GEOTECHNICAL ENGINEERING REPORT SMART CORRIDOR IMPLEMENTATION DYNAMIC MESSAGE SIGNS ALONG IL 64 FROM SMITH/KAUTZ RD TO IL 50 PTB 199-002 COOK AND DUPAGE COUNTIES ILLINOIS

for Kimley-Horn and Associates, Inc. 111 W Jackson Blvd, Suite 1320 Chicago, IL 60604

> Submitted by Wang Engineering, Inc. 1145 North Main Street Lombard, IL 60148

> > Original Report: September 09, 2022 Revised Report: September 30, 2022 December 21, 2022 January 16, 2023 January 17, 2023

Wang KE225168/148-02-01, GIR

Technical Report Documentation Page

1. Title and Subtitle		2. Report Date		
Geotechnical Engineering Report, D	January 17, 2023			
West and East of I-355, West of IL 83 and East of I-290		3. Report Type □ SGR ⊠ GIR □ Draft ⊠ Final □ Revised		
4. Route / Section / County		5. Contract		
IL 64/2020-263-SUR, SW&TS/ Coo	bk and DuPage	D-91-081-21		
6. PSB / Item No.	7. Existing Structure Number(s)	8. Proposed Structure Number(s)		
199/002	NA	NA		
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11. Abstract				
	nated as DMS Location 1 through 4 alon	g IL 64, west and east of I-355, west		
of IL 83, and east of I-290 are pr	roposed.			
hard clay to silty clay loam f encountered medium stiff to hard Boring DMS-03 encountered bu boring encountered loose to very	brings DMS-01, DMS-03 and DMS-05 e fill material. Below the pavement or f d silty clay followed by loose to dense sa ried topsoil under the fill followed by stir d dense silty loam and possible weathered	Fill, Borings DMS-01 and DMS-02 nd, gravelly sand to silty loam.Fit to hard silty clay. At 31.6 feet bgs, 1 bedrock at 608.8 feet elevation.		
Boring DMS-05 encountered stin	ff to hard silty clay to silty clay loam to t	he boring termination depth.		
Boring DMS-01 encountered groundwater while drilling at an elevation of 694.6 feet and 655.6 feet after the drilling completion. Boring DMS-02 encountered groundwater while drilling at an elevation of 693.6 feet and 677.1 feet after drilling completion. Borings DMS-03 and DMS-04 did not encounter groundwater during drilling.				
Based on the results of the subsurface investigation, we recommend the sign structures be supported on drilled shaft foundations. For final drilled shafts design at DMS Location 1 and DMS Location 2, we recommend using lateral soil parameters. Recommended lateral soil modulus and soil strain parameters are provided in the report. IDOT Standard drawing as per IDOT Sign Structure Manual could be used for a sign structure at DMS Location 3 and DMS Location 4.				
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1.0 INTRODUCTION

This report presents foundation recommendations for the design and construction of four Dynamic Message Sign (DMS) structures along IL 64. This investigation was performed for IDOT Contract D-91-081-21. Based on the soil conditions revealed during our subsurface investigation, we are providing geotechnical recommendations for the design of drilled shafts to support the sign structures. A *Site Location Map* is presented as Exhibit 1.

The purpose of this investigation was to characterize the site soil and groundwater conditions, perform geotechnical engineering analyses, and provide recommendations for the design and construction of the proposed DMS structures.

1.1 Proposed Structure

Based on the drawing provided by Kimley-Horn and Associates, Inc (Kimley-Horn), we understand that four cantilever type DMS sing structures designated as DMS Location 1 to DMS Location 4 will be constructed along IL 64. DMS Location 1 and 2 are located west and east of I-355, respectively. DMS Location 3 is located along eastbound of IL 64 and 0.45 miles West of IL 83. DMS Location 4 is located 0.9 miles east of I-290.



