

STRUCTURE GEOTECHNICAL REPORT

BRIDGE REPLACEMENT I-72 OVER I-57

Section (10-33HB-2)BR
Champaign County, Illinois
Job No. P-95-008-21
Contract No. 70254
PTB 201-035

Existing Structure No. 010-0034 (EB)/010-0035 (WB)
Proposed Structure No. 010-0296 (EB)/010-0297 (WB)

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1.0 Project Description and Scope

1.1 Introduction

The geotechnical investigation summarized herein was performed for the proposed bridges at I-72 over I-57 in Champaign County, Illinois. See Appendix A for Location Map. The purpose of this report is to provide geotechnical design and construction recommendations to aid in the structure planning, final design plans and specification preparation.

1.2 Existing Structure Information

Built in 1965, the existing dual structures (SN 010-0034 EB and SN 010-0035 WB) were originally constructed as a four span continuous steel beam superstructure on pile supported stub abutments and reinforced concrete three column hammerhead piers founded on spread footings. In 1988, the wearing surface and bridge railings were replaced and the deck carrying shoulders were replaced and widened. The face to face of parapets width varies from 48'-0" to 52'-1 $\frac{1}{8}$ " with 3'-0" outer and 5'-0" inner shoulders, two 12'-0" thru lanes and a varying width acceleration/deceleration lane for adjacent ramps. Both structures are 260'-0" back-to-back of abutments with a 1°-22'-45" right ahead skew to the local tangent and are located on a 1,800-foot crest vertical curve. The reconstructed superstructure consists of 9 composite steel beam lines of 36WF160. The reinforced concrete deck thickness is 7".

SN 010-0034 has a sufficiency rating of 64.2 with a deck rating of 4 in poor condition with advanced deterioration, superstructure rating of 4 in poor condition with advanced deterioration, and a substructure rating of 6 in satisfactory condition with minor deterioration.

SN 010-0035 has a sufficiency rating of 63.6 with a deck rating of 4 in poor condition with advanced deterioration, superstructure rating of 4 in poor condition with advanced deterioration, and a substructure rating of 6 in satisfactory condition with minor deterioration.

1.3 Proposed Structure Information

The proposed replacement structures are 4 span bridges with W33 rolled steel beams supporting an 8" concrete deck on a 1°-22'-45" right ahead skew. Proposed back-to-back abutment lengths are 272'-4" with span lengths of 51'-10" – 84'-4" – 84'-4" – 51'-10". The structures consist of 9 beams with 6 spaces at 7'-1" and 2 spaces at 10'-2 $\frac{3}{8}$ " to 14'-2" (varies), for an overall width of 58'-10" to 62'-10" (varies) out-to-out. The roadway cross sections consist of a 6'-0" shoulder, 16'-0' to 20'-0" merge lane, 24'-0" roadway, and 10'-0" shoulder. The structures will be replaced utilizing cross over traffic lanes. For further proposed structure information, see Appendix B for Type, Size, and Location Plan (TS&L).

2.0 Field Exploration

2.1 Subsurface Exploration and Testing

The subsurface investigation consisted of 10 borings (EB-1 through EB-5, and WB-1 through WB-5) drilled by Millennia Professional Services on 11/10/2022. EB-1, EB-2, WB-1, and WB-2 were taken near the west abutment of the structures, WB-3 and EB-3 were taken in the I-57 Median, and EB-4, EB-5, WB-4, and WB-5 were taken near the east abutment of the structures. Soil boring



exploration was performed using a hollow stem auger and/or mud rotary drilling techniques. See Appendix C for Subsurface Data Profile Plot and Appendix D for Soil Boring.

Table 2.1 - Boring Log Summary

Location	Boring No.	Station	Offset	Ground Surface Elevation
SN 010-0296	EB-1	1958+80 (I-72)	17' RT - CL I-72	760.8
SN 010-0296	EB-2	481+25 (I-57)	75' LT - CL I-57	739.8
SN 010-0296	EB-3	480+25 (I-57)	7' LT - CL I-57	737.7
SN 010-0296	EB-4	481+25 (I-57)	78' RT - CL I-57	739.8
SN 010-0296	EB-5	1962+50 (I-72)	18' RT - CL I-72	760.3
SN 010-0297	WB-1	1958+80 (I-72)	17' LT - CL I-72	760.6
SN 010-0297	WB-2	482+40 (I-57)	74' LT - CL I-57	740.1
SN 010-0297	WB-3	481+45 (I-57)	3' LT - CL I-57	739.9
SN 010-0297	WB-4	482+30 (I-57)	75' RT - CL I-57	740.0
SN 010-0297	WB-5	1962+50 (I-72)	18' LT - CL I-72	760.1

2.2 Subsurface Conditions

The groundwater conditions at each soil boring varies. See Table 2.2 below. Temperature, seasonal variations, and recent rainfall conditions may influence the levels of groundwater table. Without extended periods of observation, the measurement of groundwater conditions herein may not give a true indication of typical groundwater levels. Volume of water depends on the permeability of the soils.



Table 2.2 – Groundwater Conditions Summary

Location	Boring No.	First Encounter	Upon Completion	After 24 Hours
SN 010-0296	EB-1	682.8	720.8	-----
SN 010-0296	EB-2	726.8	-----	-----
SN 010-0296	EB-3	-----	-----	-----
SN 010-0296	EB-4	-----	-----	-----
SN 010-0296	EB-5	721.3	720.3	-----
SN 010-0297	WB-1	707.6	-----	-----
SN 010-0297	WB-2	714.1	-----	-----
SN 010-0297	WB-3	700.9	-----	-----
SN 010-0297	WB-4	-----	-----	-----
SN 010-0297	WB-5	734.1	-----	-----

SN 010-0296 – Borings EB-1 and EB-5 encountered Silty Clay to Silty Clay Loam for approximately the first 80 feet of drilling with SPT (N) values from 5 to 20, Qu values of 1.2 to NC (no recovery) and moisture contents ranging between 9% and 22%. From Depths 80 to 100 feet the soil was Silty Loam to Silty Clay Loam, with SPT (N) Values from 59 to 50/2”, Qu values of 1.5 to NC, and moisture contents ranging between 6% to 13%.

Borings EB-2, EB-3, and EB-4 encounters Silty Clay and Silty Clay Loam to approximately 55 feet of drilling, with SPT (N) values from 4 to 26, Qu values of 1.4 to 8.1, and moisture contents ranging between 7% and 27%. Between 55 and 75 feet of drilling the soil was Silty Clay and Silty Clay Loam, with SPT (N) values from 43 to 93, Qu values of 3.5 to 11.3, and moisture contents ranging between 9% and 17%. From 75 to 100 feet of drilling the soils varied from Sand, Silt, and Sandy Loam, with SPT (N) values from 50/5.5” to 50/3”, Qu values of NC, and with no recovery on most moisture contents, moisture contents that were able to be recovered ranged from 18% to 20%.

SN 010-0297 – Borings WB-1 and WB-5 encountered Silty Clay to Silty Clay Loam for approximately the first 80 feet of drilling with SPT (N) values from 7 to 22, Qu values of 1.4 to NC (no recovery) and moisture contents ranging between 11% and 27%. From Depths 80 to 100 feet the soil was Silty Loam to Silty Clay Loam, with SPT (N) Values from 51 to 50/3.5”, Qu values of 8.7 to NC, and moisture contents ranging between 10% to 18%.

Borings WB-2, WB-3, and WB-4 encounters Silty Clay and Sand to approximately 55 feet of drilling, with SPT (N) values from 7 to 30, Qu values of 1.2 to 7.0, and moisture contents ranging between 10% and 26%. Between 55 and 75 feet of drilling the soil was Silty Clay, with SPT (N) values from 50 to 90, Qu values of 5.0 to 12.1, and moisture contents ranging between 8% and 18%. From 75 to 100 feet of drilling the soils varied from Sand, Silt, and Sandy Clay, with SPT (N) values from 44 to 50/2.5”, Qu values of 1.4 to NC, and with moisture contents that ranged from 18% to 23%.

For a more detailed representation of the subsurface conditions, see Appendix C and Appendix D.



3.0 Geotechnical Evaluations and Recommendations

3.1 Settlement

Based on the provided plan and profile, the anticipated difference between the existing and proposed elevations at the abutments is less than 1 foot. From preliminary settlement calculations, the proposed structure settlement results in less than 0.4 inches. Per IDOT Geotechnical Manual Section 6.9.2, driven pile capacity need not account for downdrag if total settlement of soil around the piling is less than 0.4 inches.

Regarding settlement of approach slabs, one end of the slab is supported by the pile supported abutment. The other end of the slab is supported by the existing embankment subgrades. Provided proper compaction according to IDOT Standard Specifications is performed during construction, settlement of the approach slab is not a concern.

3.2 Slope Stability

As previously discussed herein, the difference in proposed profile grade and embankment from the existing is minimal. The proposed 1:2 (V:H) sideslopes match the existing sideslopes and the height of the proposed slope is approximately 22 feet. The critical fill is generally stiff silty clay with an average SPT (N) value of 12 and an average Qu value of 3.2 tsf. Using the general rule of thumb equation below, determine a preliminary assessment of the slope stability factor of safety (FOS).

$$FOS = 6c/\gamma h = 6(3,200 \text{ psf})/[(120 \text{ pcf})(22')] = 7.2$$

A preliminary FOS of 7.2 is greater than the minimum FOS of 1.5. As validation, no known issues or concerns are present or have been present at the existing slopes which have been in place for over 57 years. In addition, the existing piles supporting the abutments will remain in place and increase the nominal slope stability FOS by intersecting the circular failure planes. For the reasons discussed, a slope stability analysis was not performed as slope stability is not considered a concern given the circumstances at this bridge.

3.3 Seismic Considerations

LRFD Seismic Soil Site Class Definition was determined based on the methodology described in IDOT AGMU 9.1 and the IDOT BBS 149 form for Seismic Site Class Determination. See Appendix E for determination.

Further seismic parameters were determined using the figures and tables provided in AASHTO LRFD Bridge Design Specifications, Article 3.10 for Earthquake Effects, EQ. These parameters are based on a 1000 Year Return Period with a Probability of Exceedance of 7% in 75 years. See table below for a summary of seismic parameters.



Table 3.1 - Summary of Seismic Parameters

Parameter	Value
Seismic Soil Site Class	C
Spectral Acceleration Coefficient at period of 0.2 sec., S _s	0.146g
Spectral Acceleration Coefficient at period of 1.0 sec., S ₁	0.056g
Site Factor, Short Period, F _a	1.2
Site Factor, Long Period, F _v	1.7
Design Spectral Acceleration at 0.2 sec. (SDS)	0.175g
Design Spectral Acceleration at 1.0 sec. (SD1)	0.095g
Seismic Performance Zone	SPZ 1

The Spectral Acceleration Coefficient at T=1.0 sec. (SD1) and Seismic Performance Zone were confirmed using Bridge Manual Planning Section 2.3.10.3.

3.4 Scour

Scour is not applicable because this is a grade separation structure.

3.5 Mining Activity

Reviewing the Illinois State Geological Survey (ISGS) County Coal Data for Champaign County, no mining activity is present at the bridge location.

3.6 Lateral Load Analysis

The tables below provide soil parameters to structural engineer for lateral or displacement analysis of the foundations. The values were estimated based on the descriptions given in the soil boring logs. Full cohesion was used with a friction angle of 0 degrees for cohesive soils. No specific analyses were performed on the soil to determine the estimated parameters.



