## GENERAL NOTES Fasteners shall be AASHTO M164 Type 1, mechanically galvanized bolts. Bolts $7_8$ in. dia., holes $15_{16}$ in, dia., unless otherwise noted.

2. Calculated weight of Structural Steel: AASHTO M270 Grade 50 = 524,980 lbs AASHTO M270 Grade 36 = 66,650 lbs

3. No field welding is permitted except as specified in the contract documents.

- 4. Reinforcement bars shall conform to the requirements of ASTM A 706 Gr 60. See Special Provisions.
- 5. Reinforcement bars designated (E) shall be epoxy coated.
- 6. If the Contractor elects to use cantilever forming brackets on the exterior beams or girders, the brackets shall be placed at the same locations as required for the hardwood blocks in Article 503,06(b) of the Standard Specifications. If additional cantilever forming brackets are required, hardwood blocking shall be wedged between the exterior and first interior beam at each of these additional bracket locations.
- 7. Bearing seat surfaces shall be constructed or adjusted to the designated elevations within a tolerance of  ${}^{\prime}_{B}$  in. (0.01 ft.). Adjustment shall be made either by grinding the surface or by shimming the bearings.
- 8. Concrete Sealer shall be applied to the designated areas of the piers.
- 9. The existing structural steel coating contains lead. The Contractor shall take appropriate precautions to deal with the presence of lead on this project.
- 10. The Organic Zinc Rich Primer / Epoxy / Urethane Paint System shall be used for painting of new structural steel except where otherwise noted. The entire system shall be shop applied, with the exception of the exterior surfaces and the bottom of the bottom flange of fascia beams, masked off connection surfaces, field installed fasteners and damaged areas shall be touched up and finish coated in the field. The color of the final finish coat for all interior steel surfaces shall be Gray. Munsell No. 5B 7/1. The color of the final finish coat for the exterior and the bottom of the bottom flange of fascia beams shall be Blue, Munsell No. 10B 3/6. See Special Provision for "Cleaning and Painting New Metal Structures."
- 11. The embankment configuration shown shall be the minimum that must be placed and compacted prior to construction of the abutments.
- 12. The structural steel plates of the Bearing Assembly shall conform to the requirements of AASHTO M 270 Grade 50.
- 13. If the contractor chooses to alter the temporary cantilevered sheet piling design requirements shown on the plans, a design submittal including plan details and calculations will be required for review and acceptance by the Engineer.
- 14. The Contractor shall connect the first sheet to the existing abutment wall to ensure stability of sheets driven to the top of the existing footing. This connection shall be reviewed and accepted by the Engineer and included in the cost for Temporary Sheet Piling.



## STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION INDEX OF SHEETS

SH-1

SH-2

SH-3

. SH-4

SH-5

SH-6 SH-7

SH- 8

SH-9

SH-10

SH-11

SH-12

SH-13

SH~ 14

SH-15

SH-16

SH-17

SH-18 SH- 19

SH-20

SH-21

SH-22

SH-23 SH-24

SH-25

SH-26

SH-27 SH-28

SH-29

SH-30

	General Plan and Elevation		Approach Slab Details (NB)
	General Notes & Total Bill of Material		SB Framing Plan
	Construction Staging		NB Framing Plan
	Footing Layout	0.1.0.1	Steel Details 1 of 2
	Top of Slab Elevations 1 of 7		Steel Details 2 of 2
	Top of Slab Elevations 2 of 7	* SH- 36	Bearing Details 1 of 2
	Top of Slab Elevations 3 of 7	SH-37	Bearing Details 2 of 2
	Top of Slab Elevations 4 of 7	SH-38	East Abutment & Details (SB)
	Top of Slab Elevations 5 of 7	SH- 39	East Abutment & Details (NB)
	Top of Slab Elevations 6 of 7	SH-40	West Abutment & Details (SB)
	Top of Slab Elevations 7 of 7	'SH-41	West Abutment & Details (NB)
	Top of East Approach Slab Elevations (SB)	SH-42	East and West Abutment Removal
	Top of East Approach Slab Elevations (NB)	SH-43	Pier 1 (SB)
	Top of West Approach Slab Elevations (SB)	SH- 44	Pier 1 (NB)
	Top of West Approach Slab Elevations (NB)	SH-45	Pier 2 (SB)
	Southbound Deck Geometry Plan	SH-46	Pier 2 (NB)
	Northbound Deck Geometry Plan	SH-47	Pier 3 (SB)
	Deck Plan and Section (SB)	SH- 48	Pier 3 (NB)
	Deck Plan and Section (NB)	SH-49	Piers 1, 2 and 3 Removal
)	Parapet Details 1 of 2	SH-50	Temporary Concrete Barrier for Stage Construction
	Parapet Details 2 of 2	SH-51	Bar Splicer Assembly and Mechanical Splicer Details
2	Deck Details and Bill of Material	SH-52	HP Pile Details
ĩ	Bar Cutting Diagrams	SH-53	Cantilever Forming Brackets
1	Diaphraam at East Abutment (SB)	SH-54	Soil Boring Logs
į	Diaphragm at East Abutment (NB)	SH-55	Soil Boring Logs
	Diaphraam at West Abutment (SB)	SH-56	Soil Boring Logs
	Diaphraam at West Abutment (NB)		
2	Approach Slab Plan (SB)		and the second
2	Approach Slab Details (SB)	-	Bk. of Q. Pier. No. 1
	Approach Slab Plan (NB)		E. Abut.
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\<u>\*4″ ¢ Perforated</u>

