

INTERIOR DIAPHRAGM D

The alternate, if utilized, shall be provided at

no additional cost to the Department.

**34" \$ HS bolts, 1516 " \$ holes

Note:

set of oversized holes.

C 12 x 25 *€ Beam and € C 12 at end of channel

INTER	TUR GIRDE	R MOMENT TABLE
		0.5 Span
Is	(in ⁴)	3,270
Ic(n)	(in ⁴)	10,383
Ic(3n)	(in ⁴)	7,688
Ss	(in 3)	243
Sc(n)	(in ³)	390
Sc(3n)	(in ³)	352
DC1	(k/')	0.736
M DC1	('k)	257
DC2	(k/')	0.129
M DC2	('k)	45
DW	(k/')	0.286
Mow	('k)	100
M4_ + IM	('k)	560
Mu (Strength I)	('k)	1,506
Ør Mn	('k)	2,091
fs DC1	(ksi)	12.70
fs DC2	(ksi)	1.53
fs DC2 fs DW	(ksi)	3.41
fs (4+IM)	(ksi)	17.23
fs (Service II)	(ksi)	40.04
$0.95R_hF_{yf}$	(ksi)	47.50
Vf	(k)	23.75

INTERIOR GIRDER REACTION TABLE				
Abut.				
R _{DC1}	(k)	20.1		
R _{DC2}	. (k)	3.4		
Row	(k)	7.6		
R4 + IM	-(k)	79.4		
R Total	(k)	110.5		

B В (4 sides 4" x 4" x 12' $\mathcal{Q} = \frac{3}{4}$ " ϕ H.S. bolts ¹⁵16 '' \$ holes

END DIAPHRAGM DI

Note: Two hardened washers required for each set of oversized holes.

A sides Channel flanges outward from joint
SECTION B-B

All cross frames or diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted. Individual cross frames or diaphragms at supports may be temporarily disconnected to install bearing anchor rods.

- For Information Only

CONSULTING ENGINEERS, LLC LIL K. Waker Drive, Suite 620 Chiang, LL 6690	USER NAME = PLOT SCALE =	DESIGNED - HAA CHECKED - RAD DRAWN - WHI	REVISED REVISED REVISED	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION	STRUCTURAL STEEL DETAIL STRUCTURE NO. 016–0772
Phone (312) 977-0660 Fax (312) 977-0661	PLOT DATE = 10/13/2011	CHECKED - RAD	REVISED		SHEET NO. S16 OF S33 SHEETS

SECTION A-A Two hardened washers required for each *Alternate channels (C 12 x 30) are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section.

R _{DC1}	(k)	20.1
R _{DC2}	(k)	3.4
Row	(k)	7.6
R4 + IM	(k)	79.4
R Total	(k)	110.5

2"	
21/2 -	
112 / 112 / 12	
6″ C 12 x 25	
• • <u>•</u> <u>-</u> <u>'</u> <u>'</u> <u>P</u>	V

Is, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs (Total-Strength I, and Service II) due to non-composite dead loads (in.⁴ and in.³). $I_c(n)$, $S_c(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s(Total-Strength I, and Service II) in uncracked sections, due to short-term composite live loads (in.4 and in.3).

 $I_c(3n)$, $S_c(3n)$; Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s(Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in.4 and in.3). DC1: Un-factored non-composite dead load (kips/ft.).

M_{DC1}: Un-factored moment due to non-composite dead load (kip-ft.). DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

M_{DW}: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.). ML + IM: Un-factored live load moment plus dynamic load allowance (impact)

((kip-ft.).

Mu (Strength I): Factored design moment (kip-ft.).

1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 M4 + IM

 $\phi_{f}M_{n}$: Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).

fs DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi).

MDC1 / Snc

fs DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).

MDC2/ Sc(3n).

fs DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).

MDW / Sc(3n).

fs (4+IM): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).

M4+ IM / Sc(n).

fs (Service II): Sum of stresses as computed below (ksi). fsDC1 + fsDC2 + fsDW + 1.3 fs(4 + IM)

0.95RhFyf: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

> Vf: Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

TS	· · · ·	ILLINOIS FED. AID PROJECT				
			CONTRACT	NO. 6	OR36	
172	2845	2011-206-F	COOK	18	9	
FAIL	F.A.U. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.	