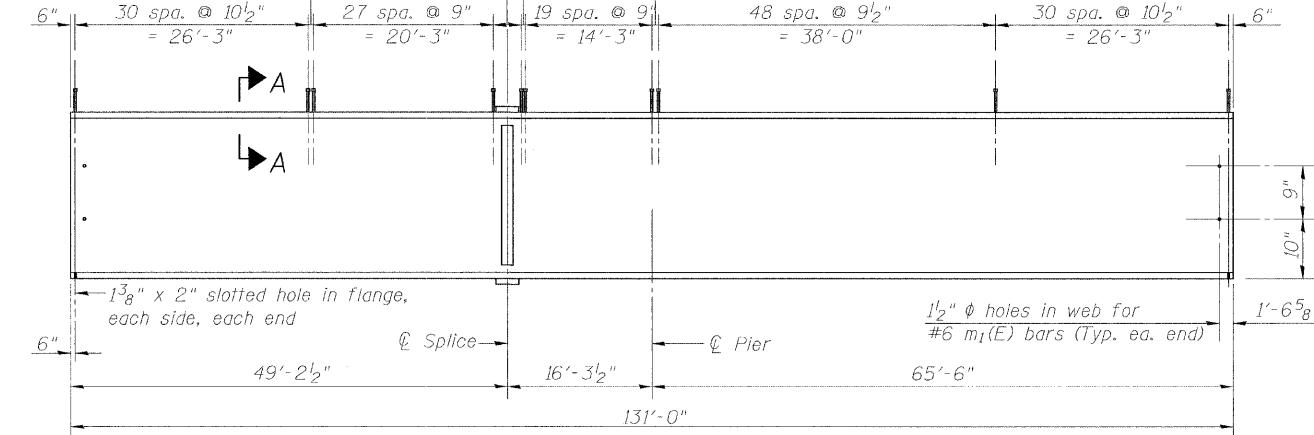


TOP OF BEAM ELEVATIONS

(For Fabrication Only)

	Q Brdg. W. Abut.	Q Splice	Q Pier	Q Brdg. E. Abut.
Beam 1	625.324	625.509	625.602	625.974
Beam 2	625.467	625.657	625.749	626.117
Beam 3	625.585	625.776	625.868	626.235
Beam 4	625.692	625.882	625.975	626.342
Beam 5	625.585	625.776	625.868	626.235
Beam 6	625.467	625.657	625.749	626.117
Beam 7	625.324	625.509	625.602	625.974

INTERIOR GIRDER REACTION TABLE		
	Abut.	Pier
RDC1 (k)	22.6	75.0
RDC2 (k)	3.1	10.5
RDW (k)	7.7	25.5
R _L + IM (k)	72.0	120.4
R _{Total} (k)	105.4	231.4



ELEVATION

INTERIOR GIRDER MOMENT TABLE

	0.4 Sp. 1 or 0.6 Sp. 2	Pier
I _s (in ⁴)	7020	7020
I _{c(n)} (in ⁴)	18310	
I _{c(3n)} (in ⁴)	13083	
I _{e(cr)} (in ⁴)	9046	
S _s (in ³)	505	505
S _{c(n)} (in ³)	736	
S _{c(3n)} (in ³)	658	
S _{e(cr)} (in ³)	568	
DC1 (k'/')	0.925	0.925
M _{DC1} (k')	275.4	483.5
DC2 (k'/')	0.129	0.129
M _{DC2} (k')	38.4	67.4
DW (k'/')	0.314	0.314
M _{DW} (k')	93.5	164.1
M _{L + IM} (k')	738.3	710.6
M _u (Strength I) (k')	1824.5	2178.4
Φ _r M _n (k')	3378.5	2211.8
f _s DC1 (ksi)	6.54	11.49
f _s DC2 (ksi)	0.70	1.42
f _s DW (ksi)	1.71	3.47
f _s (L+IM) (ksi)	12.04	15.01
f _s (Service II) (ksi)	24.60	35.89
0.95R _b F _{yf} (ksi)	47.5	47.5
f _s (Total)(Strength I) (ksi)	-	47.61
Φ _r F _n (ksi)	-	50.0
V _r (k)	15.7	25.2