Table 3.2 – Soil Parameters for Lateral Load Analysis at SN 010-0296 W Abut. (EB-1)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff to Very Stiff Silty Clay	125	1.2	0	300	0.007
Stiff Silty Clay Loam	125	2.3	0	300	0.007
Medium Stiff Silty Clay	125	1.7	0	300	0.007
Stiff to Very Stiff Silty Clay Loam	125	2.1	0	300	0.007
Medium Stiff to Very Stiff Silty Clay	125	1.9	0	300	0.007
Hard Silty Clay Loam	130	12.1	0	500	0.005
Hard Silt Loam	145	0.0	35	-	0.001

Table 3.3 – Soil Parameters for Lateral Load Analysis at SN 010-0296 Pier 1 (EB-2)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff Silty Clay Loam	125	2.5	0	300	0.007
Medium Stiff to Stiff Silty clay	125	5.0	0	300	0.007
Very Stiff Silty Clay	125	3.4	0	300	0.007
Hard Silty Clay Loam	130	9.7	0	500	0.005
Very Dense Sand	150	0.0	45	-	0.001
Hard Silt	145	0.0	35	500	0.005
Very Dense Sand	150	0.0	45	-	0.001

Table 3.4 – Soil Parameters for Lateral Load Analysis at SN 010-0296 Pier 2 (EB-3)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Medium Dense Sand	125	0.0	30	300	0.007
Stiff to Very Stiff Silty Clay	125	3.3	0	300	0.007
Very Dense Sandy Loam	150	0.0	45	-	0.001
Very Dense Sand	150	0.0	45	-	0.001



Table 3.5 – Soil Parameters for Lateral Load Analysis at SN 010-0296 Pier 3 (EB-4)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff Silty Clay Loam	125	2.9	0	300	0.007
Medium Stiff to Hard Silty Clay	125	1.9	0	300	0.007
Hard Silt	145	0.0	35	500	0.005
Very Dense Sand	150	0.0	45	-	0.001

Table 3.6 – Soil Parameters for Lateral Load Analysis at SN 010-0296 E Abut. (EB-5)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff to Very Stiff Silty Clay Loam	125	3.4	0	300	0.007
Medium Stiff to Stiff Silty Clay	125	2.4	0	300	0.007
Medium Dense Sand	125	0.0	30	-	0.007
Stiff to Very Stiff Silty Clay	125	4.4	0	300	0.005
Hard Silty Loam	130	-	0	500	0.005
Hard Silty Clay Loam	130	12.1	0	500	0.005
Hard Silty Clay	130	10.9	0	500	0.005
Hard Silty Clay Loam	130	0.0	30	500	0.005
Very Dense Sand	150	0.0	45	-	0.001

Table 3.7 – Soil Parameters for Lateral Load Analysis at SN 010-0297 W Abut. (WB-1)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff Silty Clay Loam	125	2.1	0	300	0.007
Stiff Silty Clay	125	3.5	0	300	0.007
Stiff Silty Clay Loam	125	3.2	0	300	0.007
Medium Stiff to Stiff Silty Clay	125	2.7	0	300	0.007
Very Stiff Silty Clay Loam	130	4.5	0	300	0.007
Stiff to Very Stiff Silty Clay	130	2.3	0	300	0.007
Soft Silty Clay Loam	120	0.2	0	100	0.01
Medium Dense Sand	125	0.0	30	-	0.007



Stiff to Very Stiff Silty Clay	130	4.9	0	300	0.007
Hard Silty Clay Loam	130	8.7	0	500	0.005
Hard Silty Clay	130	9.3	0	500	0.005

Table 3.8 – Soil Parameters for Lateral Load Analysis at SN 010-0297 Pier 1 (WB-2)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff Silt Loam	125	0.0	30	300	0.007
Stiff to Very Stiff Silty Clay	125	3.3	0	300	0.007
Very Stiff Sandy Loam	130	0.0	30	500	0.005
Very Stiff Silty Clay	125	0.6	0	300	0.007
Very Stiff Silt	125	0.0	30	500	0.005
Very Stiff to Hard Silty Clay	130	4.5	0	500	0.005
Very Dense Sand	150	0.0	45	-	0.001
Hard Silt	145	1.4	0	500	0.005

Table 3.9 – Soil Parameters for Lateral Load Analysis at SN 010-0297 Pier 2 (WB-3)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff Sandy Clay	125	2.4	0	300	0.007
Medium Dense Sand	125	0.0	30	-	0.007
Medium Stiff to Stiff Silty Clay	125	2.5	0	300	0.007
Medium Dense Sand	125	0.0	30	300	0.007
Stiff to Hard Silty Clay	125	3.0	0	500	0.005
Hard Silt	145	0.0	35	500	0.005
Very Dense Sand	150	0.0	45	-	0.001



Table 3.10 – Soil Parameters for Lateral Load Analysis at SN 010-0297 Pier 3 (WB-4)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Medium Stiff to Very Stiff Silty Clay	125	1.2	0	300	0.007
Medium Dense Sand	125	0.0	30	-	0.001
Very Stiff to Hard Silt	130	3.5	0	500	0.005
Hard Silty Clay	135	10.3	0	500	0.005
Very Dense Sand	150	0.0	45	-	0.001
Hard Silt	145	4.2	0	500	0.005
Hard Silty Clay	135	4.6	0	500	0.005

Table 3.11 – Soil Parameters for Lateral Load Analysis at SN 010-0297 E Abut. (WB-5)

Soil Description	γ (pcf)	c' (psf)	θ (deg.)	K (pci)	ϵ_{50}
Stiff Silty Clay	125	1.4	0	300	0.007
Stiff Sandy Clay Loam	125	4.1	0	300	0.007
Medium Stiff to Stiff Silty Clay	125	2.1	0	300	0.007
Hard Silt Loam	145	0.0	35	500	0.005
Hard Silty Clay	145	11.5	0	500	0.005

3.7 Liquefaction

According to IDOT AGMU Memo 10.1, liquefaction is not applicable in Seismic Performance Zone 1.

4.0 Foundation Recommendations

4.1 Integral Abutment Feasibility

Integral abutments are preferred to eliminate joints in the bridge decks, decreasing maintenance costs and increasing service life. The proposed structure length typically fits in the range of applicability for integral abutments; however, the soil at a critical depth of 10 feet below the abutment is very stiff (Weighted unconfined compressive strength, $Q_u > 3.0$ tsf). According to the IDOT Bridge Manual 3.8.3-Note 21, the integral abutment study only pertains to soils with Q_u less than 3.0 tsf.



To allow the use of integral abutments when Q_u exceeds 3.0 tsf, the pile locations may be pre-cored to 10 ft below the bottom of abutment and backfilled with bentonite pellets, which reduces the soil pressures on the pile during expansion and contraction. To simulate the effects of bentonite, assume $Q_u = 1.5$ tsf over the critical depth. The bentonite backfill option satisfies integral abutment applicability and is recommended at each abutment.

For results of the preliminary Integral Abutment Feasibility Analysis, see Appendix F. The designer shall verify integral abutment feasibility analysis with final configuration. Bridge Manual General Note #38 shall be placed on the appropriate abutment plan sheets. A 24" diameter precored hole shall be used for all metal shell piles. See IDOT Bridge Manual 3.8.3 for further integral abutment design guidance.

4.2 Abutment Foundation Type

Preliminary superstructure loads for the proposed structure configuration discussed above were provided by Veenstra & Kimm Inc. See tables below for total factored loads at each substructure. These loads include the approach slab and abutment self-weight.

Table 4.1 – SN 010-0296 Abut. Load

Location	Total Factored Reaction (k)
W. Abut.	1,550
E. Abut.	1,550

Table 4.2 – SN 010-0297 Abut. Load

Location	Total Factored Reaction (k)
W. Abut.	1,550
E. Abut.	1,550

Per the preliminary TS&L, integral abutments are anticipated with the bottom of the west abutment at Elev. 753.87 (W.B.) and Elev. 753.81 (E.B.) and bottom of east abutment at Elev. 753.52 (W.B.) and 753.56 (E.B.).

The use of H-piles and metal shell piles were both evaluated. While hard till is present at approximately 80 feet below the surface, the soil above provides opportunity to develop side friction and achieve sufficient axial resistance with a much shorter pile. H-piles have a smaller relative cross sectional displacement when driven and are typically considered a non-displacement pile; while metal shell piles have a larger relative cross sectional displacement when driven and are considered a more effective displacement pile. Metal shell piles will develop an equivalent required bearing at shorter pile lengths than H-piles in friction soil situations. Thus, metal shell piles are the more effective pile for the given conditions.

Tables 4.3 through 4.6 below summarize the nominal required bearing (R_N), factored resistance available (R_F), estimated pile length and estimated pile tip elevation for the strength limit state. R_N indicates the resistance of the pile during driving, which assists the Contractor from causing damage to the pile. R_F represents the net long term axial geotechnical resistance available to support the factored structure loads. The estimated pile lengths include a 2 foot embedment into the abutment. Analyses have been performed using the IDOT Static Method of Estimating Pile Length. See Appendix G.



The factored resistance available values shown in the tables are intended to provide the designer with a range of feasible options for the anticipated vertical loading. Piles shall be evaluated for lateral resistance in final design. IDOT integral abutment policy requires one pile under each beam. One test pile is recommended at each abutment location. Due to the presence of stiff cohesive materials, pile shoes (conical tips) are recommended.

Table 4.3 – Pile Capacity at SN 010-0296 West Abutment (EB-1) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	297	163	49	706.8
	337	185	54	701.8
	378	208	59	696.8
	392	215	62	693.8
MS 14x0.250 (Max. R_N = 459 Kips)	349	192	49	706.8
	399	219	54	701.8
	447	246	59	696.8
	459	252	62	693.8
MS 14x0.312 (Max. R_N = 570 Kips)	447	246	59	696.8
	477	263	64	691.8
	510	280	69	686.8
	527	290	74	681.8
	570	314	80	675.8
MS 16x0.312 (Max. R_N = 655 Kips)	517	285	59	696.8
	549	302	64	691.8
	586	322	69	686.8
	603	332	74	681.8
	655	360	80	675.8



Table 4.4 – Pile Capacity at SN 010-0296 East Abutment (EB-5) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	290	160	46	709.5
	327	180	49	706.5
	380	209	54	701.5
	392	215	56	699.5
MS 14x0.250 (Max. R_N = 459 Kips)	346	190	46	709.5
	389	214	49	706.5
	451	248	54	701.5
	459	252	56	699.5
MS 14x0.312 (Max. R_N = 570 Kips)	346	190	46	709.5
	389	214	49	706.5
	451	248	54	701.5
	523	287	59	696.5
	570	314	62	693.5
MS 16x0.312 (Max. R_N = 655 Kips)	404	222	46	709.5
	454	250	49	706.5
	525	289	54	701.5
	608	335	59	696.5
	655	360	62	693.5

Table 4.5 – Pile Capacity at SN 010-0297 West Abutment (WB-1) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	274	151	42	713.8
	287	158	47	708.8
	392	215	52	703.8
MS 14x0.250 (Max. R_N = 459 Kips)	324	178	42	713.8
	335	185	47	708.8
	459	252	52	703.8
MS 14x0.312 (Max. R_N = 570 Kips)	324	178	42	713.8
	335	185	47	708.8
	540	297	52	703.8
	570	314	54	701.8
MS 16x0.312 (Max. R_N = 655 Kips)	376	207	42	713.8
	384	211	47	708.8
	655	360	52	703.8

Table 4.6 – Pile Capacity at SN 010-0297 East Abutment (WB-5) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. $R_N = 392$ Kips)	271	149	43	712.5
	319	175	48	707.5
	366	201	53	702.5
	392	215	55	700.5
MS 14x0.250 (Max. $R_N = 459$ Kips)	323	178	43	712.5
	379	208	48	707.5
	434	239	53	702.5
	459	252	55	700.5
MS 14x0.312 (Max. $R_N = 570$ Kips)	379	208	48	707.5
	434	239	53	702.5
	490	269	58	697.5
	545	300	63	692.5
	570	314	70	685.5
MS 16x0.312 (Max. $R_N = 655$ Kips)	441	242	48	707.5
	504	277	53	702.5
	567	312	58	697.5
	631	347	63	692.5
	655	360	70	685.5

4.3 Pier Foundation Type

Preliminary superstructure loads for the proposed structure configuration discussed above were provided by Veenstra & Kimm Inc. See tables below for total factored loads at each substructure including self weight.

Table 4.7 – SN 010-0296 Pier Load

Location	Total Factored Reaction (k)
Pier 1	3,000
Pier 2	3,400
Pier 3	3,000

Table 4.8 – SN 010-0297 Pier Load

Location	Total Factored Reaction (k)
Pier 1	3,000
Pier 2	3,400
Pier 3	3,000

A shallow foundation (spread footing) and deep foundation (pile supported spread footing) were investigated for the proposed pier foundation type. While the existing piers are founded on spread footings, the proposed design vertical and lateral loadings including the 600 kip vehicular collision force are greater than the existing design conditions. Thus, a pile supported footing is anticipated to be more adequately suited foundation type. In addition, driven piles are recommended at the abutments so pile driving equipment will already be mobilized.

