.7	70	20	0	18	
727.20	3.00	41		Sandy Gravel	21.1	140.9	140.2	31.3	15.2	94.6	95	32	0	35	
726.40	0.80	24		Medium Sand	1.6	82.4	145.3	2.4	8.9	97.5	97	33	0	35	
723.20	3.20	25		Medium Sand	6.9	85.9	186.5	10.2	9.3	111.3	111	33	0	39	
721.70	1.50	35		Fine Sand	4.5	120.2	90.1	6.7	13.0	107.1	90	33	0	40	
719.20	2.50	1.00		Fine Sand	8.3	19.3	99.7	12.4	2.1	119.6	100	33	0	43	
717.20	2.00	6		Fine Sand	1.0	20.6	100.7	1.4	2.2	121.1	101	33	0	45	
714.70	2.50	6		Fine Sand	1.2	20.6	263.4	1.8	2.2	140.3	140	33	0	47	
712.20	2.50	53		Sandy Gravel	30.7	182.1	266.6	45.6	19.6	182.9	183	33	0	50	
709.70	2.50	45		Sandy Gravel	22.0	154.6	257.7	32.6	16.7	212.2	212	33	0	52	
707.20	2.50	36		Sandy Gravel	13.3	123.7	305.3	19.7	13.3	235.6	236	33	0	55	
704.70	2.50	46		Sandy Gravel	23.1	158.0	513.9	34.2	17.0	289.8	290	33	0	57	
704.20	0.50			Limestone	58.5	343.5	572.4	86.9	37.0	376.7	377	33	0	57.6	
703.70	0.50			Limestone	58.5	343.5	631.0	86.9	37.0	463.6	464	33	0	58.1	
703.20	0.50			Limestone	58.5	343.5	689.5	86.9	37.0	550.4	550	33	0	58.6	
702.70	0.50			Limestone	58.5	343.5	748.1	86.9	37.0	637.3	637	33	0	59.1	
702.20	0.50			Limestone	58.5	343.5	806.6	86.9	37.0	724.2	724	33	0	59.6	
701.70	0.50			Limestone	58.5	343.5	865.1	86.9	37.0	811.1	811	33	0	60.1	
701.20	0.50			Limestone	58.5	343.5	923.7	86.9	37.0	898.0	898	33	0	60.6	
700.70	0.50			Limestone	58.5	343.5	982.2	86.9	37.0	984.9	982	33	0	61.1	
700.20	0.50			Limestone	58.5	343.5	1040.8	86.9	37.0	1071.8	1044	33	0	61.6	
699.70	0.50			Limestone	58.5	343.5	1099.3	86.9	37.0	1158.7	1099	33	0	62.1	
699.20	0.50			Limestone	58.5	343.5	1157.9	86.9	37.0	1245.6	1158	33	0	62.6	
698.70	0.50			Limestone		343.5			37.0						

# IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

I.D.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

Modified 10/18/2011

SUBSTRUCTURE===== west abut.

REFERENCE BORING ===== B-1

LRFD or ASD or SEISMIC ===== LRF

PILE CUTOFF ELEV. ===== 760.65 ft

GROUND SURFACE ELEV. AGAINST PILE DURING DRILLING ===== 758.65 ft

GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None

BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 424.00 ft

TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== 434.00 ft

## MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
578 KIPS	578 KIPS	318 KIPS	52 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 847 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.00 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 199.29 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 74.74 KIPS

PILE TYPE AND SIZE ===== Steel HP 14 X 73

Plugged Pile Perimeter===== 4.700 FT. Unplugged Pile Perimeter===== 6.975 FT.