I_s, S_s: Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total-Strength I, and Service II) due to non-composite dead loads (in.⁴ and in.³).
I_{c(n)}, S_{c(n)}: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total-Strength I, and Service II) in uncracked sections, due to short-term composite live loads (in.⁴ and in.³).
I_{c(3n)}, S_{c(3n)}: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in.⁴ and in.³).
I_{e(cr)}, S_{e(cr)}: Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing f_s (Total-Strength I and Service II) in cracked sections, due to both short-term composite live loads and long-term composite dead loads (in.⁴ and in.³).
DC1: Un-factored non-composite dead load (kips/ft.).
M_{DC1}: Un-factored moment due to non composite dead load (kip-ft.).
DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).
M_{DC2}: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).
DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).
M_{DW}: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).
M_{L + IM}: Un-factored live load moment plus dynamic load allowance (impact) (kip ft.).
M_u (Strength I): Factored design moment (kip-ft.).
Φ_rM_n (Strength I) (ksi): 1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_{L + IM}

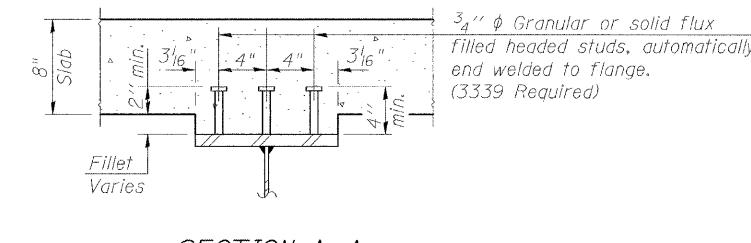
	Abut.	Pier
RDC1 (k)	22.6	75.0
RDC2 (k)	3.1	10.5
RDW (k)	7.7	25.5
R _L + IM (k)	72.0	120.4
R _{Total} (k)	105.4	231.4

Notes:

Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.

All diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted. Individual diaphragms at supports may be temporarily disconnected to install bearing anchor rods.

All structural steel beams shall conform to the requirements of AASHTO M 270 Grade 50W.



SECTION A-A

Φ_rM_n: Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).

f_s DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi).

M_{DC1} / S_{DC1}

f_s DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).

M_{DC2} / S_{DC2} or M_{DC1} / S_{DC1} as applicable.

f_s DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).

M_{DW} / S_{DW} or M_{DC1} / S_{DC1} as applicable.

f_s (L+IM): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).

M_{L + IM} / S_{L+IM} or M_{DC1} / S_{DC1} as applicable.

f_s (Service II): Sum of stresses as computed below (ksi).

f_s DC1 + f_s DC2 + f_s DW + 1.3 f_s (L + IM)

0.95R_bF_{yf}: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

f_s (Total)(Strength I): Sum of stresses as computed below (ksi)

1.25 (f_s DC1 + f_s DC2) + 1.5 f_s DW + 1.75 f_s L + IM

Φ_rF_n: Non-Compact composite positive or negative stress capacity for Strength I loading according to Article 6.10.7.2 (ksi).

V_r: Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

URS

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FILE NAME =	USER NAME = Brian K. Nicholson	DESIGNED - MJP	REVISED -
CHECKED - KWB	REVISED -		
PLOT SCALE =	DRAWN - BKN	REVISED -	
PLOT DATE =	CHECKED - KWB	REVISED -	

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

STRUCTURAL STEEL
STRUCTURE NO. 058-6026

SHEET NO. 11 OF 22 SHEETS

F.A.U. RTE*	SECTION	COUNTY	TOTAL SHEETS	sheet no.
7398	09-00905-00-BR	MACON	63	41
				CONTRACT NO. 95687

ILLINOIS FED. AID PROJECT