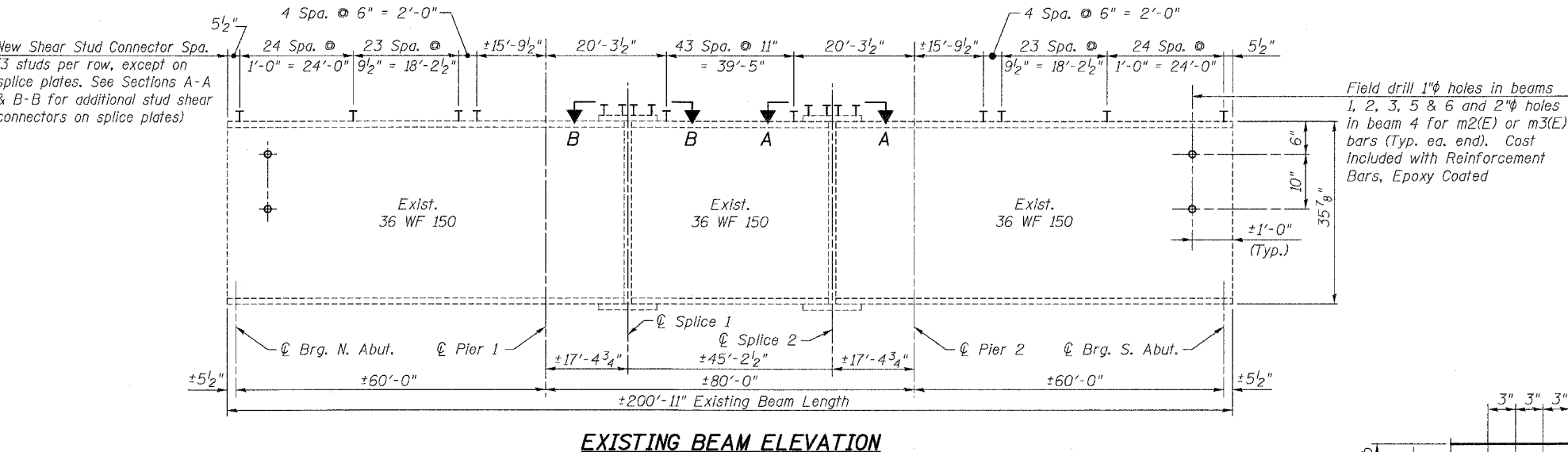
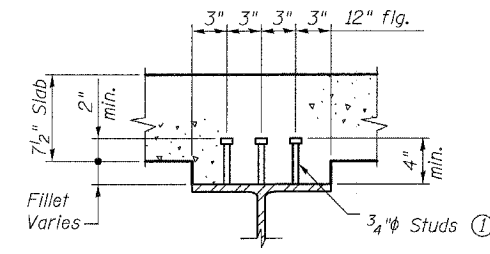


	0.4 SPAN 1 & 0.6 SPAN 3	PIER 1 & 2	0.5 SPAN 2
I_s (in.4)	9040	12674	9040
I_c (in.4) (n=9)	21283		21283
I_c (in.4) (n=27)	15606		15606
S_s (in.3)	504	688	504
S_c (in.3) (n=9)	700		700
S_c (in.3) (n=27)	633		633
Z (in.3)		781	
DL (k./ft.)	0.761	1.186	0.761
M _{DL} (ft.k./beam)	166.7	605.4	204.0
s DL (k./ft.)	0.425		0.425
M _s DL (ft.k./beam)	103.6		140.0
M _{LL} (ft.k./beam)	368.9	269.7	435.2
M _{Imp.} (ft.k./beam)	99.6	72.8	111.0
5/3 M _{LL} +Imp. (ft.k./beam)	780.9	570.8	910.2
M _a (ft.k.)	1366.6	1529.0	1630.6
M _u (ft.k.)	2581.8	2147.8	2581.8
f_s (DL non-comp) (k.s.i.)	3.97	10.56	4.86
f_s (DL comp.) (k.s.i.)	1.96		2.65
f_s 5/3 [M _{LL} +M _{Imp.}] (k.s.i.)	13.39	9.96	15.60
f_s (Overload) (k.s.i.)	19.32	20.52	23.12
f_s (Total) (k.s.i.)			
VR (k)	45.4		43.3