2.0 SITE LOCATION

The project area is in Cook and DuPage Counties, Illinois. On the USGS *Lombard and Elmhurst Quadrangle 7.5 Minute Series* map, the project area is located at NW ¹/₄ of Sec. 1, NW ¹/₄ of Sec. 3, SW ¹/₄ of Sec. 31, SE ¹/₄ of Sec 31, Sections 1, and Tier 39, 40 N, Range 10, 11, 12 E of the Third Principal Meridian.

3.0 METHODS OF INVESTIGATION

3.1 Field Investigation

Our subsurface investigation consists of four sign structure borings designated as DMS-01 to DMS-03, and DMS-05, one at each sign structure location. Please note that structure DMS Location 3 initially proposed was canceled and moved to a new location. New DMS Location 3 is 0.45 miles west of IL 83 as shown in *Boring Location Plan* (Exhibit 2) and the reference boring is DMS-05. Borings DMS-01 and DMS-02 were drilled for structures designated as DMS Location 1 and 2, respectively. Boring DMS-03 was drilled for structure designated as DMS Location 4. The borings were drilled by Wang Engineering a Terracon Company (Wang) from August 9, 2022 to January 5, 2023. The as-drilled boring locations were surveyed by Wang with a mapping-grade GPS unit. Boring location data are presented in the *Boring Logs* (Appendix A). While the northing and easting surveyed with the GPS have a good precision (within +/- 6 inches), the elevations do not have always accurate readings. Sometimes the elevations are off by as much as 3 to 4 feet depending on the project location. Thus, boring elevations should be checked against site surveys. The as-drilled boring location *Plan* (Exhibit 2).

ATV and Truck-mounted drilling rig, equipped with hollow stem augers, were used to advance and maintain open boreholes to termination depths. Soil sampling was performed according to AASHTO T 206, *"Penetration Test and Split Barrel Sampling of Soils."* The soils were sampled at 2.5-foot intervals to 30 feet, and 5 feet thereafter to boring termination depths. Soil samples collected from each sampling interval were placed in sealed jars and transported to Wang Geotechnical Laboratory in Lombard, Illinois for further examination and laboratory testing.

Field boring logs, prepared and maintained by Wang geologists, include lithological descriptions, visual-manual soil (IDH Textural) classifications, results of Rimac and pocket penetrometer unconfined compressive strength tests, and results of Standard Penetration Tests (SPT) recorded as

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blows per 6 inches of penetration. The SPT N values (N-value), expressed as blows/foot, shown on the *Boring Logs* (Appendix A), is the sum of the second and third blows per 6 inches of penetration. Groundwater observations were made during and at the end of drilling operations. Due to safety considerations, boreholes were backfilled immediately upon completion with soil cuttings and/or bentonite chips, and where necessary, the pavement surface was restored to its original condition.

3.2 Laboratory Testing

All soil samples were tested in the laboratory for moisture content (AASHTO T265). Atterberg limits (AASHTO T89/T90) and particle size analyses (AASHTO T88) tests were performed on selected soil samples. Laboratory test results are shown in the *Boring Logs* (Appendix A) and in the *Laboratory Test Results* (Appendix B).

4.0 INVESTIGATION RESULTS

Detailed descriptions of the soil conditions encountered during our subsurface investigation are presented in the attached *Boring Logs* (Appendix A). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

4.1 General Lithological Profiles

The following sections present the soil conditions encountered during our subsurface investigation. The existing shoulder pavement consists 8-inch thick concrete or 2 to 4-inch thick asphalt over 7 to 10-inch thick concrete. The base consists of sand to sandy gravel or silty clay. Boring DMS-05 encountered 12-inch thick topsoil at the surface.

4.1.1 DMS Location 1 (Boring DMS-01)

Beneath the surface pavement, the boring encountered dense, black and gray sandy gravel base course followed by 2.5 feet thick, stiff black and gray silty clay fill. The silty clay fill has the Unconfined Compressive Strength (Qu) value of 1.9 tsf, and the moisture content value of 22%. Underneath the fill, boring encountered 3.9 feet of natural medium stiff silty clay. At an elevation of 696.2 feet, boring encountered 24.8 feet thick, loose to very dense, brown and gray sand, gravelly sand to loam with SPT-N values of 8 to more than 50 and moisture content values of 13 to 24. Deeper soil at an elevation of 671.4 feet shows medium dense to very dense, gray silty loam with SPT-N values of 27 to more than 50 with moisture content values of 8 to 13%.

