

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

INTERIOR GIRDER MOMENT TABLE (W36x150)		
	Pier	E. Abut.
I_s (in ⁴)	9,040	9,040
$I_{c(n)}$ (in ⁴)	23,394	-
$I_{c(3n)}$ (in ⁴)	17,221	17,221
S_s (in ³)	504	504
$S_{c(n)}$ (in ³)	729.5	-
$S_{c(3n)}$ (in ³)	660.4	660.4
Z (in ³)	581	581
R (kip)	0.943	0.943
M_Q (kip)	220.8	319.7
S_Q (kip)	0.34	0.34
M_{sP} (kip)	79.6	115.3
M_L (kip)	391.7	293.2
M_{Imp} (kip)	109.7	82.1
$S_g [M_L + M_{Imp}]$ (kip)	835.7	625.5
M_o (kip)	1,477	1,379
M_u (kip)	2,979	1,743
f_s (non-comp) (ksi)	5.25	7.6
f_s (comp) (ksi)	1.45	2.75
f_s [5 ₃ (M _L + M _{Imp})] (ksi)	13.75	14.9
f_s (Overload) (ksi)	20.45	25.2
f_s (Total) (ksi)	-	-
VR (kip)	46.4	-
		39.5

INTERIOR GIRDER REACTION TABLE	
Abut.	Pier
R_B (kip)	27.8
R_L (kip)	38.9
M_{Imp} (kip)	10.9
R_{Total} (kip)	77.6
	146.6

* Compact section

** Braced non-compact and partially braced section

I_s , S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total and Overload) due to non-composite dead loads (in.⁴ and in.³).

$I_{c(n)}$, $S_{c(n)}$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total and Overload) due to short-term composite live loads (in.⁴ and in.³).

$I_{c(3n)}$, $S_{c(3n)}$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total and Overload) due to long-term composite (superimposed) dead loads (in.⁴ and in.³).

Z : Plastic Section Modulus of the steel section in non-composite areas (in.³).

\bar{Q} : Un-factored non-composite dead load (kips/ft.).

M_{Q} : Un-factored moment due to non-composite dead load (kip-ft.).

S_Q : Un-factored long-term composite (superimposed) dead load (kips/ft.).

M_{sP} : Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).

M_L : Un-factored live load moment (kip-ft.).

M_{Imp} : Un-factored moment due to impact (kip-ft.).

M_o : Factored design moment (kip-ft.).

$1.3 [M_Q + M_{sP} + \frac{5}{3} (M_L + M_{Imp})]$

M_u : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).

f_s (Overload): Sum of stresses as computed from the moments below (ksi).

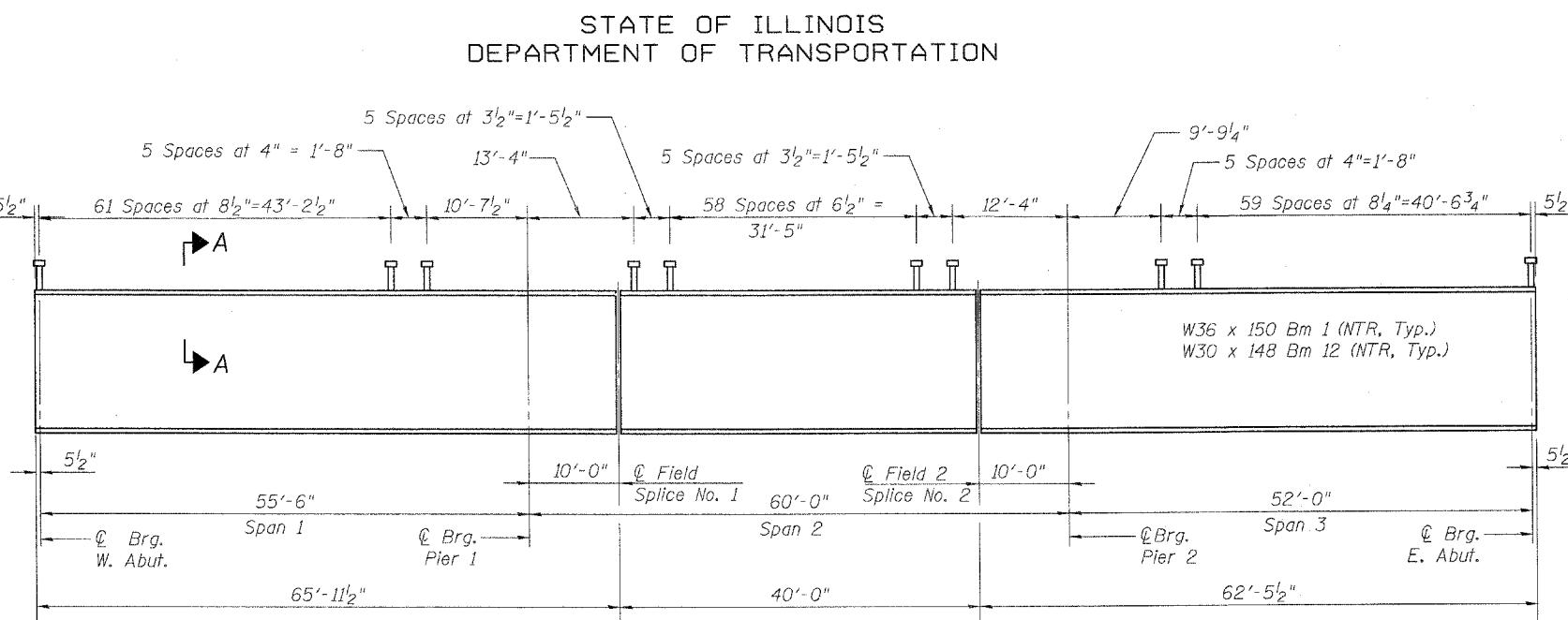
$M_Q + M_{sP} + \frac{5}{3} (M_L + M_{Imp})$

f_s (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).

