

INTERIOR GIRDER MOMENT TABLE Pier 1 0.6 Sp. 3 25949 10926 25949 14458 10926 25949 28056 (in⁴)28056 25949 41402 G(3n)(in4) 21403 25949 30071 25949 21403 502 709 (in^3) 502 1128 798 1128 709 1104 1128 65.3 1022 65.3 (in³) 1128 (in³) 709 1104 1128 709 1128 Sxe 0.966 0.966 (k/') 0.996 1.066 1.066 M DC1 ('k) 302 1263 613 1194 2.36 0.173 0.173 0.173 0.173 (k/') 0.173 M DC2 ('k) 72 176 145 168 60 0.350 0.350 0.350 0.350 0.350 DW (k/')357 293 339 ('k) 147 120 Mow M & + IM ('k) 1115 1227 1449 1195 1032 2356 Mu (Strenath I. ('k) 2639 4482 3923 4302 ('k) 23 26 14 13.4 (ksi) 7.2 9.2 12.7 5.6 (ksi) 1.9 1.1 2.2 22.7 fs DW (ksi) 3.4 24.5 17.0 20.5 fs 1.3(4+IM) (ksi) 16.5 (ksi) 10.1 6.4 9.0 7.5 6.2 34.8 31.6 fs (Service II) (ksi, 36.1 34.6

47.8

47.5

57.6

(ksi)

(k)

(ksi)

(ksi)

fs (Total)(Strength

(Fatique I)

F_{cr} (Service II,

STATE OF ILLINOIS

INTERIOR GIRDER REACTI
| N. Abut. | Pier 1 | ION TABLE Pier 2 S. Abut. (k) 25.2 119.3 115.7 22.7 R DC1 (k) P*DC2* 19.8 *19.2* 4.6 (k) 10.2 40.2 39.0 9.3 (k) 116.0 157.9 156.1 107,4 R4 + IM (k) 156.5 337.2 330.0 144.0

47.7

40.0

 $I_{\mathcal{S}}$, $S_{\mathcal{S}}$: Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total-Strength I, and Service II) due to non-composite dead loads (in.4 and in.3).

Ic(n), Sc(n): Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total-Strength I, and Service II) due to shortterm composite live loads (in.4 and in.3).

 $I_c(3n)$, $S_c(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in.4 and in.3).

 S_{xt} : Section modulus about the major axis of section to the controlling flange, tension or compression, taken as yield moment with respect to the controlling flange over the yield strength of the controlling flange (in.³).

DC1: Un-factored non-composite dead load (kips/ft.).

M_{DC1}: Un-factored moment due to non-composite dead load (kip-ft.). DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

Mow: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.). M\forall + Im: Un-factored live load moment plus dynamic load allowance

(impact)(kip-ft.).

Mu (Strength I): Factored design moment (kip-ft.).

1.25 (MDC1 + MDC2) + 1.5 MDW+ 1.75 ME + IM

Mbl: Factored lateral bending moment for controlling flange plate (kip-ft.).

fe: Factored calculated normal stress at edge of flange for controlling flange plate due to lateral bending (kip-ft.).

fs (Service II): Sum of stresses as computed from the moments below (ksi). M DC1 + MDC2 + MDW + 1.3 M € + IM

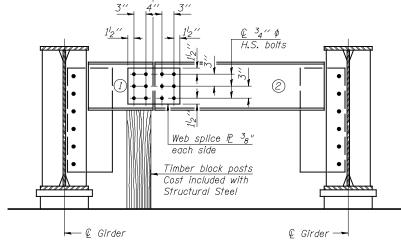
 $f_{\mathcal{S}}$ (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi). 1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 M& + IM

For (Service II): Critical flange stress at Service II computed according to Article 6.10.4.2 (ksi).

For: Critical flange stress computed according to Article 6.10.7 or 6.10.8 (ksi).

Vf: Maximum factored shear range computed according to Article 6.10.10.

M' and R' include the effects of centrifugal force and superelevation.



Stage II construction

END DIAPHRAGM

END DIAPHRAGM STAGE CONSTRUCTION SEQUENCE

- 1.) Order diaphragm in two sections.
- 2.) Attach section 1 of diaphragm to girder 3.
- 3.) Place timber block posts between section (1) of diaphragm and abutment bearing section.
- 4.) Attach section (2) of diaphragm to both girder 4 and section (1) of diaphragm during stage II construction with splice plates.
- 5.) Remove timber block posts.

Stage I construction

₡ Splice		← © Splice 2	┌──Top & Bottom of Web
© Brg Pier 1	1,3 1,3	© Brg. Pier 2	© Brg. S. Abut.
" " " " " " " " " " " " " " " " " " "		- α - α - α - α - α - α - α - α - α - α	
4 Spc. at A/4 = A	B1 4 Spc. at B2/4 =	B2 B3 4 Spc. at	C/4 = C

CAMBER DIAGRAM

Note:

45.8

40.0

46.4

47.5

54.0

42.3

47.5

57.6

50

For dimensions A, B & C, see previous sheet.

Notes:

All structural steel shall be AASHTO M 270 Grade 50.

Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.

All cross frames or diaphragms between beams or girders shall be installed with erection pins and bolts in accordance with the erection plan approved by the Engineer. Individual cross frames or diaphragms at supports may be temporarily disconnected to install bearing anchor rods.

For STAGE II CONSTRUCTION, the diaphragms between Beams 3 & 4 shall be installed with bolts at both beams only finger-tight and with slots positioned to allow maximum differential deflection during the deck pour. Bolts shall be fully tightened as soon as possible after deck pour to minimize differential deflections due to traffic.

STRUCTURAL STEEL STRUCTURE NO. 057-0250

SHEET 15	F.A.I. RTE.	SECTION			COUNTY	TOTAL SHEETS	SHEET NO.		
	55	(57-7HB-1)BR				MCLEAN	153	65	
OF 27		STA. 626+53.70				CONTRACT	NO. 7	0520	
	FED. RO	DAD DIST.	NO.	ILLINOIS	FED.	AID	PROJECT		

CONS	Depp ULTING ingfield	ENG	

8 Spa.

6 Spa.

at 21/2

Мах.

4"

8 Spa._

at 21/4

FIELD SPLICE DETAIL

(Splice 2 shown, Splice 1

similar by opposite hand)

6 Spa.

P 12"x12"x2'-10" (NTR)

P 14"x12"x1'-434

2 Ps 2"x5"x2'-10'

(One Ea. Side)

2 Ps 34"x5"x3"-7"

P 12"x12"x1'-914"

P 34"x12"x3'-7"

 $P^{3}_{8}''x1'-1''x3'-3'' (NTR)$

(NTR)

(NTR)

(NTR)

	CONSULTING ENGINEERS Springfield, Illinois				
DESIGNED:	DCD	DRAWN:	P. Ray		
CHECKED:	CMV	CHECKED:	CMV/DCD		