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4.1.1 DMS Location 2 (Boring DMS-02)

Beneath the surface pavement, the boring encountered very stiff to hard, brown silty clay with a Qu value of 3.6 tsf, and a moisture content value of 21%. At an elevation of 720.8 feet, boring encountered 37.8 feet thick, loose to medium dense, brown gravelly loam with SPT-N values of 7 to 34 and moisture content values of 7 to 13%. Deeper soil at an elevation of 683.1 feet shows stiff to hard, gray silty clay with Qu values of 1.5 to 4.5 tsf and moisture content values of 11%.

4.1.3 DMS Location 3 (Boring DMS-05)

Beneath the topsoil, the boring encountered 7 feet thick, very stiff to hard clay to silty clay loam fill with Qu values of 2 to greater than 4.5 tsf, and moisture content values of 16 to 27%. Underneath the fill to the boring termination depths, boring encountered stiff to hard silty clay to silty clay loam with Qu values of 1.5 to 7.4 tsf and moisture content values of 12 to 18%.

4.1.4 DMS Location 4 (Boring DMS-03)

Beneath the surface pavement, the boring encountered stiff, brown and gray silty clay with Qu values of 1.0 to 1.8 tsf and moisture content values of 25 to 26% followed by 11-inch thick buried topsoil. At an elevation of 644.3 feet, boring encountered 4.1 feet thick, medium dense, brown and gray silt with SPT-N values of 11 and 13 and moisture content values of 20 and 21%. Stiff to hard, gay silty clay encountered at an elevation of 640.2 feet with Qu values of 1.4 to 4.5 tsf and moisture content values of 10 to 19%. A laboratory test result in this layer shows Liquid Limit (L_L) value of 29 and Plastic Limit (P_L) value of 14. Deeper soil at an elevation of 621.4 feet shows loose to very dense, gray silty loam with SPT-N values of 9 to more than 50. A laboratory test result on silty loam layer shows L_L value of 16 and P_L value of 11. Augur refusal and higher blow counts at 608.8 feet elevation shows possible bedrock at 44.7 feet bgs.

4.2 Groundwater Conditions

Boring DMS-01 encountered groundwater while drilling at an elevation of 694.6 feet (11 feet bgs) and 655.6 feet (50 feet bgs) after drilling completion.

Boring DMS-02 encountered groundwater while drilling at an elevation of 693.6 feet (33.5 feet bgs) and 677.1 feet (50 feet bgs) after drilling completion.

Borings DMS-03 and DMS-05 did not encounter groundwater during drilling. Boring DMS-03 recorded dry at the end of drilling. At the end of the drilling, groundwater was not recorded for Boring DMS-05 as rotary mud method was used.

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5.0 ANALYSES AND RECOMMENDATIONS

The following sections present the results of our analyses and recommendations for the proposed DMS sign structures.

5.1 Overhead Sign Structures

Based on preliminary drawings, Wang understands that four new DMS sign structures are proposed along IL 64. IDOT Sign Structure Manual (2012) Section 2.2 provides drilled shaft foundation for cantilever sign structure. The schedules provide standard drilled shaft diameter, embedment length, as well as reinforcement details based on the presence of mostly cohesive soil with an average Q_u of greater than 1.25 tsf. No provisions are provided for cohesionless soil.

Based on our evaluation of the soils encountered at the proposed DMS sign locations, the standard foundation schedules established by IDOT Sign Structure Manual (2012) Section 2.2 can be used for the foundation of the proposed sign structures at DMS Location 3 and 4; as shown in Table 1 satisfying IDOT criteria.

