# **STRUCTURE GEOTECHNICAL REPORT**

## Proposed S.N. 081-1120

Existing S.N. 081-1018

IL Rte 5/John Deere Road **Over Drainage Ditch** 1.2 Miles East of I-74 FAP Route 595 Section (142-1, 142)R **Rock Island County** 

PTB 155 - Item 026 IDOT Job No. D-92-003-06 Contract No. 64B83

Prepared By: Pete Sarich, EIT Lin Engineering Ltd. 3261 S Meadowbrook Road Suite 500 Springfield, IL 62711 (217) 679-2928

**Date Prepared:** February, 2012

Date Revised: August, 2012

Prepared For: Joseph Hosanna, SE Ciorba Group 5507 N Cumberland Ave., Suite 402 Chicago, IL 60656 (773) 775-4009

### Approved By:

Mike Haley, PE, SE Lin Engineering Ltd. 3261 S Meadowbrook Road Suite 500 Springfield, IL 62711 (217) 679-2928

### Exhibits:

- 1) Location Map
- 2) Boring Locations
- KL 3) Subsurface Data Profile
- 4) Boring Logs
- 5) Slope Stability Output
- 6) Special Provisions

### **Project Description and Proposed Structure Information**

This project consists of replacing an existing single barrel concrete box culvert with a double barrel reinforced concrete box culvert under IL Rte. 5 at station 310+60 to accommodate proposed widening of the roadway. The structure will be rotated clockwise to improve its alignment with the channel. The structure will carry three lanes of traffic in each direction. The proposed structure is an 11'x4' double barrel reinforced concrete box culvert, 174'-0" long out-to-out headwalls with no skew. The proposed structure design will follow the LRFD Design Specifications. The proposed culvert opening has been increased to satisfy hydraulic design requirements. Complete removal of the existing structure will be required for construction. This work will need to be completed using stage construction.

The stage construction requires soil retention for excavation during removal of existing structure and construction of the proposed structure. The maximum fill height is approximately 4'-0" above the proposed culvert. The structure will have  $\pm$ 7'-3" long horizontal cantilever wingwalls at the south end that will retain a 1:2 (V:H) embankment slope. The north end of the culvert will have L-type wingwalls placed at right angles to the structure. On the USGS Coal Valley quadrangle map, the project area falls within Section 15 of Township 17 N and Range 1 W of the 4<sup>th</sup> PM. A location map is presented in Exhibit 1.

The project also requires separate SGR's to be prepared for SN 081-1118, 44<sup>th</sup> Avenue Culvert and Retaining Wall Location-1.

### Existing Information

The existing culvert is located at station 310+71.36. The 10'x4' single barrel culvert has a length of  $\pm 132'-0"$  measured along its centerline and has a  $\pm 5$  degree right ahead skew. Existing IL Rte. 5 was built on a horizontally curved alignment. The existing structure has a maximum fill height of  $\pm 4'-0"$ . The roadway currently provides 2 lanes of traffic in each direction. Stationing along the roadway increases from west to east.

Existing plans were not available for the structure.

## Site Investigation, Subsurface Exploration and Generalized Subsurface Conditions

The site is located in an urban area approximately one mile north of the Rock River. The drainage ditch flows from north to south towards the existing structure and merges with another drainage ditch to the west. Existing underground water main and sanitary sewer are outside the limits of the structure.

The boring data was provided by IDOT District 2 personnel. Three borings drilled in July of 2011 are associated with the proposed culvert location. Boring B-1 was drilled at station 310+55 at the centerline of the roadway and was terminated at a depth of 23.5 ft. Boring B-2 was drilled at station 310+28 approximately 87 ft left of the centerline and was terminated at a depth of 21 ft below ground surface. Boring B-3 was drilled at station 310+60 approximately 81.5 ft right of the centerline of roadway and was

Lin Engineering, Ltd.

terminated 26 ft below the ground surface. Boring locations relative to the culvert location are shown in Exhibit 2. It should be noted there is an apparent error in elevations referenced in Boring B-1. It's estimated the boring is approximately 12 ft higher than indicated on the boring log.

