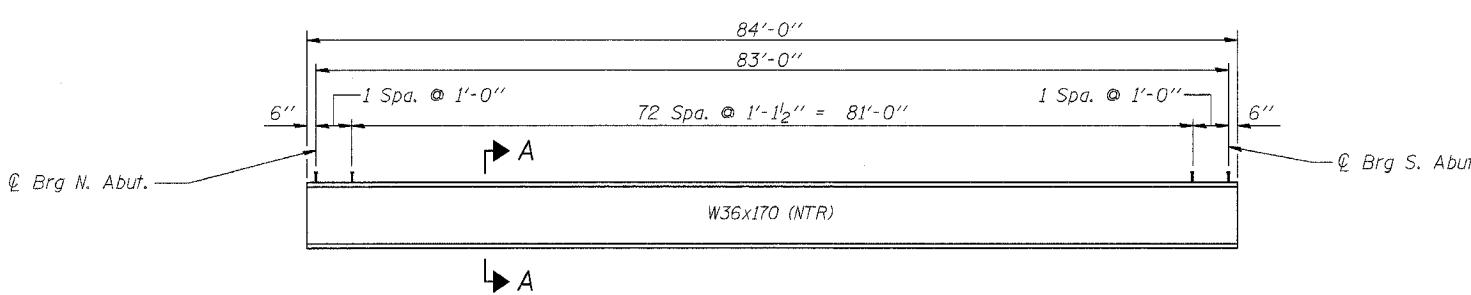
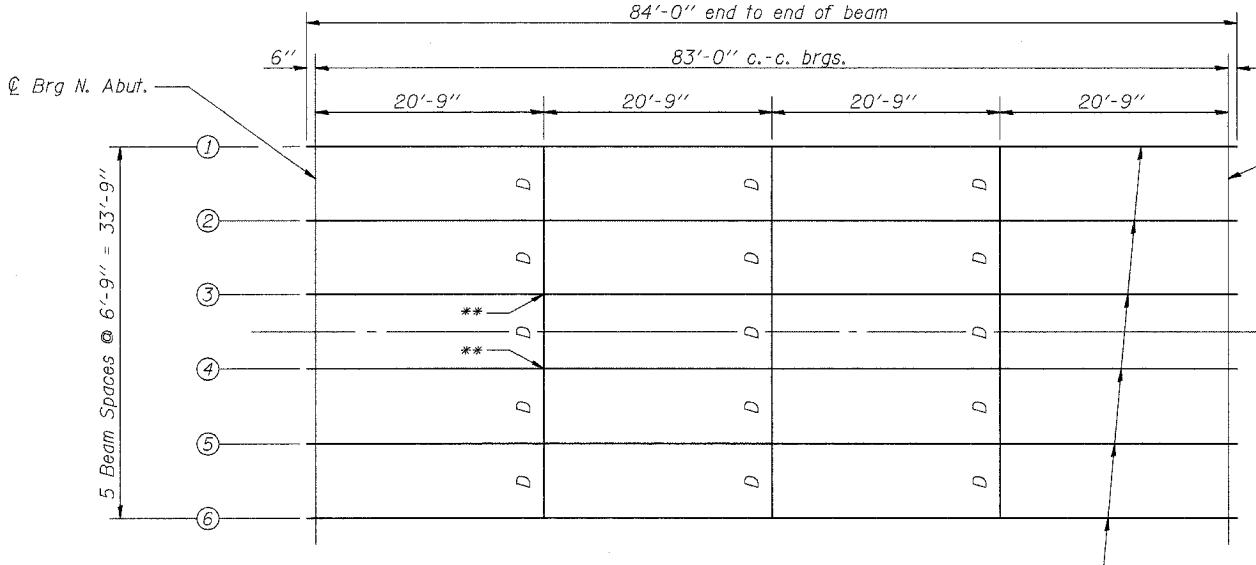
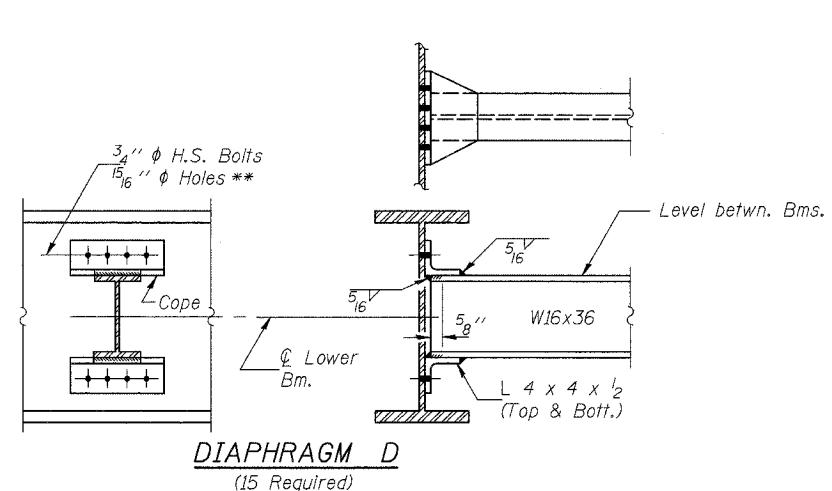
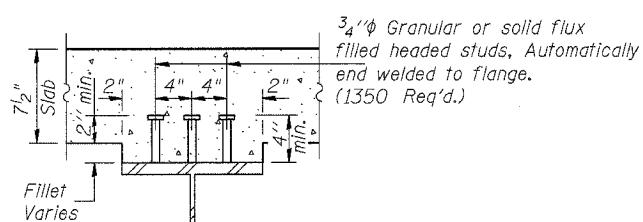