Bk. of Abut. Drain Pipe Pipe Underdrains for S All drainage system components shall extend to 2'-0" from the end of each wingwall except an outlet pipe shall extend until intersecting with the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101)

## SECTION THRU INTEGRAL ABUTMENT

(Horiz. dim. @ Rt. L's)

Bridge Omission

1'-0" min.

PJF

(Full Length,

Rondea

Const.



SHEET NO. SH-2 SHEETS SH-56

\*Included in the cost of

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ITEM				
	UNIT	SUPER	SUB	TOTAL
of Existing Structures No. 3	Each			1
of Existing Structures No. 4	Each			1
e Shield	Sq.Yd	2,174		2,174
Excavation	Cu Yd		706	706
Structures	Cu Yd		1,071.0	1,071.0
Superstructure	Cu Yd	1,325.0		1,325.0
eck Grooving	Sq Yd	3,131		3,131
Encasement	Cu Yd		16.0	. 16.0
e Coat	Sq Yd	3,644		3,644
g and Erecting Structural Steel	L. Sum	0.53		0,53
ar Connectors	Each	18,198	100 400	18,198
ement Bars, Epoxy Coated	Pound	1,960	186,420 528	511,310 2,488
ers II 4 Inch	Each Sq Yd	1,900	1,174	1,174
g Steel Piles HP10x57	Ft Ft	1.1	1,914	1,174
iles	Ft		1,914	1,914
Steel HP10x57	Each		2	2
Sicci III 10851	Each	1	46	46
tes	Each	2		2
ic Bearing Assembly, Type I	Each		36	36
Bolts, 3/4"	Each		36	36
Bolts, 1"	Each	1	144	144
Sealer	Sq Ft		9,149	9,149
osite Wall Drain	Sq Yd		203	203
xcavation	Cu. Yd		2,990	2,990
ranular Embankment, Special	Cu Yd		336	336
y Sheet Piling	Sq Ft		5,012	5,012
erdrains for Structures 4".	F†		302	302
19°-16'-12"				
Skew	<b>V</b> .			
er No. 2 / Pier No. 3	N, N	· · · · · · · · · · · · · · · · · · ·	of V	
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4'-8 <sup>5</sup> 8", Sta 311+37.70 (I-57	$(\lambda + \lambda)$			
/Sta 1311+57.48 (IL		=		0
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		<u>,</u>		
<u>4'-8<sup>5</sup>8"</u>	4	1		
4'-8 <sup>5</sup> 8"		\ \ 		
$\frac{4' - 8^{5}_{B}"}{5' - 9^{l_{5}_{E}}"} + \frac{4' - 8^{9}_{l_{6}}}{4' - 8^{9}_{l_{6}}}"$	4	1	. 15. "	
<u>4'-8<sup>5</sup>8"</u>	4	47'	-1 <sup>5</sup> 8"	
$\frac{4' - 8^{5}_{6}"}{5' - 9^{15}_{16}"} + \frac{4' - 8^{9}_{16}"}{56' - 1^{3}_{4}"}$	4	47'	- <u>1<sup>5</sup>8</u> "	
$\frac{4' - 8^{5}_{B}"}{5' - 9^{l_{5}_{E}}"} + \frac{4' - 8^{9}_{l_{6}}}{4' - 8^{9}_{l_{6}}}"$	4	47'	- 1 <sup>5</sup> 8 "	
$\frac{4' - 8^{5}_{6}"}{5' - 9^{15}_{16}"} + \frac{4' - 8^{9}_{16}"}{56' - 1^{3}_{4}"}$	4	47'	- <u>1<sup>5</sup>8</u> "	
$\frac{4' - 8^{5}_{6}"}{5' - 9^{15}_{16}"} + \frac{4' - 8^{9}_{16}"}{56' - 1^{3}_{4}"}$	4	47'	- <u>1<sup>5</sup>8</u> "	