At each boring location, a standard penetration test (SPT) was conducted every 2.5 ft according to AASHTO T 206 using a hollow stem auger drill. Boring B-1 was the only boring that encountered water, at the depth of 12 ft. All borings show a majority of the soil immediately below the surface consisting of silty clay loam with blow count values ranging from 4 to 7 blows per ft and unconfined compressive strengths ranging from 0.3 to 3.5 tsf. Borings B-1 and B-2 encountered a 2.5 ft thick sand layer approximately 9 ft below the ground surface. The sand present for borings B-1 and B-2 had blow counts of 4 blows per ft. The cohesive soil just above the rock layers had similar soil properties as the cohesive layers just below the surface with blow counts ranging from 2 to 5 blows per ft and unconfined compressive strengths ranging from 0.2 to 0.8 tsf. Shale rock layer was encountered between depths of 20 to 22 ft from ground surface. Further descriptions of the soil layers can be found in the boring logs attached in Exhibit 4 and Subsurface Data Profile in Exhibit 3.

### Geotechnical Evaluations

Settlement: No significant changes are proposed to the profile grade. The proposed culvert will be extending beyond the existing roadway limits on each end due to proposed widening and clear zone requirements. The soil within the existing roadway limits should be naturally compacted and no significant settlement is anticipated. However, soils outside these limits will have an increase in pressure due to weight of the culvert and new fill, which will cause the culvert to sustain differential settlements. One foot deep removal and replacement will be required along the length of the culvert to establish a working platform and this was taken into account with the settlement calculations. According to the structural planner, a tolerable settlement amount of  $\frac{1}{2}$ " is recommended to address differential settlement concerns. To achieve the desired limit, removal and replacement of unsuitable soils with Rockfill-Foundation is suggested at the south end. The removal and replacement will only be required outside the limits of the existing embankment (approximately 25 feet from the south end). We recommend removal down to elevation 565.2 ft at the south end. Due to the large amount of excavation, braced excavation should be used during construction. Per IDOT Bridge Manual 2.3.11.4.1, an alternative is to utilize a settlement collar at the south end where the structure transitions into new embankment (approximately 25 feet from the end). Settlements near 0.98" at the south end are expected if this option is chosen. This section of the bridge manual also states that a precast box culvert should not be allowed under these conditions.

*Slope Stability:* Stability analyses were performed using a temporary excavation 1:1 slope model which rendered a factor of safety over 3. The resulting maximum excavation required for removal and replacement is 12 ft.

*Scour:* The design scour elevations should correspond to the bottom of the toe wall elevation on upstream and downstream ends as shown in the table below. 10-year velocity thru the proposed culvert is 7.10 fps. The Hydraulic Report recommends Class

A4 Riprap at the upstream end and an excelsior blanket at the downstream end for erosion protection.

Design Secur Elevation (ft.)	Upstream	Downstream
Design Scour Elevation (ft.)	572.90	572.60

*Mining Activity:* According to the Illinois State Geological Survey (ISGS) "Coal Mines in Illinois Viewer," there is an abandoned mine 0.3 miles northwest of the structure's location. However, as per ISGS, the project area is outside the underground mine proximity region.

### Box Culvert Evaluations and Design Recommendations

*Culvert Barrel.* Based on hydraulic requirements and size limitations, a 3-sided structure is not a viable option.

Due to anticipated differential settlements at the ends of the culvert, the precast culvert option is not recommended.

With the large foundation area and proposed Rockfill-Foundation material at the culvert base, the bearing capacity at the base of the foundation was found to be more than adequate for resistance of estimated bearing pressures.

*Wingwalls.* There are several feasible options for selection of wingwalls. The wall type selection should be performed considering but not limited to soil conditions, length and economy.

Per IDOT Culvert Manual Figure 3.1.5-2, based on the 0° skew, 1:2 (V:H) slope behind the wingwall, and an estimated  $H_{L}$  of 5'-7", the wingwall length chart shows a length of 7'-3" with an angle of 45°.

The horizontal cantilever wingwall is the most appropriate design choice according to the Culvert Manual. Horizontal cantilever walls will not be feasible at the north end of the culvert due to geometry restrictions. Based on the Culvert Manual 3.1.3, the appropriate wingwall is an L-type vertical cantilever. The recommended active earth pressure as an equivalent fluid pressure on the wingwalls according to the proposed design is 56 pcf.