Per the preliminary TS&L, the proposed piers are multi-column with 2 rows of piles in the footing with the bottom of footing near the bottom of existing pier footing. The number of pile rows shall be verified in final design. Similar to the abutments, metal shell piles are considered more effective than H-Piles for the given conditions.

Tables 4.9 through 4.14 below summarize the nominal required bearing (R_N), factored resistance available (R_F), estimated pile length and estimated pile tip elevation. R_N indicates the resistance of the pile during driving, which assists the Contractor from causing damage to the pile. R_F represents the net long term axial geotechnical resistance available to support the factored structure loads. The estimated pile lengths include a 1 foot embedment into the pier footing. Analysis has been performed using the IDOT Static Method of Estimating Pile Length. See Appendix G.

The factored resistance available values shown in the tables are intended to provide the designer with a range of feasible options for the anticipated vertical loading. Piles shall be evaluated for lateral resistance in final design. One test pile is recommended at each pier location. Due to the presence of stiff cohesive materials, pile shoes (conical tips) are recommended.

Table 4.9 – Pile Capacity at SN 010-0296 Pier 1 (EB-2) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	301	165	27	705.5
	326	179	32	700.5
	354	195	37	695.5
	392	215	38	694.5
MS 14x0.250 (Max. R_N = 459 Kips)	359	198	27	705.5
	384	211	32	700.5
	416	229	37	695.5
	459	252	38	694.5
MS 14x0.312 (Max. R_N = 570 Kips)	384	211	32	700.5
	416	229	37	695.5
	488	269	42	690.5
	570	314	48	684.5
MS 16x0.312 (Max. R_N = 655 Kips)	442	243	32	700.5
	479	264	37	695.5
	568	312	42	690.5
	655	360	48	684.5

Table 4.10 – Pile Capacity at SN 010-0296 Pier 2 (EB-3) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	285	157	39	693.5
	321	176	44	688.5
	348	191	49	683.5
	392	215	54	678.5
MS 14x0.250 (Max. R_N = 459 Kips)	335	184	39	693.5
	379	209	44	688.5
	409	225	49	683.5
	459	252	54	678.5
MS 14x0.312 (Max. R_N = 570 Kips)	335	184	39	693.5
	379	209	44	688.5
	409	225	49	683.5
	570	314	54	678.5
MS 16x0.312 (Max. R_N = 655 Kips)	386	212	39	693.5
	439	241	44	688.5
	471	259	49	683.5
	655	360	54	678.5

Table 4.11 – Pile Capacity at SN 010-0296 Pier 3 (EB-4) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	248	136	37	695.5
	311	171	42	690.5
	332	182	47	685.5
	392	215	52	680.5
MS 14x0.250 (Max. R_N = 459 Kips)	292	161	37	695.5
	374	205	42	690.5
	391	215	47	685.5
	459	252	52	680.5
MS 14x0.312 (Max. R_N = 570 Kips)	292	161	37	695.5
	374	205	42	690.5
	391	215	47	685.5
	570	314	52	680.5
MS 16x0.312 (Max. R_N = 655 Kips)	337	186	37	695.5
	439	241	42	690.5
	452	248	47	685.5
	655	360	52	680.5

Table 4.12 – Pile Capacity at SN 010-0297 Pier 1 (WB-2) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	244	134	31	701.5
	289	159	36	696.5
	345	190	41	691.5
	392	215	45	687.5
MS 14x0.250 (Max. R_N = 459 Kips)	285	157	31	701.5
	344	189	36	696.5
	411	226	41	691.5
	459	252	45	687.5
MS 14x0.312 (Max. R_N = 570 Kips)	344	189	36	696.5
	411	226	41	691.5
	469	258	46	686.5
	570	314	51	681.5
MS 16x0.312 (Max. R_N = 655 Kips)	402	221	36	696.5
	479	264	41	691.5
	546	300	46	686.5
	655	360	51	681.5

Table 4.13 – Pile Capacity at SN 010-0297 Pier 2 (WB-3) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	293	161	34	698.5
	317	174	38	694.5
	358	197	42	690.5
	392	215	45	687.5
MS 14x0.250 (Max. R_N = 459 Kips)	347	191	34	698.5
	375	206	38	694.5
	425	234	42	690.5
	459	252	45	687.5
MS 14x0.312 (Max. R_N = 570 Kips)	375	206	38	694.5
	425	234	42	690.5
	479	264	47	685.5
	570	314	52	680.5
MS 16x0.312 (Max. R_N = 655 Kips)	434	239	38	694.5
	494	272	42	690.5
	556	306	47	685.5
	655	360	52	680.5

Table 4.14 – Pile Capacity at SN 010-0297 Pier 3 (WB-4) – Strength Limit State

Pile Size	Nominal Required Bearing, R_N (kips)	Factored Resistance Available, R_F (kips)	Estimated Pile Length (ft.)	Estimated Pile Tip Elevation (ft.)
MS 12x0.250 (Max. R_N = 392 Kips)	303	167	32	700.5
	345	190	39	693.5
	386	213	43	689.5
	392	215	44	688.5
MS 14x0.250 (Max. R_N = 459 Kips)	362	199	32	700.5
	411	226	39	693.5
	459	252	43	689.5
MS 14x0.312 (Max. R_N = 570 Kips)	362	199	32	700.5
	411	226	39	693.5
	459	252	43	689.5
	570	314	47	685.5
MS 16x0.312 (Max. R_N = 655 Kips)	424	233	32	700.5
	479	263	39	693.5
	533	293	43	689.5
	655	360	47	685.5

5.0 Construction Considerations

5.1 Construction Activities

All construction activities shall be performed in accordance with the current IDOT Standard Specifications for Road and Bridge Construction and any pertinent Special Provisions or Policies.

5.2 Temporary Soil Retention System / Sheet Piling

Temporary sheet piling will not be required to construct the abutments because the structures will be constructed utilizing cross over lanes. At the pier locations, the distance from ground surface to the bottom of proposed pier spread footing is approximately 5-8 feet. At Pier 2, construction of the footing appears feasible without the need for temporary retention. Though, the designer shall verify the final excavation depth and evaluate the proposed I-57 traffic staging to determine if temporary retention is required. At Piers 1 and 3, temporary soil retention systems will be necessary due to the proximity to the I-57 roadway and soil layers within the sheet piling embedment with a Q_u value larger than 4.5 tsf.

5.3 Foundation Construction

Conventional pile driving equipment and methodologies shall be assumed.

5.4 Excavation

Excavation shall be performed in accordance with IDOT Standard Specifications Section 202. Substructure construction shall occur after removal of the existing structure is complete.

A Joint Utility Locating Information for Excavators (J.U.L.I.E.) locate shall be performed prior to commencing construction activities to determine underground utilities within the project limits. In addition, IDOT shall be contacted to locate private utilities.

At foundation and structural fill locations, the exposed subgrade shall be proofrolled to aid in locating any unstable and unsuitable materials. Unstable and unsuitable materials shall be removed and replaced with compacted structural fill.

6.0 Limitations

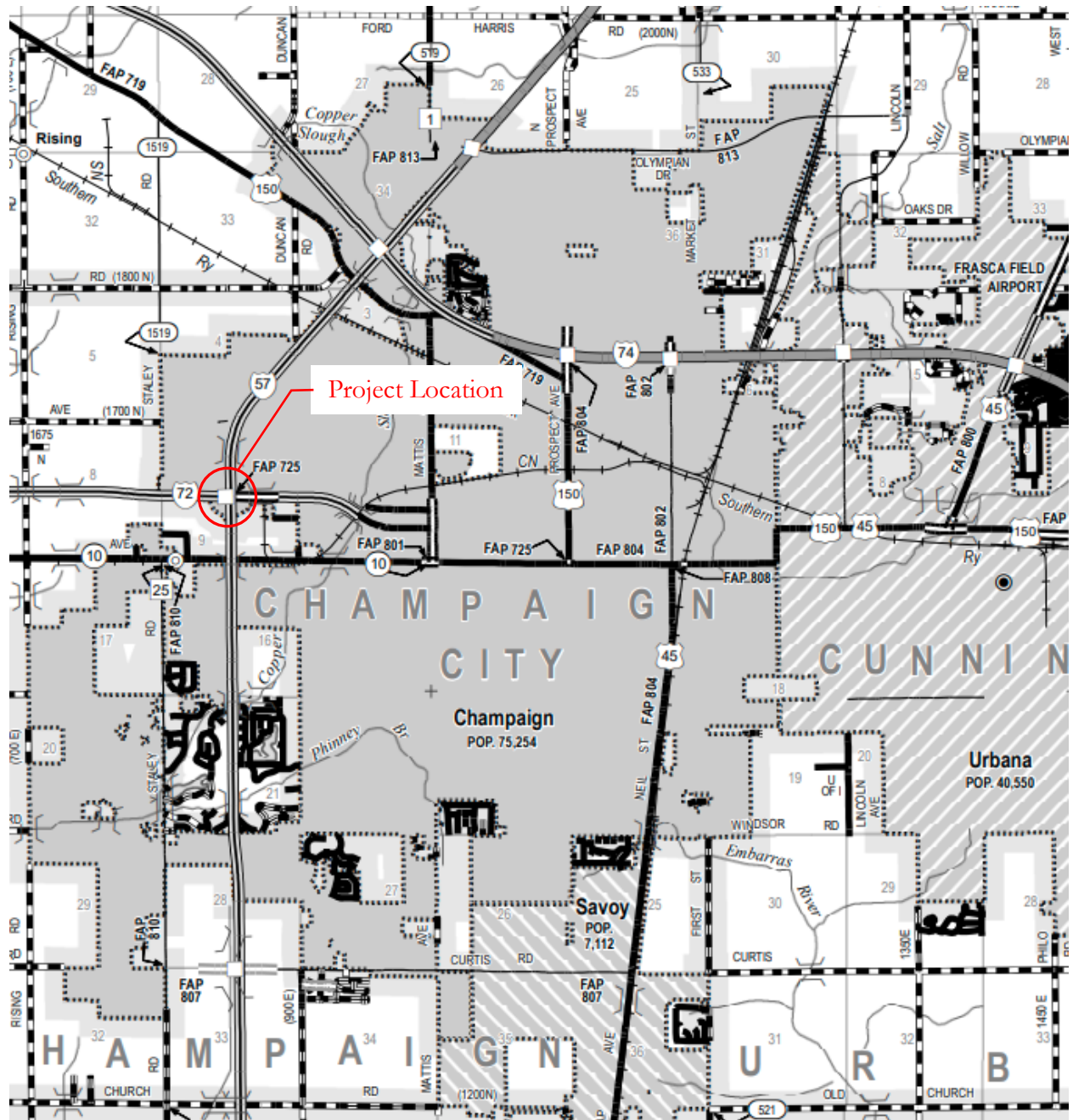
The analysis and discussion provided herein are for the exclusive use of IDOT and Veenstra & Kimm Inc. They are based upon the subsurface data obtained at boring locations within the bridge area and are specific to the project described, our understanding of the project as described herein, and geotechnical engineering practice consistent with the standard of care.