$\frac{4' - 8^{5}_{6}"}{5' - 9^{15}_{16}"} + \frac{4' - 8^{9}_{16}"}{56' - 1^{3}_{4}"}$	4	47'	- <u>1<sup>5</sup>8</u> "	
$\frac{4' - 8^{5}_{6}"}{5' - 9^{15}_{16}"} + \frac{4' - 8^{9}_{16}"}{56' - 1^{3}_{4}"}$	4	47'		
$\frac{4'-8^{5}_{\theta}"}{5'-9^{15}_{16}"} + \frac{4'-8^{9}_{16}"}{56'-1^{3}_{4}"}$ <u>ET SKETCH</u>	4	47'	-1 <sup>5</sup> 8"	
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$\frac{4'-8^{5}_{\theta}"}{5'-9^{15}_{16}"} + \frac{4'-8^{9}_{16}"}{56'-1^{3}_{4}"}$ <u>ET SKETCH</u>	4	47'		
$\frac{4'-8^{5}g''}{5'-9^{15}g''} + \frac{4'-8^{9}g''}{56'-1^{3}q''}$ <u>ET SKETCH</u>	4	47'		
$\frac{4'-8^{5}e''}{5'-9^{15}6''}$ $\frac{4'-8^{9}6''}{56'-1^{3}4''}$ $ET SKETCH$ $\frac{Edge of Deck}{Welded Wire/}$	2'-0'' <i>2'-</i> 0''	47.		
$\frac{4'-8^{5}g''}{5'-9^{15}g''} + \frac{4'-8^{9}g''}{56'-1^{3}q''}$ <u>ET SKETCH</u>	4	47'		
$\frac{4'-8^{5}e''}{5'-9^{15}6''}$ $\frac{4'-8^{9}6''}{56'-1^{3}4''}$ $ET SKETCH$ $\frac{Edge of Deck}{Welded Wire/}$	2'-0'' <i>2'-</i> 0''	47'		
$\frac{4' - 8^{5}g''}{5' - 9^{15}h''} + \frac{4' - 8^{9}h''}{56' - 1^{3}4''}$ $ET SKETCH$ $Edge of 2' - 0''$ $Deck$ $Welded Wire + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0''' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0'' + 0''' + 0'' + 0''' + 0''' + 0''' + 0''' + 0''' + 0'''' + 0'''' + 0'''' + 0''''''''$	2'-0'' <i>2'-</i> 0''	D Min		
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$\frac{4' - 8^{5} g''}{5' - 9^{15} g''} + \frac{4' - 8^{9} g''}{5' - 9^{15} g''} + \frac{4' - 8^{9} g''}{5' - 1^{3} 4''}$ $ET SKETCH$ $\frac{Edge of 2' - 0''}{Deck} + \frac{2' - 0''}{1 - 1^{3} 4''} + \frac{1}{5} f'' + 1$	2 <sup>7</sup> -0 <sup>77</sup> 4.1 (V:H)	D Min 1:2 Min	10'-0''	
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$\frac{4' - 8^{5} g''}{5' - 9^{15} g''} + \frac{4' - 8^{9} g''}{5' - 9^{15} g''} + \frac{4' - 8^{9} g''}{5' - 1^{3} 4''}$ $\frac{ET \ SKETCH}{ET \ SKETCH}$ $\frac{Welded \ Wire}{Fabric} + \frac{2' - 0''}{6''} + \frac{1}{6''} + \frac{1}{6'''} + \frac{1}{6'''} + \frac{1}{6'''} + \frac{1}{6'''} + \frac{1}{6''''} + \frac{1}$	2 <sup>2</sup> -0 <sup>2</sup> 42 42 42 42 42 42 42 42 42 42 42 42 42	Lie Min 1:2 Mi	10'-0'' N:HI fabric, per 100	sq. ft.
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$\frac{4'-8^{5}e''}{5'-9^{15}e''}$ $\frac{4'-8^{5}e''}{5'-9^{15}e''}$ $\frac{4'-8^{5}e''}{56'-1^{3}e''}$ $\frac{ET SKETCH}{Beck}$ $\frac{15}{Fabric}$ $\frac{15}{6''}$ $\frac{15}{56'-1^{3}e''}$ $\frac{15}{6''}$ $\frac{15}{6$	2 <sup>2</sup> -0 <sup>2</sup> 42 42 42 42 42 42 42 42 42 42 42 42 42	Lie Min 1:2 Mi	10'-0'' N:HI fabric, per 100	0,2,6, ft.