Cantilever sheet pile wall with a concrete cap is a feasible option. Given cohesive soils at the base, driving piles appears to be possible. However, this wall type is not economical for short walls.

Soldier pile walls are not an ideal option considering fill situation for the project. Additionally, this wall will require drainage behind it and is not economical for shorter walls.

Gabion baskets appear to be feasible and can be constructed easily and quickly with traditional labor equipment. This wall can be labor intensive and expensive if a nearby stone source is not available.

Lin Engineering, Ltd.

#### **Construction Considerations**

*Cofferdams:* In order to maintain a dry construction area, dewatering techniques may be necessary. However, based on hydraulic conditions, a temporary cofferdam is not expected to be necessary. Stream diversion could be utilized in order to facilitate construction of the box culvert.

*Stage Construction:* In order to maintain traffic flow, stage construction shall be utilized. To retain fill at the edge of slab during stage construction, it is recommended that temporary timber blocking be used to retain the Stage I fill. If this method is not adequate, it may be necessary to provide a Temporary Geotextile Wall per IDOT Bridge Manual Fig. 3.13.2-1.

*Temporary Soil Retention System:* Due to the presence of a rock layer within the required embedment depth of temporary sheet piling, it is recommended that a Temporary Soil Retention System be included in design plans.

*Excavation:* A 1:1 temporary excavation slope for construction clearance has an adequate factor of safety. The factor of safety is limited to 1:1 slopes and any steeper slopes should not be used.

*Backfill:* Backfill within the limits of the paved surface to the top of culvert elevation should be performed according to the special provision for Granular Culvert Backfill which is shown in Exhibit 6. The pay limits of Granular Culvert Backfill include a vertical line projected at the outside edge of shoulder. All other backfill may be composed of soil materials excavated from the project site placed and compacted according to the Standard Specifications.

Ground Improvement: Existing soil shall be excavated down 1 ft to provide a working platform. If settlement collars are not chosen, removal of soil down to elevation 565.2 ft at the south end is recommended to satisfy the planner's recommendation. The pay limits for removal and replacement shall extend 2 feet outside the limits of the barrel.

ίth.





Page 6

Lin Engineering, Ltd.

Exhibit 2 – Boring Locations

IL Rte. 5 (John Deere Road)



	of Transportal Division of Highways Illinios Department of Transportation					0811120	SOIL BORING LO	u		Date	77/3	1
ROUTE	FAP 595	DES	SCRIPT	ION	prope		ert, double 7' x 4' box, .16 m. E. of 41st Street	LO	GGEI	) BY	<u>W. G</u>	arza
SECTION _	142–R		I	OCATIO	)N _	S. Moline	2 Twp 15NE, SEC. , TWP. 17N, RNG. 1W					
COUNTY	Rock Island	DRILLING	METH	OD		Hol	low Stem Auger HAMMI	ER TYPE	C	ME-45 A	utomatic	;
STRUCT. NO. Station	081-1120 310+60		D E P T	B L O W	U C S	M O I S	Surface Water Elev. Stream Bed Elev.		D E P T	B L O W	U C S	M O I S
Station Offset Ground Surface		ft	H	S (⁄6")	Qu (tsf)	T (%)	First Encounter5 Upon Completion After Hrs	70.1 ft ┸ Dry ft ft ft ft ┸	H (ft)	8	Qu (tsf)	T (%)
STIFF brown SI	LTY CLAY LOAM			-	1.5 P	18.0	HARD graytan CLAY with COAL fragments (continued)	560.60		8 12	5.1 S	21.0
MEDIUM brown LOAM	SILTY CLAY	580.10 578.60		3 2 4	0.8 P	23.0	VERY DENSE gray SHALE with COAL lens	558.60		37 1008"		
MEDIUM tan S	ILTY CLAY LOAM			1 2	0.7	24.0	End of Boring					
		576.10		3	B							
VERY SOFT tan	I SILTY LOAM	573.10		2 1 3	0.3 B	27.0	Y,					
VERY LOOSE t: with medium m		01010		2		21.0			30			
VERY SOFT gra	w SILT	570.60	<b>_</b>	0								
		568.60		0 2	0.2 P	32.0						
SOFT gray SILT ORGANICS	LOAM with	566.10	15	0	0.4 B	38.0			35			
VERY SOFT gra	y SILT	00010		0		20.0				1		
				0 4	0.3 B	30.0				1		Ť