Appendix A

Location Map





Location Map

I-72 over I-57

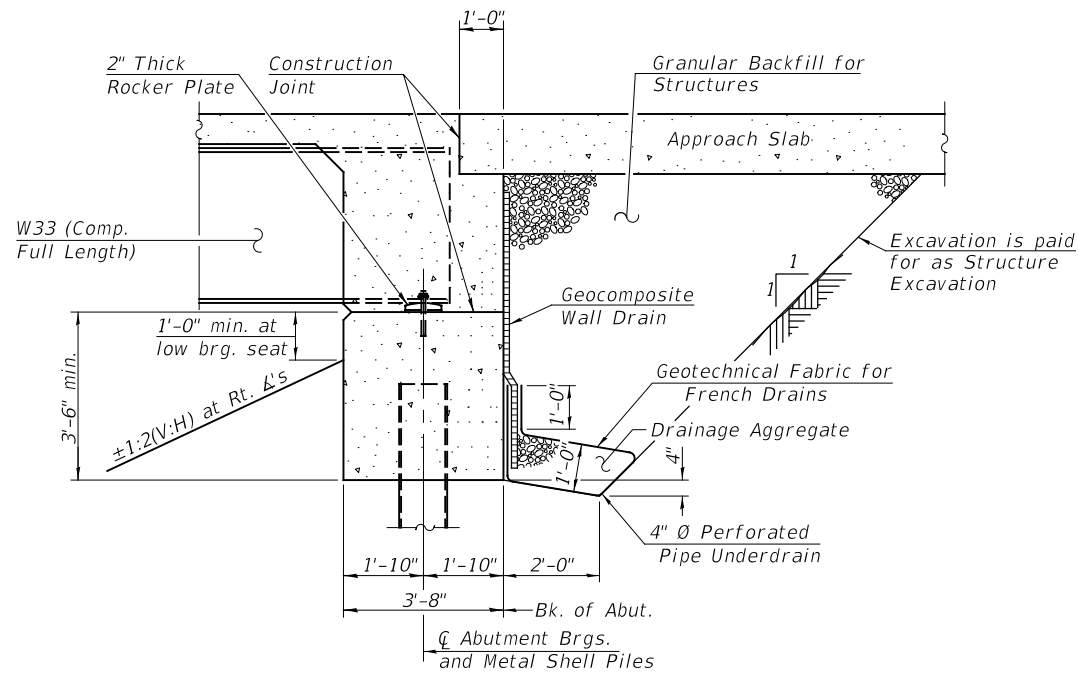
Champaign County, Illinois



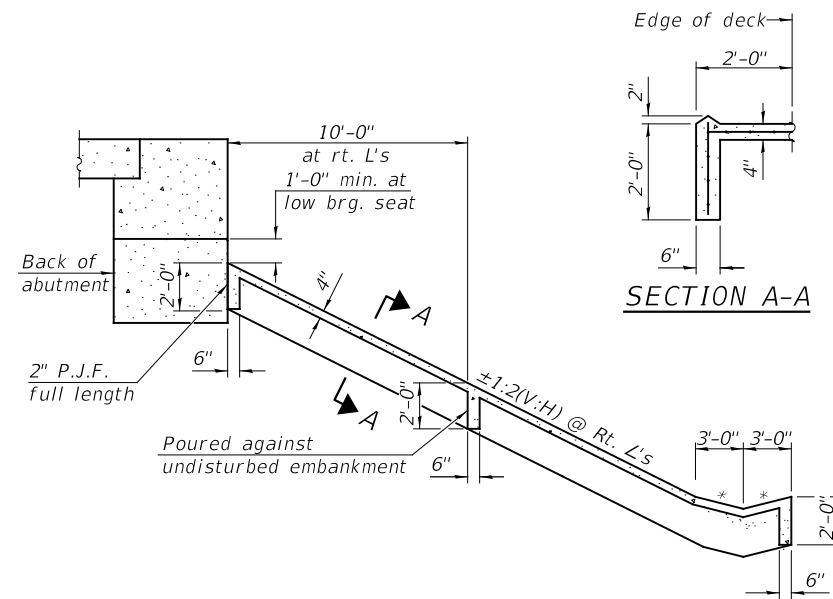
Appendix B

Type, Size, and Location Plan (TS&L)

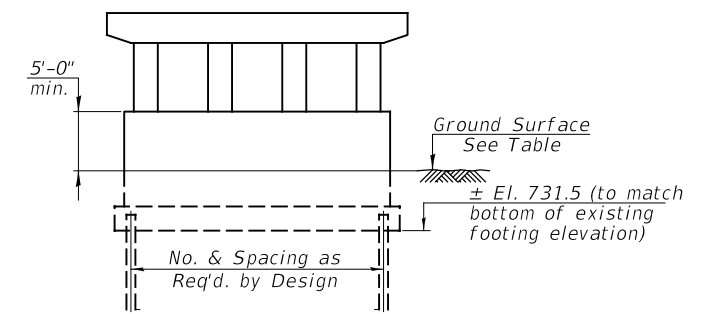




SECTION THRU INTEGRAL ABUTMENT
(Horiz. dim. @ Rt. L's)



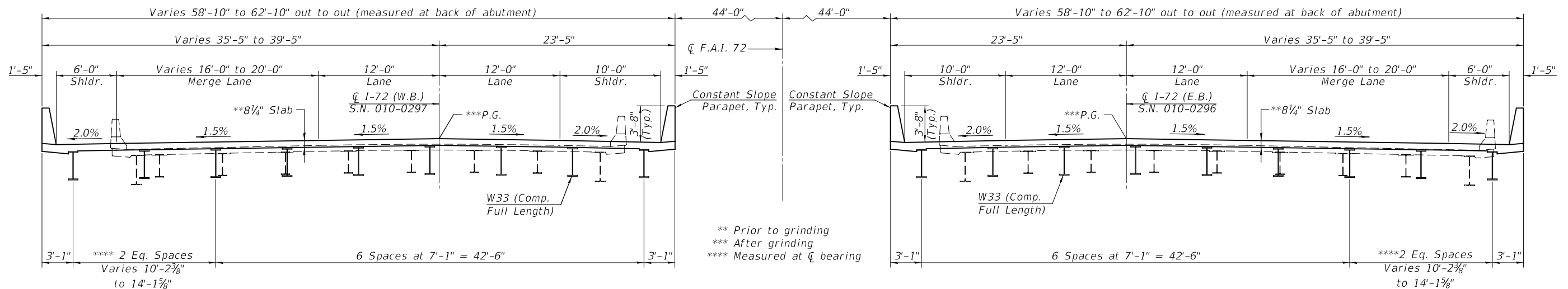
SECTION THRU CONCRETE SLOPEWALL
*1:6 (V:H)



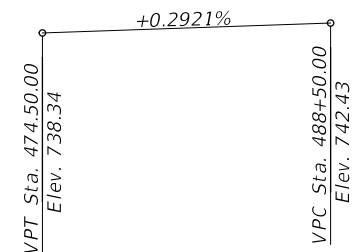
PIER SKETCH

GROUND ELEV. AT PIERS

W.B. Pier 1	El. 739.7
W.B. Pier 2	El. 739.0
W.B. Pier 3	El. 739.7
E.B. Pier 1	El. 738.8
E.B. Pier 2	El. 738.8
E.B. Pier 3	El. 739.3

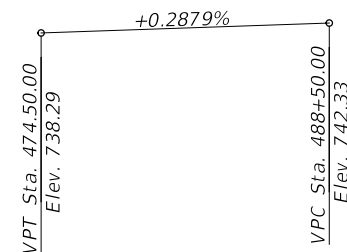


PROPOSED CROSS SECTION
(Looking East)



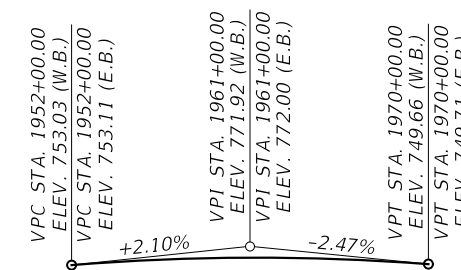
PROFILE GRADE

(Along NB I-57)
(Centerline of Thru Lanes)
(Stations increase South to North)



PROFILE GRADE

(Along SB I-57)
(Centerline of Thru Lanes)
(Stations increase South to North)



PROFILE GRADE

LVC = 180'

DETAILS
I-72 OVER I-57
F.A.I. ROUTE 72 - SECTION (10-33HB-2)BR
CHAMPAIGN COUNTY
STATION 1960+69.89
STRUCTURE NO. 010-0296 (E.B.)
STRUCTURE NO. 010-0297 (W.B.)



USER NAME =	DESIGNED -	REVISOR -
PLOT SCALE =	CHECKED -	REVISOR -
PLOT DATE = 8-4-2020	DRAWN -	REVISOR -
	CHECKED -	REVISOR -

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

GENERAL DETAILS
STRUCTURE NO. 010-0296 (E.B.) & 010-0297 (W.B.)

SHEET NO. 2 OF 2 SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
	(10-33HB-2)BR	CHAMPAIGN		
		CONTRACT NO. 70254		

ILLINOIS FED. AID PROJECT

Appendix C

Subsurface Data Profile Plot



Boring EB-1 (I-72)
 STA 1958+80
 OFFSET 17 FT LT
 EL 760.8 FT
 12/19/22

LEGEND

EL = Elevation (FT)
 D = Depth Below Existing Ground Surface (FT)
 N = SPT N-VALUE (AASHTO T206)
 Qu = Unconfined Compressive Strength in tons per sq. ft. (tsf)
 Failure Mode (B=bulge, S=shear, P=penetrometer)

W% = Moisture Content Percentage
 R% = Recovery Percentage
 RQD% = Rock Quality Designation Percentage

▼ = Groundwater Level First Encountered
 ▽ = Groundwater Upon Completion
 ▾ = Groundwater After 24 to 72 hours
 Soil profile is for illustrative purposes only. Actual conditions will vary.

EL	D	N	Qu	W%	R%	RQD%
760.8						
	5	20	2.9 B	11		
	13	13	1.2 B	11		
	11	4.0 B	13			
750.30	10	12	4.0 S	15		
	13	2.3 B	16			
	15	11	4.1 B	13		
				13		
740.30	20	11	3.6 B	16		
	5	2.7 B	22			
735.30	25	5	1.7 B	16		
	13	5.2 B	13			
	30	14	4.8 B	15		
	35	24	2.1 B	13		
724.05	40	9	2.9 B	13		
	45	8	3.2 B	12		
	50	24	NC			
	55	21	1.7 B	12		
	60	13	3.4 B	12		
	65	10	3.4 B	12		
	70	27	NC			
	75	33	1.9 B	16		
	80	18	0.6 B	17		
	85	50/3"	1.5 B	12		
674.05	90	97	12.1 S	8		
664.05	95	81	12.1 S	10		
661.05	100	77	NC	13		
	105					

Boring EB-2 (I-57)
 STA 482+40
 OFFSET 75 FT LT
 EL. 739.8 FT
 01/05/23

EL	D	N	Qu	W%	R%	RQD%
739.80						
739.14		15	2.5 P	17		
	5	7	1.3 B	13		
738.69		14	6.1 B	13		
736.8	10	9	6.2 B	16		
	15	20	8.1 B	11		
	17	17	5.3 B	12		
719.80	20	17	4.9 B	12		
	15	15	4.8 B	13		
	25	17	5.1 B	13		
		16	3.4 B	14		
	30	23	7.7 B	12		
	35	20	5.0 B	12		
699.80	40	17	2.0 B	14		
	45	16	1.9 B	13		
	50	20	5.3 B	12		
	55	25	NC	14		
683.05						
	60	93	10.9 B	11		
	65	89	3.5 S	10		
	70	73	9.7 B	12		
663.05	75	92	10.1 B	13		
	80	50/3"	NC			
	85	50/5"	NC			
653.05						
	90	50/5.5"	NC	19		
648.05						
	95	50/3"	NC			
640.90	100	50/5"	NC			
	105					

Boring EB-3 (I-57)
 STA 480+25
 OFFSET 7 FT LT
 EL. 737.7 FT
 12/08/22

EL	D	N	Qu	W%	R%	RQD%
737.70						
	17	NC	13			
734.70	5	9	3.3 B	14		
	10	4.1 B	7			
	10	12	6.1 B	11		
	15	11	4.9 B	12		
		16	2.9 S	13		
	20	16	4.2 B	11		
		13	5.1 B	11		
	25	12	1.8 B	13		
		9	3.1 B	13		
	30	11	3.6 B	15		
	35	4	0.5 B	18		
	40	10	0.9 B	13		
	45	17	1.5 P	14		
	50	21	2.9 B	14		
	55	26	1.8 P	16		
	60	86	NC			
	65	53	8.2 S	9		
	70	43	7.6 B	13		
665.95						
	75	50/4.5"	NC	13		
660.95						
	80	50/5.5"	NC			
	85	50/3.5"	NC			
	90	50/5.5"	NC			
	95	50/4"	NC			
	100	50/3"	NC			
	105					

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CIVIL DESIGN, INC.
 WBE / DBE
 EFFINGHAM, IL
 LICENSE # 184.003222

USER NAME =	DESIGNED - TAW	REVISED -
	CHECKED - TJZ	REVISED -
PLOT SCALE =	DRAWN - DCS	REVISED -
PLOT DATE =	CHECKED - TJZ	REVISED -

STATE OF ILLINOIS
 DEPARTMENT OF TRANSPORTATION

SUBSURFACE DATA PROFILE
 I-72 OVER I-57 SN 010-0034 (EB)

SHEET OF SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
72	(10-33HB-2)BR	CHAMPAIGN		
ILLINOIS		FED. AID PROJECT		

LEGEND

EL = Elevation (FT)
 D = Depth Below Existing Ground Surface (FT)
 N = SPT N-VALUE (AASHTO T206)
 Qu = Unconfined Compressive Strength in tons per sq. ft. (tsf)
 Failure Mode (B=bulge, S=shear, P=penetrometer)

W% = Moisture Content Percentage
 R% = Recovery Percentage
 RQD% = Rock Quality Designation Percentage

▼ = Groundwater Level First Encountered
 ∇ = Groundwater Upon Completion
 ∇ = Groundwater After 24 to 72 hours

Soil profile is for illustrative purposes only. Actual conditions will vary.

