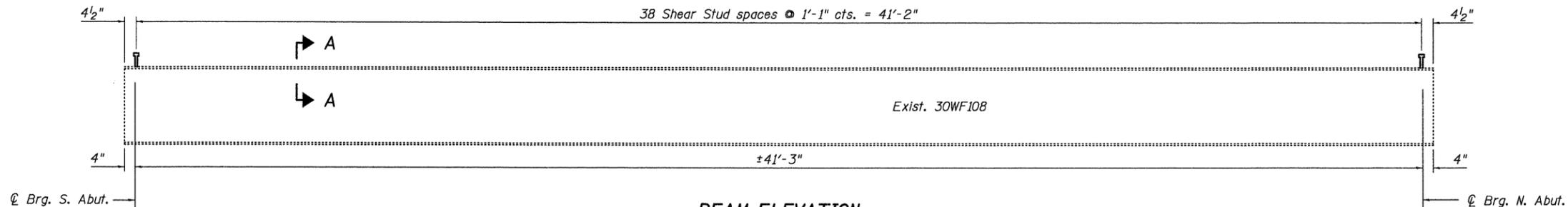


STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION



BEAM ELEVATION

(Typ. all beams)

* Section properties and moment capacities are based upon a 10% reduction in flange thickness due to deterioration documented during an April 2009 inspection.

INTERIOR GIRDER MOMENT TABLE*		
0.462 Span		
I_s	(in ⁴)	4,043
$I_c(n)$	(in ⁴)	11,530
$I_c(3n)$	(in ⁴)	8,612
S_s	(in ³)	272
$S_c(n)$	(in ³)	415
$S_c(3n)$	(in ³)	376
$\bar{\rho}$	(k/')	0.710
$M\bar{\rho}$	('k)	150
$s\bar{\rho}$	(k/')	0.30
$M_s\bar{\rho}$	('k)	64
M_L	('k)	261
M_{IM}	('k)	78
$^{5/3}[M_L + I]$	('k)	566
M_a	('k)	1,014
M_u	('k)	1,641
$f_s \bar{\rho}$ non-comp	(ksi)	6.7
$f_s \bar{\rho}$ (comp)	(ksi)	2.0
$f_s \bar{\rho} [M_L + M_I]$	(ksi)	16.3
f_s (Overload)	(ksi)	25.0
f_s (Total)	(ksi)	-
VR	(k)	40

I_s, S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total and Overload) due to non-composite dead loads (in⁴ and in³).

$I_c(n), S_c(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total and Overload) due to short-term composite live loads (in⁴ and in³).

$I_c(3n), S_c(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total and Overload) due to long-term composite (superimposed) dead loads (in⁴ and in³).

$\bar{\rho}$: Un-factored non-composite dead load (kips/ft.).

$M\bar{\rho}$: Un-factored moment due to non-composite dead load (kip-ft.).

$s\bar{\rho}$: Un-factored long-term composite (superimposed) dead load (kips/ft.).

$M_s\bar{\rho}$: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).

M_L : Un-factored live load moment (kip-ft.).

M_I : Un-factored moment due to impact (kip-ft.).

M_a : Factored design moment (kip-ft.).

$1.3 [M\bar{\rho} + M_s\bar{\rho} + \frac{5}{3} (M_L + M_I)]$

M_u : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).

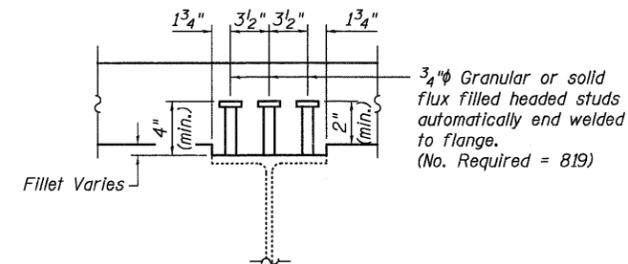
f_s (Overload): Sum of stresses as computed from the moments below (ksi).

$M\bar{\rho} + M_s\bar{\rho} + \frac{5}{3} (M_L + M_I)$

f_s (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).

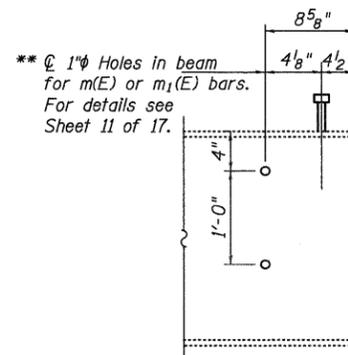
$1.3 [M\bar{\rho} + M_s\bar{\rho} + \frac{5}{3} (M_L + M_I)]$

VR: Maximum $\bar{\rho}$ + impact shear range within the composite portion of the span for stud shear connector design (kips).



SECTION A-A

INTERIOR GIRDER REACTION TABLE		
Abutments		
$R\bar{\rho}$	(k)	20.8
R_L	(k)	30.8
R_I	(k)	9.2
R_{Total}	(k)	60.8



TYP. END OF BEAM ELEVATION

** Field drill holes. Cost included with "Concrete Superstructure".

STRUCTURAL STEEL
INTERSTATE 55 W. FRONTAGE ROAD
OVER I & M CANAL & STATE TRAIL
F.A.I. ROUTE 55 - SECTION 86B-3-R
WILL COUNTY
STRUCTURE NO. 099-0036
PUBLIC WATERS

DESIGNED - SDS
CHECKED - CWC
DRAWN - DLH
CHECKED - SDS/CEH

WHKS & CO.
ENGINEERING
7018 KINGSMILL CT.,
SPRINGFIELD, IL
(217) 483-9457
DESIGN FIRM #184001036

SHEET NO. 14	F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
	55	86B-3-R	WILL	38	27
17 SHEETS	S.N. 099-0036		CONTRACT NO. 60F53		
FED. ROAD DIST. NO.		ILLINOIS	FED. AID PROJECT		