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)

					DIL BORING LOG		Data	. 7	714 4
ROUTE FAP 595	_ DESCR		pro N	posed	120 D92-003-06 John Deere Road culvert, double 7' x 4' box, .16 m. E. of 41st Street		Date	<u> </u>	<u>//11</u>
SECTION 142-R		LOCA		S M	Dline Twp 15NE, SEC. , TWP, 17N, RNG	LUGG	ED BI	Y	Garz
COUNTY Rock Island		ETHO	n	<u></u>	When Twp ISINE, SEC., IWP. 1/N, RNG	<u>. 1W</u>			<u> </u>
			и т —		Ilow Stem Auger HAMMER TYP	PE	<u>ME-45</u>	Auton	natic
STRUCT. NO. 081-1120 Station 310+60	- D E	BL	U C	M	Surface Water Elev ft	D		U	м
BORING NO. B-2	- Р Т		S	1	ft	E	LO	C S	0
Station 310+28   Offset 87.00ft Lt Med CL	- н		Qu	S T	Groundwater Elev.:	T H	W		S
Offset87.00ft Lt Med CL Ground Surface Elev581.50	- 	(/6'')	(tsf)	(%)	First Encounter <u>None</u> ft Upon Completion <u>Dry</u> ft			Qu	Т
VERY STIFF brown SILTY CLAY	_ 11   14	(0)	((3))	(/0)	After Hrs. ft	(ft)	(/6")		(%)
LOAM	<u> </u>		3.5	10.0	(continued)	50	00/12	ľ	
5	79.50		P		End of Boring				<u> </u>
MEDIUM light brown SILTY CLAY	_	2							
5	78.00	3 4	0.8 B	24.0					
SOFT light brown/gray SILTY		2							
CLAY LOAM		1		28.0		25			
57	75.50	3	В						
SOFT tan SILTY LOAM									
		0	0.3	28.0	X X	_			
		2	В						
· · · · · · · · · · · · · · · · · · ·	2.50	1							
LOOSE tan dirty SAND with medium moist GRAVEL	-10	0				-30			
	_	3							
	0.00								
MEDIUM gray/red CLAY LOAM		1							
EA	B.00	2 3	0.8 P	30.0					
00		Ť							
SOFT redish brown CLAY LOAM	4	1							
		2		27.0		-35			
	5.00	2	В						
DENSE gray SHALE									
CENCE GRAY OFFICE	-	10 12							
	1	· - 1	1					1	

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)

	of Transpo	ortat	ior	)		SC	DIL BORING LOO	G		3-	<u>1</u>	
	ivision of Highways linics Department of Tran	sportation/	D-2		pro	081-1 <sup>-</sup>	120 D92-003-06 John Deere Road culvert, double 7' x 4' box, .16 m. E. c	∧f		Date	7/8	<u>B/11</u>
ROUTE	FAP 595	DE	SCR	IPTIO	N		culvert, double 7' x 4' box, .16 m. E. c 41st Street	LC	DGG	ED BY	<u>W. (</u>	Garza
SECTION	142-R		L	OCA		S. Mo	line Twp 15NE, <b>SEC. , TWP.</b> 17N, F	RNG. 1	W			
COUNTY R	ock Island D	RILLIN	G ME	THO	)	Ho	llow Stem Auger HAMMER		C	VE-45	Autom	atic
STRUCT. NO Station	<u>081-1120</u> 310+60		DE	B L	U C	M	Surface Water Elev	ft	D	В	U	м
			Р	0	s	1	Stream Bed Elev.	ft	E P	L O	C S	0
	B-3 310+60		T H	W S	Qu	S T	Groundwater Elev.: First Encounter <u>None</u>	4	Т Н	W S	Qu	S T
Offset	81.50ft Rt Med C ce Elev. 579.20		(ff)	//ค"า	(tsf)	(%)	Upon Completion Dry	ft		_		-
	LTY CLAY LOAM			(0)	(131)	(70)	After Hrs MEDIUM gray SILTY CLAY	ft	(п)	(/6'') 0	(tsf)	(%) 34.0
				-	1.3 P	19.0				2	В	
		577.20						557.70	·			
STIFF brown SI	LTY CLAY LOAM		_	2	1.8	22.0	VERY DENSE gray SHALE			4 30		
		575.70		4	В	22.0		555.70		55		
			—									
MEDIUM tan SII	TY CLAY LOAM		5	2			VERY DENSE gray SHALE		-25	100/9"		
		573.20		4	0.7 B	28.0		553.20				
							End of Boring	000.20				
MEDIUM tan Sil	TY LOAM			2								
		570.70		2 3	0.6 P	28.0						
		070.70										
STIFF gray SILT	Y LOAM with		-10	0					-30			
SAND lens		r.co. oo		1	1.4 P	26.0		-				
		568.20		-7								
MEDIUM gray S	ILTY LOAM with			0								
SAND lens				2	0.7	31.0						
		565.70	+	2	В				_			
SOFT orav SILT	Y CLAY with 12%		_	0							_	
ORGANICS			-15	0	0.3	63.0			-35			
		563.20		2	P	<u> </u>				V		
				~								
MEDIUM gray S 10% ORGANICS	CLAY WITH		-+	0	0.5	41.0					•	
		560.70		2	В			-				
								-				
MEDIUM gray Si	LTY CLAY		-20	0					-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)