Boring EB-5 (I-72)
 STA 1962+50
 OFFSET 18 FT RT
 EL. 760.3 FT
 12/20/22

Boring EB-3 (I-57)
 STA 480+25
 OFFSET 7 FT LT
 EL. 737.7 FT
 12/08/22

Boring EB-4 (I-57)
 STA 481+25
 OFFSET 78 FT RT
 EL. 739.8 FT
 01/10/23

EL	D	N	Qu	W%	R%	RQD%
737.70		17	NC	13		
734.70	5	9	3.3 B	14		
	10	4.1 B	7			
	12	6.1 B	11			
	15	11	4.9 B	12		
	16	2.9 S	13			
	20	16	4.2 B	11		
	25	12	1.8 B	13		
	30	11	3.6 B	15		
	35	4	0.5 B	18		
	40	10	0.9 B	13		
	45	17	1.5 P	14		
	50	21	2.9 B	14		
	55	26	1.8 P	16		
665.95	70	43	7.6 B	13		
660.95	75	50/4.5"	NC	13		
	80	50/5.5"	NC			
	85	50/3.5"	NC			
	90	50/5.5"	NC			
	95	50/4"	NC			
638.95	100	50/3"	NC			
	105					

EL	D	N	Qu	W%	R%	RQD%
739.80		12	4.6 B	27		
738.80	5	9	2.9 B	20		
	10	10	2.9 B	11		
	15	12	3.9 B	12		
	20	11	2.9 B	14		
	25	9	1.8 B	13		
	30	7	1.4 B	13		
	35	50/5.5"	NC			
	40	17	4.0 B	12		
	45	25	1.9 S	14		
	50	26	6.1 B	12		
	55	17	2.5 B	6		
	60	73	7.3 S	9		
	65	62	9.4 S	11		
	70	66	11.3 B	13		
	75	88	8.5 S	17		
663.05	80	50/4"	NC	19		
	85	50/3.5"	NC	18		
648.05	90	50/3"	NC	20		
	95	50/3"	NC			
640.55	100	50/3"	NC			
	105					

EL	D	N	Qu	W%	R%	RQD%
760.3		16	4.9 B	11		
	5	12	5.7 B	16		
	10		3.4 B	16		
	15	13	6.6 B	15		
	20	12	4.7 B	13		
	25	8	3.5 B	19		
	30	11	3.9 B	13		
	35	11	2.5 P	12		
	40	11	NC			
	45	11	4.4 B	15		
	50	10	4.6 B	13		
	55	12	4.8 B	11		
	60	13	5.8 B	12		
	65	17	6.0 B	12		
	70	21	6.8 B	12		
	75	17	5.5 B	15		
683.55	80	79	NC	6		
678.55	85	59	12.1 B	9		
673.55	90	66	10.9 B	9		
668.55	95	50/2.5"	>4.5 P	7		
663.55	100	50/2"	NC			
661.60	105					

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CIVIL DESIGN, INC.
 WBE / DBE
 EFFINGHAM, IL
 LICENSE #184.003222

USER NAME =	DESIGNED - TAW	REVISED -
	CHECKED - TJZ	REVISED -
PLOT SCALE =	DRAWN - DCS	REVISED -
PLOT DATE =	CHECKED - TJZ	REVISED -

STATE OF ILLINOIS
 DEPARTMENT OF TRANSPORTATION

SUBSURFACE DATA PROFILE
 I-72 OVER I-57 SN 010-0034 (EB)

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
72	(10-33HB-2)BR	CHAMPAIGN		

Boring WB-1 (I-72)
 STA 1958+80
 OFFSET 17 FT LT
 EL 760.6 FT
 12/14/22

LEGEND

EL = Elevation (FT)
 D = Depth Below Existing Ground Surface (FT)
 N = SPT N-VALUE (AASHTO T206)
 Qu = Unconfined Compressive Strength in tons per sq. ft. (tsf)
 Failure Mode (B=bulge, S=shear, P=penetrometer)

W% = Moisture Content Percentage
 R% = Recovery Percentage
 RQD% = Rock Quality Designation Percentage

▼ = Groundwater Level First Encountered
 ▽ = Groundwater Upon Completion
 ▾ = Groundwater After 24 to 72 hours
 Soil profile is for illustrative purposes only. Actual conditions will vary.

	EL	D	N	Qu	W%	R%	RQD%
Brown, stiff, dry, SILTY CLAY LOAM	760.60		10	2.1 B	14		
	757.60	5	9	4.0 B	21		
		12	10	3.5 B	15		
	750.10	10	10	3.7 B	18		
Brown, stiff, dry, SILTY CLAY LOAM, trace gravel					21		
	745.10	15	15	3.2 B	15		
Grey, medium stiff to stiff, dry, SILTY CLAY			10	5.3 B	15		
		20	9	2.8 B	18		
		8	8	3.8 B	25		
	735.10	25	7	2.7 B	26		
Brown to reddish brown, very stiff, dry, SILTY CLAY LOAM			21	9.6 S	13		
		30	18	4.5 B	13		
Grey, stiff to very stiff, dry, SILTY CLAY							
	728.85	35	16	7.2 B	11		
		40	13	2.3 B	14		
		45	11	2.9 B	13		
		50	12	2.8 B	14		
Grey, soft, moist, SILTY CLAY LOAM							
	708.85	55	11	0.2 S	19		
Grey, medium dense, saturated, SAND, fine-grained							
	703.85	60	30	NC			
Grey, stiff to very stiff, moist, SILTY CLAY							
	698.85	65	24	4.9 S	17		
		70	16	NC			
		75	15	NC			
Grey, hard, moist, SILTY CLAY LOAM							
	683.85	80	51	8.7 S	16		
Grey, hard, moist, SILTY CLAY							
	678.85	85	64	10.9 S	11		
		90	53	12.1 S	11		
		95	53	12.1 B	11		
End of Boring	661.14	100	50/5.5"	9.3 S	18		
		105					


Boring WB-2 (I-57)
 STA 482+40
 OFFSET 74 FT LT
 EL 740.1 FT
 01/06/23

	EL	D	N	Qu	W%	R%	RQD%
ASPHALT (8.0")	740.10		12	NC	19		
FILL: Crushed Limestone Aggregate Base (6.0")	739.35						
	738.90	5	10	3.4 B	16		
Brown and grey, stiff, dry, SILT LOAM							
	737.10	10	12	3.6 B	14		
Brown to grey, stiff to very stiff, dry, SILTY CLAY							
		15	19	7.0 B	11		
		17	17	3.3 B	13		
		20	17	3.4 B	13		
		18	18	4.6 B	13		
		25	17	4.7 B	12		
Grey, very stiff, moist, SANDY LOAM, with fine grained sand	714.60		17	NC	11		
Grey, very stiff, moist, SILTY CLAY, trace gravel	712.10		30	20	6.6 B	13	
		35	18	0.6 B	15		
Grey, very stiff, dry, SILT	703.35						
		40	30	NC	18		
Grey, very stiff to hard, moist, SILTY CLAY	698.35						
		45	25	4.5 S	18		
		50	26	5.1 B	12		
		55	23	5.0 S	18		
		60	62	10.1 B	10		
		65	86	12.1 S	8		
		70	71	12.1 S	10		
		75	50	7.7 B	14		
Grey, very dense, dry, SAND, fine-grained	663.35						
		80	50/4"	NC			
Grey, hard, dry, SILT	658.35						
		85	44	2.8 S	20		
		90	75	5.5 S	21		
		95	89	1.4 S	21		
End of Boring	641.20	100	50/5"	NC	23		
		105					

Boring WB-3 (I-57)
 STA 481+45
 OFFSET 3 FT LT
 EL 739.9 FT
 12/07/22

	EL	D	N	Qu	W%	R%	RQD%
Brown, stiff, dry, SANDY CLAY	739.90		14	2.4 S	16		
	736.90	5	21	NC	14		
Brown, medium dense, unsaturated, SAND, fine-grained							
Brown to grey, medium stiff to stiff, dry, SILTY CLAY	734.40		8	2.6 B	14		
		10	12	2.5 B	13		
		15	13	5.5 B	11		
		12	12	6.2 B	11		
		20	8	6.0 B	11		
		12	12	6.5 B	11		
		25	14	>4.5 P	11		
		12	12	2.8 B	14		
		30	12	3.3 B	13		
		35	11	5.9 B	13		
Grey, medium dense, saturated, SAND, fine-grained	703.15						
		40	12	NC	14		
Grey, stiff to hard, moist, SILTY CLAY	698.15						
		45	14	3.0 B	12		
		50	17	4.3 B	11		
		55	10	4.0 B	12		
		60	77	8.0 S	9		
		65	90	6.7 S	8		
		70	63	11.1 S	11		
		75	50/1.5"	>4.5 P	12		
		80	89	8.0 S	20		
		85	68	6.5 S	18		
		90	100	3.3 S	18		
Grey, hard, moist, SILT	648.15						
		95	100	NC	22		
Grey, very dense, moist, SAND, fine-grained	643.15						
End of Boring	640.60						
		100	50/3.5"	NC			
		105					

MODEL: Default
 FILE NAME: P:\5XXXX\2XX-53XX\5288 - PTB 201-035 D5_VK_I-72 over I-57\24-Structures\CAD\5288 SGR - WB Borings 1-3.dgn

 CIVIL DESIGN, INC. WBE / DBE EFFINGHAM, IL LICENSE #184.003222	USER NAME =	DESIGNED - TAW	REVISED -
		CHECKED - TJZ	REVISED -
	PLOT SCALE =	DRAWN - DCS	REVISED -
	PLOT DATE =	CHECKED - TJZ	REVISED -

STATE OF ILLINOIS
 DEPARTMENT OF TRANSPORTATION

SUBSURFACE DATA PROFILE
 I-72 OVER I-57 SN 010-0035 (WB)

SHEET OF SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
72	(10-33HB-2)BR	CHAMPAIGN		

ILLINOIS FED. AID PROJECT

LEGEND

EL = Elevation (FT)
 D = Depth Below Existing Ground Surface (FT)
 N = SPT N-VALUE (AASHTO T206)
 Qu = Unconfined Compressive Strength in tons per sq. ft. (tsf)
 Failure Mode (B=bulge, S=shear, P=penetrometer)

W% = Moisture Content Percentage
 R% = Recovery Percentage
 RQD% = Rock Quality Designation Percentage

▼ = Groundwater Level First Encountered
 ∇ = Groundwater Upon Completion
 ∇ = Groundwater After 24 to 72 hours

Soil profile is for illustrative purposes only. Actual conditions will vary.