ROUTE NO.	SECTION	COUNTY	TOTAL SHEETS	HEET NO.
F.A.P. 42	2BR	WASHINGTON	33	23
FED. ROAD DIST. NO. 8		ILLINOIS PROJECT		
Sheet 9 of 16				CONTRACT #76389



BEAM ELEVATION  
(Showing Shear Connector Spacing)



\*\* Use 13/16" wide x 1 1/2" long slotted holes in L's for diaphragm connections between beams 3 & 4. Bolts shall be finger tightened prior to deck pour for stage 2 construction and then fully tightened after completion of deck pour for stage 2 construction.

DESIGNED	Ruben V. Boehler
CHECKED	Tim S. Howard
DRAWN	Nicole L. Darling
CHECKED	Michael D. Cummins

$I_s$  and  $S_s$  are the moment of inertia and section modulus of the steel section used in computing  $f_s$  (Overload).

$I_{c(n)}$  and  $S_{c(n)}$  are the moment of inertia and section modulus of the composite section used in computing stresses due to Live Load.

$I_{c(3n)}$  and  $S_{c(3n)}$  are the moment of inertia and section modulus of the composite section used in computing stresses due to superimposed dead loads. (see AASHTO 10.38) VR is the maximum Live Load + Impact shear range in span.

The Plastic Moment capacity ( $M_u$ ) is computed according to AASHTO 10.48.1 and 10.50.1.1.

$f_s$  (Overload) is the sum of the stresses due to  $M_d$  +  $M_s$  +  $5_3(M_L + M_{Imp})$ .

$M_d$  - Moment due to dead loads on non-composite section.

$M_s$  - Moment due to dead loads on composite section.

$M_L$  - Moment due to live loads on composite section.

$M_{Imp}$  - Moment due to live load impact on composite section.

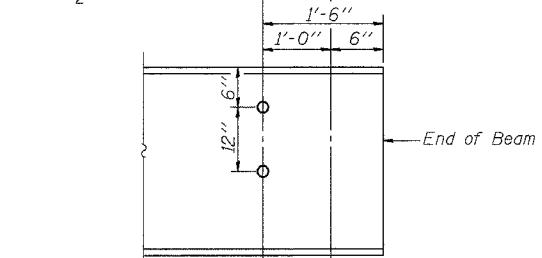
$M_a$  (Applied Moment) =  $1.3[M_d + M_s + 5_3(M_L + M_{Imp})]$ .

INTERIOR GIRDER REACTION TABLE	
Abuts.	
$R_d$ (K)	54.3
$R_t$ (K)	39.3
$Imp.$ (K)	9.4
$R$ (Total) (K)	103.0

INTERIOR GIRDER MOMENT TABLE	
0.5 Span	
$I_s$ ( $in^4$ )	10500
$I_c$ (n) ( $in^4$ )	24511
$I_c$ (3n) ( $in^4$ )	18004
$S_s$ ( $in^3$ )	580
$S_c$ (n) ( $in^3$ )	800
$S_c$ (3n) ( $in^3$ )	724
$D$ ( $K/ft.$ )	0.850
$M_d$ ('K)	732
$S_d$ ('K)	0.458
$M_s$ ('K)	394
$M_L$ ('K)	748
$M_{Imp}$ ('K)	180
$S_g [M_d + M_{Imp}]$ ('K)	1547
$M_a$ ('K)	3474
$M_u$ ('K)	3846
$f_s \delta_{non-comp} (k.s.i.)$	15.1
$f_s \delta_{comp} (k.s.i.)$	6.5
$f_s \delta_3 (L + Imp) (k.s.i.)$	23.2
$f_s$ (Overload) (k.s.i.)	44.8
$VR$ ('K)	48.7

\* Compact, Braced Section

1" Ø holes in beam  
for  $m_2(e)$  bars



Notes:

All steel for beams, diaphragms and connection L's shall be AASHTO M270, Grade 50.

Two hardened washers shall be required over all 13/16" Ø holes and two 1 1/2" x 1 1/2" x 5/16" P washers shall be required over all slotted holes for diaphragms.

"NTR" denotes members to which Notch Toughness Requirements, Zone 2 are applicable.

#### TOP OF BEAM ELEVATIONS

(For Fabrication Only)

Location	Q Brdg. N. Abut.	Q Brdg. S. Abut.
Beam 1	430.39	429.39
Beam 2	429.97	428.97
Beam 3	429.55	428.55
Beam 4	429.13	428.13
Beam 5	428.71	427.71
Beam 6	428.29	427.29

#### STRUCTURAL STEEL

IL ROUTE 127 OVER TRIBUTARY TO CROOKED CREEK  
F.A.P. ROUTE 42 SECTION 2BR  
WASHINGTON COUNTY  
STA. 487+25  
S.N. 095-0076

CUMMINS ENGINEERING CORPORATION  
JOB #: 2158  
FILE: 2158SS  
DATE: 2/10/05