	N. & S. ABUT. (3)	PIER 1 & 2
R DL (K)	52.0	93.4
R LL (K)	36.1	42.3
R IMP. (K)	9.7	8.0
R TOTAL (K)	97.8	143.7

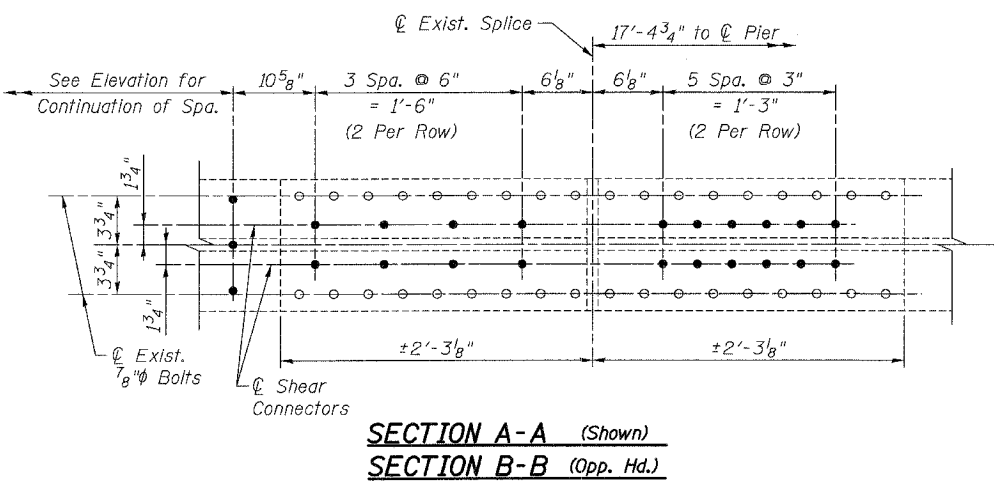
- MOMENT TABLE NOTES:
- I_s and S_s are the moment of inertia and section modulus of the steel section used in computing f_s (Total and Overload).
 - $I_c(n)$ and $S_c(n)$ are the moment of inertia and section modulus of the composite section used in computing stresses due to live load.
 - $I_c(3n)$ and $S_c(3n)$ are the moment of inertia and section modulus of the composite section used in computing stresses due to superimposed dead load.
 - VR is the maximum $L +$ Impact Shear Range within the composite portion of the span.
 - Z is the plastic section modulus to determine the fully plastic moments in the non-composite areas.
 - M_u is the Plastic Moment capacity.
 - f_s (Total) is the sum of the stresses due to $1.3[M_D + M_S D + 5/3(M_L + M_{IMP})]$.
 - f_s (Overload) is the sum of the stresses due to $[M_D + M_S D + 5/3(M_L + M_{IMP})]$.
 - M_D - moment due to dead loads on non-composite section.
 - $M_S D$ - moment due to dead loads on composite section.
 - M_L - moment due to live load on non-composite or composite section.
 - M_{IMP} - moment due to live load impact on non-composite or composite section.
 - M_a (Applied Moment) = $1.3[M_D + M_S D + 5/3(M_L + M_{IMP})]$.



TYPICAL SHEAR STUD DETAIL

(Typical, except use 2 studs per row at existing splice plates. See Sections A-A and B-B.)

- NOTES:
- All studs to be $3/4$ " ϕ Granular or solid flux filled headed studs conforming to Article 1006.32 of the Standard Specifications automatically end welded to flange. (No. required = 2,904)
 - Field drill 1 " ϕ holes in existing end diaphragms at each abutment to receive s(E) bars. See sheet 8 of 17 for Section A-A at abutments and for number and spacing of bars. Cost to drill 1 " ϕ holes is included in the cost for Reinforcement Bars, Epoxy Coated.
 - Dead load reaction at abutments includes superstructure, diaphragm and approach pavement dead load (3.0 k/foot).



TOP OF BEAM ELEVATIONS

Location	Exist. Beam 1	Exist. Beam 2	Exist. Beam 3	Exist. Beam 4	Exist. Beam 5	Exist. Beam 6
⊕ Brg. N. Abut.	444.42	444.49	444.57	444.55	444.46	444.45
⊕ Pier 1	443.14	443.24	443.26	443.25	443.18	443.17
⊕ Splice 1	442.77	442.88	442.89	442.87	442.82	442.80
⊕ Splice 2	441.91	442.05	442.11	442.07	441.98	441.91
⊕ Pier 2	441.57	441.70	441.76	441.72	441.64	441.57
⊕ Brg. S. Abut.	440.39	440.50	440.54	440.51	440.46	440.43

FRAMING PLAN
POWDER MILL ROAD OVER
EAST FORK OF WOOD RIVER
SECTION 03-00044-00-BR
VILLAGE OF EAST ALTON
STA. 13+10
STRUCTURE NO. 060-6400