$\frac{4'-8^{5}e''}{5'-9^{15}e''}$ $\frac{4'-8^{7}e''}{56'-1^{3}e''}$ $ET SKETCH$ $\frac{Edge of 2'-0''}{Deck}$ $\frac{15}{Fabric}$ $\frac{15}{Fabric}$ $\frac{15}{6''}$ $\frac{15}{56'-1^{3}e''}$ $\frac{15}{6''}$ $\frac{15}$	2 <sup>2</sup> -0 <sup>2</sup> 42 42 42 42 42 42 42 42 42 42 42 42 42	Lie Min 1:2 Mi	10'-0'' N:HI fabric, per 100	sq. ft.
$\frac{4' - 8^{5} g''}{5' - 9^{15} g''} + \frac{4' - 8^{9} g''}{5' - 9^{15} g''} + \frac{4' - 8^{9} g''}{5' - 1^{3} 4''}$ $\frac{ET \ SKETCH}{ET \ SKETCH}$ $\frac{Welded \ Wire}{Fabric} + \frac{2' - 0''}{6''} + \frac{1}{6''} + \frac{1}{6'''} + \frac{1}{6'''} + \frac{1}{6'''} + \frac{1}{6'''} + \frac{1}{6''''} + \frac{1}$	2'-0" 4.1 (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V:H) (V	ded wire g 58 lbs.	10'-0'' N:HI fabric, per 100 WALL	sq. ft.
$\frac{4'-8^{5}e''}{5'-9^{15}e''}$ $\frac{4'-8^{5}e''}{56'-1^{3}e''}$ $ET SKETCH$ $\frac{Edge of 2'-0''}{Deck}$ $\frac{15}{Fabric}$ $\frac{15}{all is}$ $\frac{SECTION D-D}{6'}$ $\frac{15}{all is}$ $\frac{SECTION D-D}{6' all be reinforce}$ $6 in. x 6 in W4.0 x W4.$ $TYPICAL SECTION$ uctures.	2'-0" 4.1 (V:HI) d with weld o, weighing THRU S	ded wire g 58 ibs. SLOPE	10'-0'' fabric, per 100 WALL TES	
$\frac{4'-8^{5}e''}{5'-9^{15}e''}$ $\frac{4'-8^{5}e''}{56'-1^{3}e''}$ $ET SKETCH$ $\frac{Edge of 2'-0''}{Deck}$ $\frac{15}{Fabric}$ $\frac{15}{all is}$ $\frac{SECTION D-D}{6'}$ $\frac{15}{all is}$ $\frac{SECTION D-D}{6' all be reinforce}$ $6 in. x 6 in W4.0 x W4.$ $TYPICAL SECTION$ uctures.	2'-0" 4.1 (V:HI) d with weld o, weighing THRU S	ded wire g 58 ibs. SLOPE	10'-0'' fabric, per 100 WALL TES	
4'-85g"       4'-85g"         5'-9 <sup>15</sup> 6"       56'-134"         ET SKETCH         Beck       1         Welded Wire/       56'-134"         Beck       1         Welded Wire/       56'-134"         Section D-D       6''         all) is       SECTION D-D         Slopewall shall be reinforce         6 in. x 6 in W4.0 x W4.         TYPICAL SECTION         uctures.	2'-0" 4'-57 <sub>16</sub> " 4'-57 <sub>16</sub> "	ded wire g 58 lbs. SLOPE	10'-0'' fabric, per 100 WALL TES MATER	RIAL
$\frac{4'-8^{5}e''}{5'-9^{15}e''}$ $\frac{4'-8^{5}e''}{56'-1^{3}e''}$ $ET SKETCH$ $\frac{Edge of 2'-0''}{Deck}$ $\frac{15}{Fabric}$ $\frac{15}{all is}$ $\frac{SECTION D-D}{6'}$ $\frac{15}{all is}$ $\frac{SECTION D-D}{6' all be reinforce}$ $6 in. x 6 in W4.0 x W4.$ $TYPICAL SECTION$ uctures.	2'-0" 4'-57 <sub>16</sub> " 4'-57 <sub>16</sub> "	ded wire g 58 lbs. SLOPE	10'-0'' fabric, per 100 WALL TES MATER	RIAL