Borings encountered mostly granular soil at DMS Locations 1 and 2. Wang recommends site specific design at these locations using lateral soil parameters provided in Table 2 and 3. The final shaft embedment depths may vary depending on actual soils encountered during construction.



		Sign	Span	Soil Boring/	Standard
	Structure Location	Structure	Length	Drilled Depth	Foundation Criteria;
Name		Туре	(feet)	(feet)	Ave. $Q_u > 1.25$ tsf
DMS Location 1	IL Rte. 64 (North Avenue) West of I-355	Cantilever	NA	DMS-01/50	Mostly Granular
DMS Location 2	IL Rte. 64 (North Avenue) East of I-355	Cantilever	NA	DMS-02/50	Mostly Granular
DMS Location 3	IL Rte. 64 (North Avenue) West of IL 83	Cantilever	NA	DMS-05/50	Criteria Satisfied (Avg. Q _u = 2.95 tsf)
DMS Location 4	IL Rte. 64 (North Avenue) East of I-290	Cantilever	NA	DMS-03/45	Criteria Satisfied (Avg. Q _u = 2.1 tsf)

Table 1: Sign Structure Standard Foundation Criteria Evaluation Summary

Table 2: Recommended Soil Parameters for Laterally Loaded Drilled Shaft Analysis at DMS Location 1

Ref. Boring: DMS-01					
Soil Type / Layer Elevation	Moist Unit Weight, γ (pcf)	Undrained Shear Strength, c _u (psf)	Estimated Undrained Friction Angle, Φ (°)	Estimated Lateral Soil Modulus Parameter, k (pci)	Estimated Soil Strain Parameter, ɛ ₅₀ (%)
Stiff Silty Clay Fill El. 705.6 to 700.1	120	1900	0	600	0.7
Medium Stiff Silty Clay El. 700.1 to 696.2	120	1200	0	300	0.9
M Dese Sand El. 696.2 to 661.7	115	0	30	50	
Loose to Very Dense Sand to Gravelly Sand El. 661.7 ⁽¹⁾ to 671.4	53 ⁽²⁾	0	30	70	
M Dense to V Dense Silty Loam El. 671.4 to 655.6 ⁽³⁾	58 ⁽²⁾	3	32	100	
⁽¹⁾ Groundwater Elevation ⁽²⁾ Submerged Unit Weight					

⁽²⁾Submerged Unit Weight

⁽³⁾Boring termination depth

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Moist Unit Weight, γ (pcf)	Undrained Shear Strength, c _u (psf)	Estimated Undrained Friction Angle, Φ (°)	Estimated Lateral Soil Modulus Parameter, k (pci)	Estimated Soil Strain Parameter, ϵ_{50} (%)
120	3600	0	1300	0.5
115	0	30	50	
58 ⁽²⁾	0	32	95	
58 ⁽²⁾	2000	0	600	0.7
	Unit Weight, γ (pcf) 120 115 58 ⁽²⁾	Unit Weight, γ (pcf)Shear Strength, cu (psf)1203600115058 ⁽²⁾ 0	MoistUndrained ShearUndrained Friction Angle, Φ (°)Weight, γ (pcf)Strength, c_u (psf)Undrained Friction Angle, Φ (°)1203600011503058 ⁽²⁾ 032	Moist Unit Weight, γ (pcf)Undrained Shear (psf)Undrained Friction Angle, Φ (°)Estimated Lateral Soil Modulus Parameter, k (pci)1203600013001150305058 ⁽²⁾ 03295

Table 3: Recommended Soil Parameters for Laterally Loaded Drilled Shaft Analysis at DMS Location 2

Groundwater Elevation

⁽²⁾Submerged Unit Weight

⁽³⁾Boring termination depth



6.0 CONSTRUCTION CONSIDERATIONS

6.1 Drilled Shaft Construction

Foundation excavations should be performed in accordance with local, state, and federal regulations. The potential effect of ground movements upon nearby roadways and utilities should be considered on the design and during construction. The drilled shafts for sign structures support should be constructed in accordance with IDOT Standard Specification of Road and Bridge Construction Section 516 (2022), *Drilled Shafts*.