Vertical Coordinate

### GRANULAR CULVERT BACKFILL 4/10/06

This work consists of backfilling box culverts or three-sided structures with granular materials. This work shall be performed at locations shown on the plans or as directed by the Engineer.

Backfilling shall be performed according to Article 502.10. The backfill material shall meet the requirements of Article 1004.06, except the gradation shall be CA-06 or CA-10.

Granular Culvert Backfill will be measured for payment in cubic yards compacted in place. Additional material required to backfill excavation outside the limits shown on the plans will not be measured for payment. This work shall be paid for at the contract unit price per cubic yard for GRANULAR CULVERT BACKFILL. 

#### ROCKFILL - FOUNDATION 4/22/05

This work consists of constructing a layer of rockfill below culverts or spread footings having unstable or unsuitable soil conditions. When shown on the plans, the rockfill limits and thickness shall be confirmed by the Engineer prior to excavating below the theoretical top of rockfill line.

Materials shall meet the requirements of the following Articles of the Standard Specifications:

CA-6 and CA-7		1004.04
Rockfill	* * * * * * * * * * * * * * * * * * * *	1005.01

All rockfill shall be well graded. The gradation of rockfill shall be selected based on layer thickness as shown below:

Less than or equal to 1 ft	*******	Gradations with a max size of 4 inches <sup>b</sup>
Greater than 1 ft		Primary Crusher Run
Greater than 3 ft	•••••	Primary Crusher Run or Shot Rock (18" max size)
<sup>b</sup> Gradations with a maximum siz	e of 2 inches or sma	iler shall have less than 6% passing the No. 200 sieve.

Excavation shall be performed according to Section 202 of the Standard Specifications. Excavated material may be placed in fills according to Article 202.03 with the approval of the Engineer.

The method of rockfill placement shall be approved by the Engineer. Rockfill shall be capped according to application as shown below:

Spread Footing	4 to 6 inches CA-6	
	4 to 6 inches CA-7	
Pre-Cast Box Culverts	Porous Granular Bedding Material (Article 540.06)	
Pre-Cast Pipe Culverts	4 to 6 inches Fine Aggregate (Article 542.04(c))	

In spread footing applications, the CA-6 cap shall be compacted to the satisfaction of the Engineer. No compaction of rockfill is required for culvert applications.

This work will be measured and paid for at the contract unit price per ton for ROCKFILL -FOUNDATION. The contract price for ROCKFILL-FOUNDATION shall include excavation, aggregate materials, aggregate material placement, and placement of excavated materials within right-of-way or disposal off right-of-way. *Excavation will not be measured or paid for separately or as part of EARTH EXCAVATION.* For precast concrete box culverts, porous granular bedding material and the excavation required for bedding will be paid for according to Article 540.08. For pipe culverts, the fine aggregate and the excavation required for fine aggregate shall be included in the cost per foot for PIPE CULVERTS of the class and type specified.

KL