Boring WB-5 (I-72)
 STA 1962+50
 OFFSET 18 FT LT
 EL. 760.1 FT
 12/12/22

Boring WB-3 (I-57)
 STA 481+45
 OFFSET 3 FT LT
 EL. 739.9 FT
 12/07/22

Boring WB-4 (I-57)
 STA 482+30
 OFFSET 75 FT RT
 EL. 740.0 FT
 01/11/23

EL	D	N	Qu	W%	R%	RQD%
739.90						
736.90	5	21	NC	14		
734.40	8	2.6 B	14			
	10	12	2.5 B	13		
				12		
	15	13	5.5 B	11		
		12	6.2 B	11		
	20	8	6.0 B	11		
		12	6.5 B	11		
	25	14	>4.5 P	11		
		12	2.8 B	14		
	30	12	3.3 B	13		
	35	11	5.9 B	13		
703.15						
698.15	40	12	NC	14		
	45	14	3.0 B	12		
	50	17	4.3 B	11		
	55	10	4.0 B	12		
	60	77	8.0 S	9		
	65	90	6.7 S	8		
	70	63	11.1 S	11		
	75	50/1.5"	>4.5 P	12		
	80	89	8.0 S	20		
	85	68	6.5 S	18		
648.15	90	100	3.3 S	18		
	95	100	NC	22		
643.15						
640.60	100	50/3.5"	NC			
	105					

EL	D	N	Qu	W%	R%	RQD%
740.00						
739.10						
738.70	5	7	1.5 B	26		
	7		1.2 B	16		
	10	10	3.5 B	14		
				15		
	15	12	4.0 B	13		
		15	4.6 B	10		
	20	17	4.6 B	12		
		15	3.7 S	12		
	25	12	2.9 B	12		
		15	3.6 B	12		
	30	16	2.5 B	14		
	35	14	3.9 B	13		
	40	17	5.1 B	13		
698.25						
693.25	45	13	NC			
	50	24	4.7 S	14		
	55	35	3.5 S	16		
683.25						
	60	75	11.0 B	10		
	65	88	12.1 S	11		
	70	90	12.1 S	11		
	75	71	10.3 B	12		
663.25						
	80	50/2.5"	NC			
	85	50/4"	NC			
648.25	90	50/5"	NC			
	95	89	4.2 S	19		
643.25						
640.00	100	90	4.6 S	19		
	105					

EL	D	N	Qu	W%	R%	RQD%
760.10						
	5	12	2.8 B	37		
754.60						
752.10	10	16	5.2 B	15		
		12	5.0 S	13		
	15	17	2.1 S	13		
				12		
	20	13	3.1 B	12		
		9	3.0 B	27		
	25	7	2.3 B	18		
		7	1.9 B	15		
	30	10	2.3 B	14		
	35	20	5.8 B	11		
	40	16	5.2 B	12		
	45	13	4.1 B	12		
	50	18	NC	11		
	55	18	NC			
	60	22	NC			
	65	20	4.1 B	11		
	70	49	NC	7		
	75	16	3.8 B	12		
	80	92	>4.5 P	9		
678.35						
	85	50/5"	NC	11		
673.35						
	90	60	11.5 B	11		
	95	50/5.5"	12.1 B	10		
661.30	100	50/3.5"	NC	13		
	105					

MODEL: Default
 FILE NAME: P:\5XXXX\2XX-53XX\5288 - PTB 201-035 D5_VK_I-72 over I-57\24-Structures\CAD\5288 5GR - WB Borings 3-5.dgn



CIVIL DESIGN, INC.
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USER NAME =	DESIGNED - TAW	REVISED -
	CHECKED - TJZ	REVISED -
PLOT SCALE =	DRAWN - DCS	REVISED -
PLOT DATE =	CHECKED - TJZ	REVISED -

STATE OF ILLINOIS
 DEPARTMENT OF TRANSPORTATION

SUBSURFACE DATA PROFILE
 I-72 OVER I-57 SN 010-0035 (WB)

SHEET OF SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
72	(10-33HB-2)BR	CHAMPAIGN		
ILLINOIS		FED. AID PROJECT		

Appendix D

Soil Boring Logs





Millennia Professional Services of Illinois, Ltd.

11 Executive Drive, Suite 12 • Fairview Heights, Illinois 62208 • (Office) 618.624.8610 • (Fax) 618.624.8611

IDOT District 5
FAI 72 over Interstate 57
Structure No. 010-0034 & 010-0035
Champaign County, Illinois
PTB 195-042 Work Order No. 3
MG22080

GEOTECHNICAL SERVICES

Subsurface Exploration

A subsurface exploration program was implemented for the replacement of bridge structures located in Champaign County, Illinois. The bridges (dual structures) carry Interstate 72 over Interstate 57 on the west side of Champaign.

The subsurface exploration included six (6) borings advanced to 100-feet below the ground surface for the dual structures 010-0034 & 010-0034. The approximate boring locations have been provided by IDOT district personnel. The elevations of the borings were estimated from topographic survey data provided by IDOT, and the stationing and offsets were estimated from plans and profile sheets provided by IDOT District personnel. All the borings were advanced using Standard SPT methods using hollow stem auger and/or mud rotary drilling techniques. SPT samples were taken on 2.5-intervals to a depth of 30 feet and 5-foot intervals to termination. RIMAC strength tests were performed on all intact cohesive samples. The drilling procedures followed the subsurface exploration guidelines as stated in the IDOT Geotechnical Manual dated 2015 (Revised December 2020) and all current applicable Department AGMUs. The generated gINT logs are attached.

Laboratory testing on representative samples included:

- Moisture contents;
- Visual descriptions; and
- Dry Unit Weights.

Sincerely,
Millennia Professional Services, Ltd.

Charles R. Graham
Geotechnical Engineer/Project Manager



Millennia Professional Services

11 Executive Dr #12, Fairview Heights, IL 62208

Phone: (618) 624-8610

Fax: (618) 624-8611

Project No.: MG22080

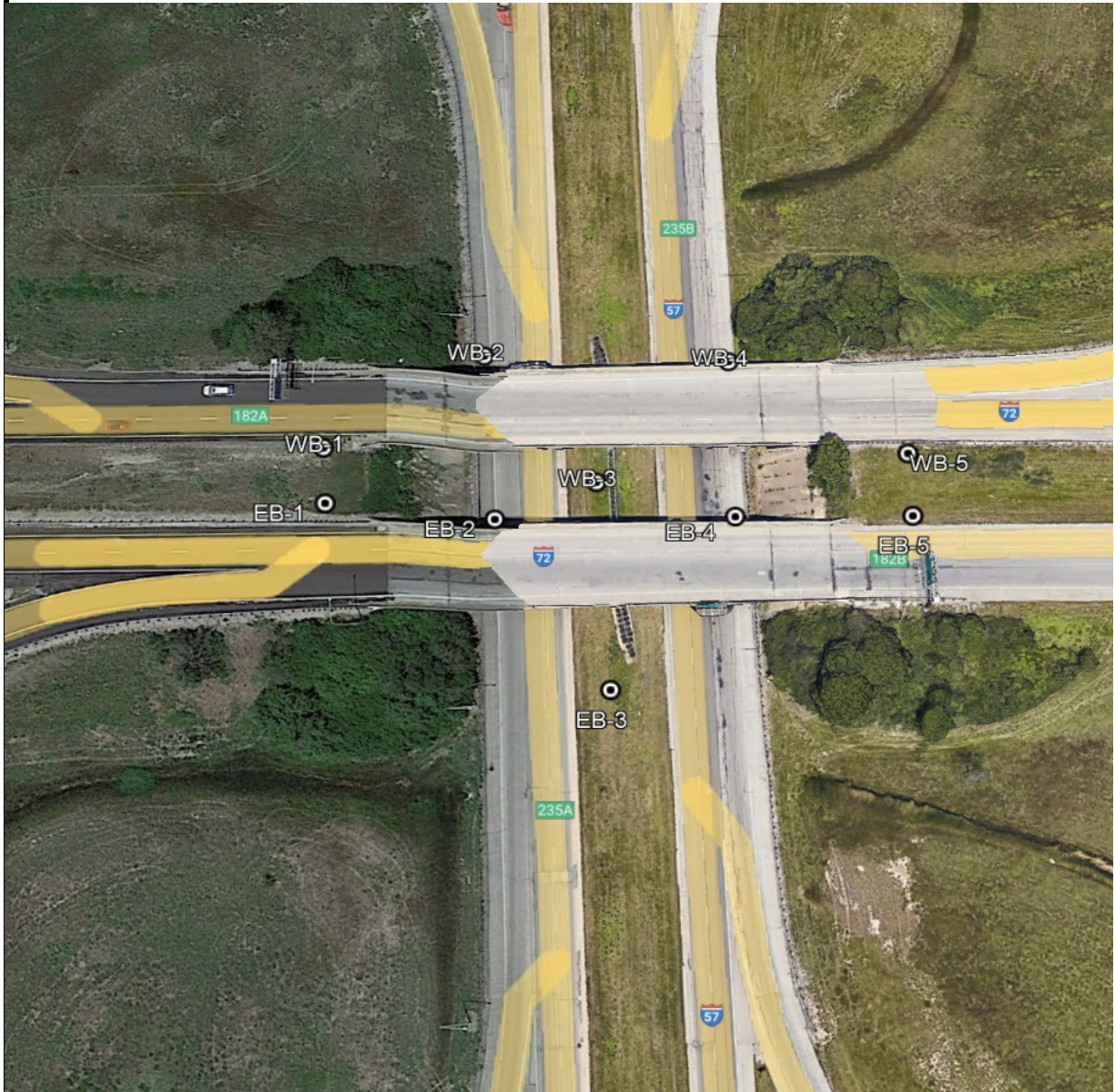


FIGURE 2.1: BORING LOCATION PLAN

PTB 195-042 WO #3 Bridge Replacement
Champaign, Illinois



Approximate
Boring Location:



Image obtained from Google Earth
*Not to scale

Drawn by:

C. Graham

Checked by:

C. Graham

Project No.:

MG22080

Date:

11/10/2022

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	ELEVATION (ft)	DEPTH (ft)	BLOWS /6" (tsf)	UCS (tsf)	MOISTURE (%)	Surface Water Elev. (ft)	Stream Bed Elev. (ft)	Groundwater Elev. (ft)	First Encounter (ft)	Upon Completion (ft)	After (ft)	ELEVATION (ft)	DEPTH (ft)	BLOWS /6" (tsf)	UCS (tsf)	MOISTURE (%)
EB-1						N/A	N/A									
Note																
Offset																
Stationing																
E																
Ground Surface Elev.	760.8															
LITHOLOGY						LITHOLOGY										
Brown, stiff to very stiff, dry, SILTY CLAY						Brown and grey, medium stiff, dry, SILTY CLAY						740.30				
			4											3		
			7	2.9	11								2	2.7	22	
			13	B									3	B		
			4										2			
			6	1.2	11								2	1.7	16	
			-5	7	B							-25	3	B		
			3													
			5	4.0	13								3			
			6	B									5	5.2	13	
			2													
			5	4.0	15								3			
			-10	7	S							-30	6	4.8	15	
			3													
			5	4.1	13								3			
			-15	6	B							-35	13	2.1	13	
					13											
			4													
			4	3.6	16								3			
			-20	7	B							-40	3	2.9	13	
													6	B		

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 1/5/2023

EB-2
SOIL BORING LOG
 Sheet 3 of 3

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO. <u>EB-2</u>	E	D	B	U	M	Surface Water Elev. <u>N/A ft</u>
Note <u>I-57</u>	L	E	L	C	O	Stream Bed Elev. <u>N/A ft</u>
Offset <u>75 ft Left</u>	E	P	O	S	I	Groundwater Elev.:
Stationing <u>481+25 (I-57)</u>	V	T	W	S	S	First Encounter <u>726.8 ft ▼</u>
	H	S	Qu	T	T	Upon Completion <u>N/A ft</u>
Ground Surface Elev. <u>739.8 ft</u>						After <u>N/A</u> Hrs. <u>N/A ft</u>

LITHOLOGY	(ft)	(ft)	(/6")	(tsf)	(%)	LITHOLOGY
Grey, very dense, dry, SAND, fine-grained (continued)						
			50/5"			
		-85				
	653.05					
Grey, hard, dry, SILT						
			50/5.5"		19	
		-90				
	648.05					
Grey, very dense, dry, SAND, fine-grained						
			42			
		-95	50/3"			
	640.90		50/5.5"			
End of Boring		-100				

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



EB-3
SOIL BORING LOG
Sheet 2 of 3

COUNTY Champaign
SECTION (10-33HB-2)BR
ROUTE IL-72 and W Kirby over I-57
JOB NO. MG22080
DATE 12/8/2022