Groundwater was encountered in Borings DMS-01 and DMS-02. In addition, thick layer of granular soils were encountered in the soil borings. Wet method, temporary casing method, or combination of the two will be required for construction of drilled shafts where granular soils and groundwater was encountered in borings during and after drilling. The construction method should be adjusted or changed based on the soil and groundwater conditions encountered during construction of the drilled shafts.



7.0 QUALIFICATIONS

The analysis and recommendations submitted in this report are based upon data obtained from the soil borings performed at the locations indicated on the *Boring Locations Plans* (Exhibit 2). This report does not reflect any variations that may occur between borings or elsewhere on the site, variations whose nature and extent may not become obvious until late in the construction phase. If changes are planned to the proposed improvements, we should be timely informed so that the changes may be reviewed, and our recommendations adjusted accordingly.

It has been a pleasure to work with Kimley-Horn and Associates, Inc. in this project. Please do not hesitate to call if there are any questions, or if we can be of further service.

Respectfully Submitted,

WANG ENGINEERING, INC.

auf.

Ramesh KC, P.E. Geotechnical Engineer

engles Hadalo

Mohammed (Mike) Kothawala, P.E., D.GE Sr. Project Manager/Sr. Geotechnical Engineer



REFERENCES

IDOT (2012) Sign Structure Manual. Illinois Department of Transportation.IDOT (2022) Standard Specifications for Road and Bridge Construction. Illinois Department of Transportation.



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EXHIBITS

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APPENDIX A



Relative Density of Non-
Cohesive Soils

N-Blows/ 12 inches	Relative Density Term
0-3	Very Loose
4-9	Loose
10-29	Medium Dense
30-49	Dense
50-80+	Very Dense

Consistency of Cohesive Soils			
Unconfined Compressive Strength Qu, tsf	Consistency Term		
<0.25	Very Soft		
0.25-0.49	Soft		
0.50-0.99	Medium Stiff		
1.00-1.99	Stiff		
2.00-3.99	Very Stiff		
>4.00	Hard		

Rock Quality Designation (RQD) Very Poor 0-25% 25-50% Poor 50-75% Fair 75-90% Good 90-100% Excelent

LEGEND FOR BORING LOG

- SS = Split Spoon
- ST = Shelby Tube
- SPT = Standard Penetration Test
- = Unconfined Compressive Qu Strength
 - NP = Non Plastic
 - P = Pocket Penetrometer
 - S = Shear failure of sample, Rimac test
 - B = Bulge failure of sample,Rimac test
- SSA = Solid Stem Augers,
- HSA = Hollow Stem Augers,

Propo	rtional	Terms
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Trace	1-9	Pe
Little	10-19	ercent Dry Weigh
Some	20-34	ent ()ry ight
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Gradation Terminology

Boulders	>200mm		
Cobbles	200mm to 75mm		
Gravel	75mm to 2mm		
Sand	2-0mm to 0.074mm		
Silt	0.074mm to 0.002mm		
Clay	<0.002mm		

Relative Moisture Conditions					
Term	Description				
Dry	Dusty, No visible moisture				
Damp	Cohesives hard to mold;				
	Granulars do not flow easily				
Moist	Cohesives can be molded;				
	Granulars start to stick together				
Wet	Cohesives can be very easily molded and sticky;				
	Granulars stick together easily				
Saturated	Only granular soils;				
	Water drains freely from sample				

Relative Drilling Resistance (RDR) No Chatter - Very Easy Drilling 1 No Chatter - Easy Drilling 2

- Some Chatter Moderate Advancement 3
- 4 Frequent Chatter - Slow Advancement
- 5 **Constant Chatter - Very Slow Advanement**





Split Spoon

Sample Type Symbols



No Recovery



Rock Core

Shelby Tube

In-situ Vane Shear Test

SPT = Standard Penetration Test N Value is the sum of the second and the third numbers



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APPENDIX B

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APPENDIX C

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