Plugged Pile End Bearing Area===== 1.379 SQFT. Unplugged Pile End Bearing Area===== 0.149 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK.	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
					7.1	14.8	10.5	11.3	11	0					
753.90	4.75	0.40			3.0	7.7	42.9	4.4	0.8	18.5	11	0	0	6	7
751.90	2.00	0.40			7.4	32.9	27.1	11.0	3.5	26.9	18	0	0	10	9
750.40	1.50	1.70			4.6	9.7	25.9	6.8	1.0	33.1	27	0	0	15	10
747.90	2.50	0.50			1.9	3.9	27.8	2.9	0.4	36.0	26	0	0	14	13
745.40	2.50	0.20			2.3	3.9	53.8	3.4	0.4	42.0	28	0	0	15	15
742.40	3.00	0.20			1.4	27.5	130.7	2.0	3.0	52.1	42	0	0	23	18
740.40	2.00		8	Medium Sand	9.4	103.1	136.7	14.0	11.1	65.7	52	0	0	29	20
737.90	2.50		30	Sandy Gravel	8.9	99.6	176.5	13.2	10.7	82.3	66	0	0	36	23
735.40	2.50		29	Sandy Gravel	14.8	130.5	163.8	22.0	14.1	101.3	82	0	0	45	25
732.90	2.50		38	Sandy Gravel	9.4	103.1	138.9	14.0	11.1	111.6	101	0	0	56	28
730.40	2.50		30	Sandy Gravel	5.1	68.7	115.9	7.6	7.4	116.2	112	0	0	61	30
727.40	3.00		20	Medium Sand	11.3	40.6	121.4	16.7	4.4	132.3	116	0	0	64	33
725.40	2.00		2.10		12.8	34.8	140.0	19.0	3.7	151.9	121	0	0	67	35
722.90	2.50		1.80		16.9	40.6	164.4	25.1	4.4	177.8	140	0	0	77	38
719.90	3.00		2.10		2.4	48.1	249.3	3.6	5.2	190.3	164	0	0	90	41
717.90	2.00		14	Medium Sand	9.7	130.5	472.0	14.4	14.1	227.6	190	0	0	105	43
715.40	2.50		38	Medium Sand	54.9	343.5	526.8	81.4	37.0	309.0	228	0	0	125	45
712.90	2.50		100	Clean Coarse Sand	65.8	343.5	592.7	97.7	37.0	406.7	309	0	0	170	48
709.90	3.00		100	Clean Coarse Sand	58.5	343.5	651.2	86.9	37.0	493.6	407	0	0	224	51
709.40	0.50			Limestone	58.5	343.5	768.3	86.9	37.0	580.5	494	0	0	271	51.3
708.90	0.50			Limestone	58.5	343.5	826.9	86.9	37.0	667.4	584	0	0	349	51.8
708.40	0.50			Limestone	58.5	343.5	885.4	86.9	37.0	754.3	667	0	0	367	52.3
707.90	0.50			Limestone	58.5	343.5	944.0	86.9	37.0	928.1	754	0	0	415	52.8
707.40	0.50			Limestone	58.5	343.5	1002.5	86.9	37.0	1014.9	841.2	0	0	463	53.3
706.90	0.50			Limestone	58.5	343.5	1061.0	86.9	37.0	1101.8	1002	0	0	510	53.8
705.90	0.50			Limestone	58.5	343.5	1119.6	86.9	37.0	1188.7	1064	0	0	551	54.3
704.90	0.50			Limestone	58.5	343.5	1178.1	86.9	37.0	1129	1188.7	0	0	616	55.3
704.40	0.50			Limestone	58.5	343.5	1236.7	86.9	37.0	1275.6	1178	0	0	648	55.8
703.90	0.50			Limestone	58.5	343.5	951.7	86.9	37.0	1362.5	952	0	0	680	56.3
703.40	0.50				0.0	0.0	951.7	0.0	0.0	1412.4	952	0	0	523	56.8
702.90	0.50				0.0	0.0	951.7	0.0	0.0	1412.4	952	0	0	523	57
702.40	0.50				0.0	0.0	951.7	0.0	0.0	1412.4	952	0	0	523	58
701.90	0.50				0.0	0.0	951.7	0.0	0.0	1412.4	952	0	0	523	59
701.40	0.50														