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	DESCRIPTION	ELEVATION (ft)	DEPTH (ft)	BLOWS /6" (tsf)	UCS (tsf)	MOISTURE (%)	Surface Water Elev. (ft)	Stream Bed Elev. (ft)	Groundwater Elev. (ft)	First Encounter Upon Completion (ft)	After (ft)	Hours	After (ft)	ELEVATION (ft)	DEPTH (ft)	BLOWS /6" (tsf)	UCS (tsf)	MOISTURE (%)
EB-3							N/A	N/A										
Note	I-57																	
Offset	7 ft Left																	
Stationing	480+25 (I-57)																	
Ground Surface Elev.	737.7 ft																	
LITHOLOGY							LITHOLOGY											
Brown to grey, stiff to very stiff, dry, SILTY CLAY (continued) - difficulty drilling from 40.0-45.0 ft. due to gravel caving into hole							Brown to grey, stiff to very stiff, dry, SILTY CLAY (continued)											
- with gravel from 43.5-45.0 ft.																		
			4													15		
			6	1.5	14										25	8.2	9	
		-45	11	P										-65	28	S		
- trace gravel below 53.5 ft.																		
			5													12		
			9	2.9	14										14	7.6	13	
		-50	12	B										-70	29	B		
- hard below 58.5 ft.																		
			6													50/4.5"		13
			12	1.8	16													
		-55	14	P										-75				
- hard below 58.5 ft.																		
			28													50/5.5"		
			38															
		-60	48											-80				
							665.95 Grey, very dense, dry, SANDY LOAM											
							660.95 Grey, very dense, dry, SAND, fine-grained											

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 12/8/2022

EB-3
SOIL BORING LOG
 Sheet 3 of 3

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO. <u>EB-3</u>	E	D	B	U	M	Surface Water Elev. <u>N/A</u> ft
Note <u>I-57</u>	L	E	L	C	O	Stream Bed Elev. <u>N/A</u> ft
Offset <u>7 ft Left</u>	E	P	O	S	I	Groundwater Elev.:
Stationing <u>480+25 (I-57)</u>	V	T	W	S	S	First Encounter <u>N/E</u> ft
	H	S	Qu	T	T	Upon Completion <u>N/A</u> ft
Ground Surface Elev. <u>737.7</u> ft						After <u>N/A</u> Hrs. <u>N/A</u> ft

LITHOLOGY	(ft)	(ft)	(/6")	(tsf)	(%)	LITHOLOGY
Grey, very dense, dry, SAND, fine-grained (continued)						
			50/3.5"			
		-85				
			50/5.5"			
		-90				
			50/4"			
		-95				
		638.95	50/3"			
End of Boring						
		-100				

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 1/10/2023

EB-4
SOIL BORING LOG
 Sheet 3 of 3

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO. EB-4 E L E V E N V (ft) (ft) (/6") (tsf) (%) M O I S T U R E (tsf) (%)
 Note I-57
 Offset 78 ft. Right
 Stationing 481+25 (I-57)
 Ground Surface Elev. 739.8 ft
 Surface Water Elev. N/A ft
 Stream Bed Elev. N/A ft
 Groundwater Elev.:
 First Encounter N/E ft
 Upon Completion N/A ft
 After N/A Hrs. N/A ft

LITHOLOGY	(ft)	(ft)	(/6")	(tsf)	(%)	LITHOLOGY
Grey, hard, dry, SILT, trace gravel (continued)						
			39			
			50/3.5"		18	
			-85			
			29			
			50/3"		20	
			-90			
			648.05			
Grey, very dense, dry, SAND, fine-grained						
			41			
			50/3"			
			-95			
			41			
			50/3"			
			640.55			
End of Boring			-100			

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 12/20/2022

EB-5
SOIL BORING LOG
 Sheet 3 of 3

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	DEPTH	BLOWS	UCS	MOISTURE	Surface Water Elev.	Stream Bed Elev.	Groundwater Elev.:	First Encounter	Upon Completion	After	Hrs.
	(ft)	(/6")	(tsf)	(%)	N/A	N/A	ft	ft	ft	N/A	ft
EB-5											
Note	I-72										
Offset	18 ft Right										
Stationing	1962+50 (I-72)										
Ground Surface Elev.	760.3										
LITHOLOGY					LITHOLOGY						
Grey, hard, moist, SILTY LOAM, with gravel (continued)											
	678.55										
Dark brown, hard, moist, SILTY CLAY LOAM											
		8									
		23	12.1	9							
		36	B								
	-85										
Dark brown, hard, moist, SILTY CLAY											
	673.55										
		23									
		32	10.9	9							
		34	B								
	-90										
Dark brown, hard, moist, SILTY CLAY LOAM											
	668.55										
		50/2.5	>4.5	7							
			P								
	-95										
Light brown, very dense, saturated, SAND, fine-grained											
	663.55										
	661.60										
End of Boring		50/2"									
	-100										

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



WB-2 SOIL BORING LOG

Sheet 1 of 3

COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 1/6/2023

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	WB-2	E	D	B	U	M	Surface Water Elev.	N/A	ft	E	D	B	U	M
Note	I-57	L	E	L	C	O	Stream Bed Elev.	N/A	ft	L	E	L	C	O
Offset	74 ft Left	E	P	O	S	I	Groundwater Elev.:			V	T	W	Q	S
Stationing	482+40 (I-57)	V	H	S	Qu	T	First Encounter	714.1	ft	H	S	Qu	T	
Ground Surface Elev.	740.1	(ft)	(ft)	(/6")	(tsf)	(%)	Upon Completion	N/A	ft	(ft)	(ft)	(/6")	(tsf)	(%)
							After	N/A	Hrs.					
LITHOLOGY							LITHOLOGY							
ASPHALT (8.0")	739.35						Brown to grey, stiff to very stiff, dry, SILTY CLAY (continued)							
FILL: Crushed limestone aggregate (6.0")	738.90			4								4		
Brown and grey, stiff, dry, SILT LOAM				6		19						8	4.6	13
				6								10	B	
	737.10													
Brown to grey, stiff to very stiff, dry, SILTY CLAY				3								4		
				4	3.4	16						8	4.7	12
				-5	B							9	B	
												-25		
				5			Grey, very stiff, moist, SANDY LOAM, with fine-grained sand					7		
				7	5.5	14						8		11
				8	B							9		
				3			Grey, very stiff, moist, SILTY CLAY, trace gravel					8		
				5	3.6	14						9	6.6	13
				-10	B		- gravel seam at 29.0 ft.					11	B	
												-30		
							-switched to mud-rotary 30-feet							
				5								4		
				8	7.0	11						8	0.6	15
				-15	B							10	B	
				5										
				7	3.3	13								
				10	B									
				4								11		
				8	3.4	13						14		18
				-20	B							16		
												-40		
							Grey, very stiff, dry, SILT							

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	WB-3	E	D	B	U	M	Surface Water Elev.	N/A	ft	E	D	B	U	M
Note	I-57	L	E	L	C	O	Stream Bed Elev.	N/A	ft	L	E	L	C	O
Offset	3 ft Left	E	P	O	S	I	Groundwater Elev.:			V	T	W	Q	S
Stationing	481+45 (I-57)	V	H	S	Qu	T	First Encounter	700.9	ft	H	S	Qu	T	
Ground Surface Elev.	739.9	(ft)	(ft)	(/6")	(tsf)	(%)	Upon Completion	N/A	ft	(ft)	(ft)	(/6")	(tsf)	(%)
							After	N/A	Hrs.					
LITHOLOGY							LITHOLOGY							
Brown, stiff, dry, SANDY CLAY							Brown to grey, medium stiff to stiff, dry, SILTY CLAY (continued)							
				3								3		
				5	2.4	16						5	6.5	11
				9	S							7	B	
				----- 736.90										
Brown, medium dense, unsaturated, SAND, fine-grained														
				9								7		
				10		14						7	>4.5	11
				-5	11							-25	7	P
				----- 734.40										
Brown to grey, medium stiff to stiff, dry, SILTY CLAY														
				2								3		
				4	2.6	14						5	2.8	14
				4	B							7	B	
				4								2		
				5	2.5	13						4	3.3	13
				-10	7	B						-30	8	B
- Dry Unit Weight: 128 pcf														
						12								
- grey, trace gravel below 13.5 ft.														
				3								2		
				5	5.5	11						4	5.9	13
				-15	8	B						-35	7	B
				4										
				5	6.2	11								
				7	B									
				----- 703.15										
							Grey, medium dense, saturated, SAND, fine-grained							
				3									3	
				4	6.0	11							5	
				-20	4	B						-40	7	

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



WB-3
SOIL BORING LOG
 Sheet 3 of 3

COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 12/7/2022

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO. WB-3 Surface Water Elev. N/A ft
 Note I-57 Stream Bed Elev. N/A ft
 Offset 3 ft Left Groundwater Elev.:
 Stationing 481+45 (I-57) First Encounter 700.9 ft ▼
 Ground Surface Elev. 739.9 ft Upon Completion N/A ft
 After N/A Hrs. N/A ft

LITHOLOGY		(ft)	(ft)	(/6")	(tsf)	(%)	LITHOLOGY	
Grey, stiff to hard, moist, SILTY CLAY (continued)								
				21				
				29	6.5	18		
				-85	39	S		
				29				
				50	3.3	18		
				-90	50/2"	S		
				648.15				
Grey, hard, moist, SILT								
				29				
				50		22		
				-95	50/4"			
				643.15				
Grey, very dense, moist, SAND, fine-grained								
				48				
				640.60	50/3.5"			
End of Boring				-100				

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



WB-4 SOIL BORING LOG

Sheet 1 of 3

COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 1/11/2023

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	WB-4	E	D	B	U	M	Surface Water Elev.	N/A	ft	E	D	B	U	M
Note	I-57	L	E	L	C	O	Stream Bed Elev.	N/A	ft	L	E	L	C	O
Offset	75 ft. Right	E	P	O	S	I	Groundwater Elev.:			E	P	O	S	I
Stationing	482+30 (I-57)	V	T	W	Q	S	First Encounter	N/E	ft	V	T	W	Q	S
Ground Surface Elev.	740.0	H	S	S	Qu	T	Upon Completion	N/A	ft	H	S	Qu	T	
		(ft)	(ft)	(/6")	(tsf)	(%)	After	N/A	Hrs.	(ft)	(ft)	(/6")	(tsf)	(%)
LITHOLOGY							LITHOLOGY							
ASPHALT (11.0")	739.10						Brown and grey, medium stiff to very stiff, dry, SILTY CLAY	(continued)						
FILL: Crushed limestone aggregate (4.0")	738.70		4									6		
Brown and grey, medium stiff to very stiff, dry, SILTY CLAY			4	3.4	24							7	3.7	12
			6	B								8	S	
			2									3		
			3	1.5	26							4	2.9	12
			-5	4	B							-25	8	B
			2									3		
			3	1.2	16							6	3.6	12
			4	B								9	B	
- brown below 8.5 ft.			3									4		
			4	3.5	14							7	2.5	14
			-10	6	B							-30	9	B
- grey, trace gravel below 11.0 ft.														
-Dry Unit Weight: 120 pcf						15								
			1									5		
			4	4.0	13							6	3.9	13
			-15	8	B							-35	8	B
			5											
			7	4.6	10									
			8	B										
			4									6		
			7	4.6	12							8	5.1	13
			-20	10	B							-40	9	B

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



WB-4 SOIL BORING LOG

Sheet 2 of 3

COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 1/11/2023

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	WB-4	E	D	B	U	M	Surface Water Elev.	N/A	ft	E	D	B	U	M
Note	I-57	L	E	L	C	O	Stream Bed Elev.	N/A	ft	L	E	L	C	O
Offset	75 ft Right	E	P	O	S	I	Groundwater Elev.:			E	P	O	S	I
Northing	482+30	V	T	W	Q	S	First Encounter	N/E	ft	V	T	W	Q	S
Ground Surface Elev.	740.0	H	S	S	Qu	T	Upon Completion	N/A	ft	H	S	Qu	T	T
		(ft)	(ft)	(/6")	(tsf)	(%)	After	N/A	Hrs.	(ft)	(ft)	(/6")	(tsf)	(%)
LITHOLOGY							LITHOLOGY							
Brown and grey, medium stiff to very stiff, dry, SILTY CLAY (continued)							Grey, hard, dry, SILTY CLAY, trace gravel (continued)							
698.25														
Grey, medium dense, unsaturated, SAND, fine-grained														
9							29							
8							38							
-45							-65							
5							50/3.5"							
693.25														
Grey, very stiff to hard, dry, SILT														
10							20							
11							40							
13							50/5"							
-50							-70							
S							S							
10							15							
16							29							
19							42							
-55							-75							
S							B							
10.3							12							
683.25							663.25							
Grey, hard, dry, SILTY CLAY, trace gravel							Grey, very dense, dry, SAND, fine-grained							
15							50/2.5"							
29														
11.0														
10														
-60							-80							
46							B							