$1.3 [M_Q + M_{sP} + \frac{5}{3} (M_L + M_{Imp})]$

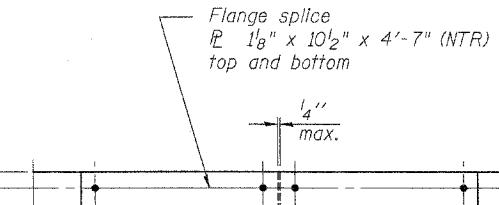
VR: Maximum horizontal shear range within the composite portion of the span for stud shear connector design (kips).

DESIGNED SSM
CHECKED JLA
DRAWN GYR
CHECKED SSM

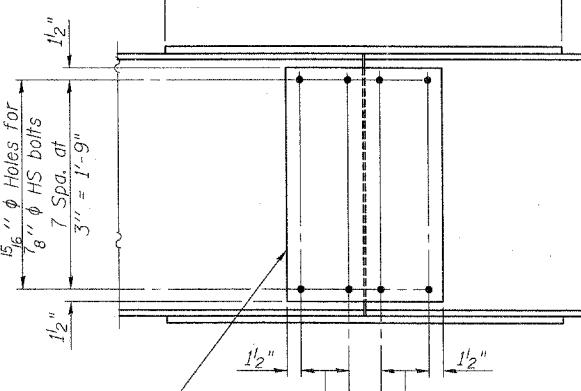


ROUTE NO.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
F.A.P. 301 (US 20)	(2HB-1D)	WINNEBAGO	107	79

Contract #64B07



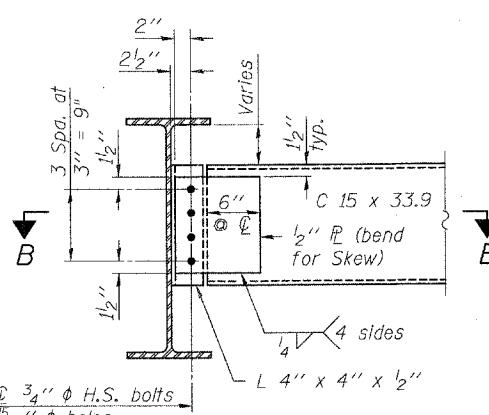
PLAN



ELEVATION

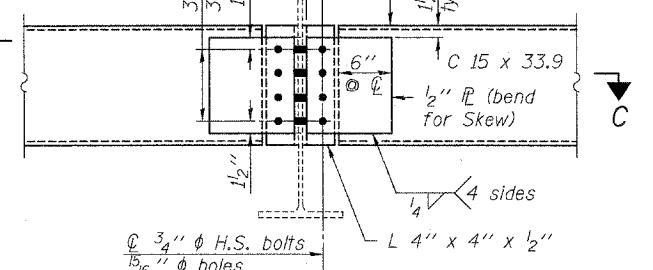
SPLICE DETAIL BEAM 12

(2 Required)



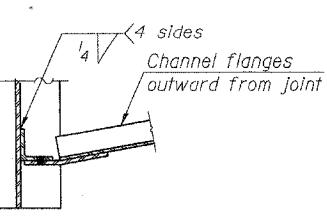
END DIAPHRAGM D
(20 Required)

NOTES:
Two hardened washers required for each set of oversized holes.
Existing diaphragm angles shall be removed from existing beams using the air-arc method.
Cost included with Structural Steel Renewal.



Holes to be drilled in existing beams in the field using holes in proposed connection angle as template Cost included with Furnishing and Erecting Structural Steel.

Channel flanges outward from joint



SECTION A-A

TOP OF BEAM ELEVATIONS

BEAM	W. ABUT.	PIER 1	***SPLICE 1	***SPLICE 2	PIER 2	E. ABUT.
1	757.19	756.63	756.53	756.13	756.03	755.47
12	757.98	757.48	757.39	757.03	756.93	756.46

For fabrication only.
*** Elevations at Top of Beams, Not Top of Splice Plates.

SECTION B-B
BEAM 1 & BEAM 12 ONLY

BEAM 2 THRU BEAM 11 ONLY

Plans Prepared by: Kudrna & Associates, Ltd.

STRUCTURAL STEEL DETAILS

F.A.P. ROUTE 301 (US 20)

OVER SIMPSON ROAD

SECTION (2HB-1D)

WINNEBAGO COUNTY

STATION 849+27.97

STRUCTURE NO. 101-0053 (W.B.)

STRUCTURE NO. 101-0054 (E.B.)

SHEET NO. 14
34 SHEETS