$\frac{4' \cdot 8^{5} 8''}{5' \cdot 9^{l_{5}} 6'} \frac{4' \cdot 8^{9} 6''}{56' \cdot 1^{3} 4''}$ $ET SKETCH$ $\frac{Edge of 2' \cdot 0''}{Deck}$ $\frac{10}{Fabric} 6'' \frac{1}{6'} \frac{1}$	2'-0" 4:1 4:1 (1:4) d with welk 0, weighing THRU S <u>GENER</u> <u>GENER</u> <u>FAL BIL</u> <u>FURE NO</u>	ded wire g 58 lbs. SLOPE AL NO L OF 0. 046	IO'-O'' fabric, per IOO WALL TES MATEF -0144	<u>RIAL</u> (S.B.)
<u>4'-8<sup>5</sup>8"</u> <u>5'-9<sup>15</sup>6"</u> <u>ET SKETCH</u> <u>ET SKETCH</u> <u>ET SKETCH</u> <u>ET SKETCH</u> <u>Etdge of 2'-0''</u> <u>Deck</u> <u>Welded Wire</u> <u>6''</u> <u>10</u> <u>10</u> <u>10</u> <u>10</u> <u>10</u> <u>10</u> <u>10</u> <u>10</u>	2'-0" 4:1 4:1 (1:4) d with welk 0, weighing THRU S <u>GENER</u> <u>GENER</u> <u>FAL BIL</u> <u>FURE NO</u>	ded wire g 58 lbs. SLOPE AL NO L OF 0. 046	IO'-O'' fabric, per IOO WALL TES MATEF -0144	<u>RIAL</u> (S.B.)
$\frac{4'-8^{5}g''}{5'-9^{15}_{16}} + \frac{4'-8^{9}_{16}}{56'-1^{3}_{4}} + \frac{56'-1^{3}_{4}}{56'-1^{3}_{4}} + 56'$	2'-0" 4:1 4:1 (1:4) d with welk 0, weighing THRU S <u>GENER</u> GENER TAL BIL TURE NO	ded wire g 58 lbs. SLOPE AL NO L OF 0. 046	IO'-O'' fabric, per IOO WALL TES MATEF -0144	<u>RIAL</u> (S.B.)
$\frac{4'-8^{5}g''}{5'-9^{15}6''}$ $\frac{4'-8^{9}6''}{5'-9^{15}6''}$ $\frac{Edge of 2'-0''}{56'-1^{3}4''}$ $\frac{Edge of 2'-0''}{56'-1^{3}4''}$ $\frac{Edge of 2'-0''}{56'-1^{3}4''}$ $\frac{15}{56'-1^{3}4''}$ $\frac{15}{56'-$	2'-0" 4:1 4:1 (1:4) d with welk 0, weighing THRU S <u>GENER</u> GENER TAL BIL TURE NO	ded wire g 58 lbs. SLOPE AL NO L OF D. 046 NO. 04	10'-0'' fabric, per 100 WALL TES MATEF -0144 6-0145	<u>RIAL</u> (S.B.)
$\frac{4'-8^{5}g''}{5'-9^{15}6''}$ $\frac{4'-8^{9}6''}{56'-1^{3}4''}$ $\frac{Edge of \qquad 2'-0''}{Deck}$ $\frac{2'-0''}{Fabric}$ $\frac{6''}{6''}$ $\frac{1}{6''}$	2'-0" 4:1 4:1 (1:4) d with welk 0, weighing THRU S <u>GENER</u> GENER TAL BIL TURE NO	ded wire g 58 lbs. SLOPE AL NO L OF 0. 046	10'-0'' fabric, per 100 WALL TES MATEF -0144 6-0145 × 100	<u>RIAL</u> (S.B.) 5 (N.B.
$\frac{4'-8^{5}8''}{5'-9^{15}6''}$ $\frac{4'-8^{9}6''}{56'-1^{3}4''}$ $ET SKETCH$ $\frac{Edge of 2'-0''}{Deck}$ $\frac{2'-0''}{Deck}$ $\frac{15}{6''}$ $$	2'-0" 4:1 4:1 (1:4) d with welk 0, weighing THRU S <u>GENER</u> GENER TAL BIL TURE NO	ded wire g 58 lbs. SLOPE AL NO L OF D. 046 NO. 04	10'-0'' fabric, per 100 WALL TES MATEF -0144 6-0145 Y TO SHE	<u>RIAL</u> (S.B.) 5 (N.B.,

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