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



WB-4
SOIL BORING LOG
Sheet 3 of 3

COUNTY Champaign
SECTION (10-33HB-2)BR
ROUTE IL-72 and W Kirby over I-57
JOB NO. MG22080
DATE 1/11/2023

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO. WB-4 E L E V E N T H S Qu T
Note I-57 L E P L O S O I
Offset 75 ft Right E P T W S I
Stationing 482+30 (I-57) V T H S Qu T
740.0 ft
Surface Water Elev. N/A ft
Stream Bed Elev. N/A ft
Groundwater Elev.:
First Encounter N/E ft
Upon Completion N/A ft
After N/A Hrs. N/A ft

Elev.	LITHOLOGY	(ft)	(ft)	(/6")	(tsf)	(%)
	Grey, very dense, dry, SAND, fine-grained (continued)					
				50/4"		
		-85				
				32		
				50/5"		
		-90				
648.25	Grey, hard, dry, SILT					
				29		
				39	4.2	19
		-95		50/5"	S	
643.25	Grey, hard, dry, SILTY CLAY					
				29		
				40	4.6	19
640.00		-100		50/6"	S	

End of Boring
The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	WB-5	E	D	B	U	M	Surface Water Elev.	N/A	ft	E	D	B	U	M
Note	I-72	L	E	L	C	O	Stream Bed Elev.	N/A	ft	L	E	L	C	O
Offset	18 ft Left	E	P	O	S	I	Groundwater Elev.:			V	T	W	Q	S
Stationing	1962+50 (I-72)	V	H	S	Qu	T	First Encounter	734.1	ft	H	S	Qu	T	
Ground Surface Elev.	760.1	(ft)	(ft)	(/6")	(tsf)	(%)	Upon Completion	N/A	ft	(ft)	(ft)	(/6")	(tsf)	(%)
							After	N/A	Hrs.					
LITHOLOGY							LITHOLOGY							
Brown, stiff, dry, SILTY CLAY							Brown and grey, medium stiff to stiff, dry to moist, SILTY CLAY (continued)							
				3								3		
				5	1.4	14						4	3.0	27
				10	B							5	B	
				4								2		
				4	2.8	37						3	2.3	18
				-5	8	B						-25	4	B
				754.60										
Grey, stiff, dry, SANDY CLAY LOAM							▼							
				4								4		
				6	4.1	11						3	1.9	15
				7	S							4	B	
				752.10										
Brown and grey, medium stiff to stiff, dry to moist, SILTY CLAY							- 2" sand seam at 29.0 ft.							
				5								2		
				6	5.2	15						4	2.3	14
				-10	10	B						-30	6	B
				5										
				5	5.0	13								
				7	S									
				5										
				7	2.1	13						5		
				-15	10	S						-35	9	5.8
												11	B	11
				5										
				5	3.1	12						6		
				5										
				5	3.1	12						7	5.2	12
				-20	8	B						-40	9	B

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.



COUNTY Champaign
 SECTION (10-33HB-2)BR
 ROUTE IL-72 and W Kirby over I-57
 JOB NO. MG22080
 DATE 12/12/2022

WB-5
SOIL BORING LOG
 Sheet 3 of 3

DESCRIPTION PTB 195-042, WO #3 DISTRICT 5
 LOCATION Champaign, Illinois CONSULTANT Millennia Professional Services
 DRILLED BY MET LOGGED BY L. Williams RIG TYPE Diedrich D50
 DRILLING METHOD Hollow Stem Auger, Mud-Rotary HAMMER TYPE Automatic EFFICIENCY N/A

BORING NO.	WB-5	E	D	B	U	M	Surface Water Elev.	N/A	ft	
Note	I-72	L	E	L	C	O	Stream Bed Elev.	N/A	ft	
Offset	18 ft Left	E	P	O	S	I	Groundwater Elev.:			
Stationing	1962+50 (I-72)	V	T	W	Q	S	First Encounter	734.1	ft ▼	
Ground Surface Elev.	760.1 ft	H	S	Qu	T		Upon Completion	N/A	ft	
		(ft)	(ft)	(/6")	(tsf)	(%)	After	N/A	Hrs. N/A ft	
LITHOLOGY							LITHOLOGY			
Brown and grey, medium stiff to stiff, dry to moist, SILTY CLAY (continued)										
-switched to mud-rotary @ 80 feet 678.35										
Grey, hard, moist, SILT LOAM										
				45						
				50/5"		11				
				-85						
				673.35						
Grey, hard, moist, SILTY CLAY										
				15						
				24	11.5	11				
				36	B					
				-90						
				17						
				50/5.5"	12.1	10				
				-95	B					
				661.30						
				50/3.5"		13				
- trace gravel below 98.5 ft.										
End of Boring										
				-100						

The Unconfined Compressive Strength (UCS) Qu column represents either the IDOT Rimac or AASHTO T 208 Test Procedure. The Qu failure mode is indicated by B for Bulge or S for Shear. P is a Pocket Penetrometer test. The Standard Penetration Test (SPT) N value is the sum of the second and third Blows /6 in. values in each sample using AASHTO T 206.

Appendix E

Seismic Site Class Determination





SEISMIC SITE CLASS DETERMINATION

PROJECT TITLE=====**I-72 over I-57 (SN 010-0034)**

Substructure 1

Base of Substruct. Elev. (or ground surf for bents) **753.81** ft.
 Pile or Shaft Dia. **12** inches
 Boring Number **0034-EB-1**
 Top of Boring Elev. **761** ft.
 Approximate Fixity Elev. **747.81** ft.

Individual Site Class Definition:

N (bar): 22 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 100 (Blows/ft.) Soil Site Class C
 s_u (bar): 2.97 (ksf) Soil Site Class C <----Controls

Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample		Layer Description Boundary
		Thick. (ft.)	N Qu (tsf)	
	758.0	3.00	20 2.90	
	755.5	2.50	13 1.20	
	753.0	2.50	11 4.00	
	750.5	2.50	12 4.00	B
	748.0	2.50	13 2.30	
2.3	745.5	2.50	11 4.10	
7.3	740.5	5.00	11 3.60	B
9.8	738.0	2.50	5 2.70	
12.3	735.5	2.50	5 1.70	B
14.8	733.0	2.50	13 5.20	
17.3	730.5	2.50	14 4.80	
22.3	725.5	5.00	24 2.10	B
27.3	720.5	5.00	9 2.90	
32.3	715.5	5.00	8 3.20	
37.3	710.5	5.00	24	
42.3	705.5	5.00	21 1.70	
47.3	700.5	5.00	13 3.40	
52.3	695.5	5.00	10 3.40	
57.3	690.5	5.00	27	
62.3	685.5	5.00	33 1.90	
67.3	680.5	5.00	18 0.60	
72.3	675.5	5.00	100 1.50	B
77.3	670.5	5.00	100 12.10	
82.3	665.5	5.00	81 12.10	B
87.3	660.5	5.00	100	
92.3	655.5	5.00	100	
97.3	650.5	5.00	100	
100.5	647.3	3.20	100	B

Substructure 2

Base of Substruct. Elev. (or ground surf for bents) **731.47** ft.
 Pile or Shaft Dia. _____ inches
 Boring Number **0034-EB-2**
 Top of Boring Elev. **739.8** ft.
 Approximate Fixity Elev. **731.47** ft.

Individual Site Class Definition:

N (bar): 32 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 100 (Blows/ft.) Soil Site Class C
 s_u (bar): 4.4 (ksf) Soil Site Class C <----Controls

Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample		Layer Description Boundary
		Thick. (ft.)	N Qu (tsf)	
	737.3	2.50	15 2.50	B
	734.8	2.50	7 1.30	
	732.3	2.50	14 6.10	
1.7	729.8	2.50	9 6.20	
6.7	724.8	5.00	20 8.10	
9.2	722.3	2.50	17 5.30	
11.7	719.8	2.50	17 4.90	B
14.2	717.3	2.50	15 4.80	
16.7	714.8	2.50	17 5.10	
19.2	712.3	2.50	16 3.40	
21.7	709.8	2.50	23 7.70	
26.7	704.8	5.00	20 5.00	
31.7	699.8	5.00	17 2.00	
36.7	694.8	5.00	16 1.90	
41.7	689.8	5.00	20 5.30	
46.7	684.8	5.00	25	B
51.7	679.8	5.00	93 10.90	
55.7	675.8	4.00	100 3.50	
61.7	669.8	6.00	73 9.70	
66.7	664.8	5.00	100 10.10	B
70.2	661.3	3.50	100	
75.7	655.8	5.00	100	B
80.7	650.8	5.00	100	B
85.7	645.8	5.00	100	
90.7	640.8	5.00	100	
95.7	635.8	5.00	100	
100.0	631.5	4.30	100	B

Substructure 3

Base of Substruct. Elev. (or ground surf for bents) **731.51** ft.
 Pile or Shaft Dia. _____ inches
 Boring Number **0034-EB-3**
 Top of Boring Elev. **737.7** ft.
 Approximate Fixity Elev. **731.51** ft.

Individual Site Class Definition:

N (bar): 31 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 100 (Blows/ft.) NA
 s_u (bar): 3.82 (ksf) Soil Site Class C <----Controls

Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample		Layer Description Boundary
		Thick. (ft.)	N Qu (tsf)	
	734.7	3.00	17	B
	732.7	2.00	9 3.30	
1.3	730.2	2.50	10 4.10	
3.8	727.7	2.50	12 6.10	
8.8	722.7	5.00	11 4.90	
11.3	720.2	2.50	16 2.90	
13.8	717.7	2.50	16 4.20	
16.3	715.2	2.50	13 5.10	
18.8	712.7	2.50	12 1.80	
21.3	710.2	2.50	9 3.10	
23.8	707.7	2.50	11 3.60	
28.8	702.7	5.00	4 5.50	
33.8	697.7	5.00	10 0.90	
38.8	692.7	5.00	17 1.50	
43.8	687.7	5.00	21 2.90	
48.8	682.7	5.00	26 1.80	
53.8	677.7	5.00	86	
58.8	672.7	5.00	53 8.20	
63.8	667.7	5.00	43 7.60	B
67.8	663.7	4.00	100	B
72.8	658.7	5.00	100	
77.8	653.7	5.00	100	
82.8	648.7	5.00	100	
87.8	643.7	5.00	100	
92.8	638.7	5.00	100	
97.8	633.7	5.00	100	
100.0	631.5	2.20	100	B

Substructure 4

Base of Substruct. Elev. (or ground surf for bents) **731.51** ft.
 Pile or Shaft Dia. _____ inches
 Boring Number **0034-EB-4**
 Top of Boring Elev. **739.8** ft.
 Approximate Fixity Elev. **731.51** ft.

Individual Site Class Definition:

N (bar): 42 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 100 (Blows/ft.) Soil Site Class C
 s_u (bar): 3.32 (ksf) Soil Site Class C <----Controls

Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample		Layer Description Boundary
		Thick. (ft.)	N Qu (tsf)	
	737.3	2.50	12 4.60	
	734.8	2.50	9 2.90	
	732.3	2.50	12 3.10	
1.7	729.8	2.50	10 2.90	B
6.7	724.8	5.00	12 3.90	
9.2	722.3	2.50	11 2.90	
11.7	719.8	2.50	11 2.40	
14.2	717.3	2.50	9 1.80	
16.7	714.8	2.50	8 1.70	
19.2	712.3	2.50	9 1.90	
21.7	709.8	2.50	7 1.40	
25.7	705.8	4.00	100	
31.7	699.8	6.00	17 4.00	
36.7	694.8	5.00	25 1.90	
41.7	689.8	5.00	26 6.10	
46.7	684.8	5.00	17 2.50	
51.7	679.8	5.00	73 7.30	
56.7	674.8	5.00	62 9.40	
61.7	669.8	5.00	66 11.30	
66.7	664.8	5.00	100 8.50	B
70.7	660.8	4.00	100	
75.7	655.8	5.00	100	
80.7	650.8	5.00	100	B
85.7	645.8	5.00	100	
90.7	640.8	5.00	100	
95.7	635.8	5.00	100	
100.0	631.5	4.30	100	B

Global Site Class Definition: Substructures 1 through 5

N (bar): 29 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 84 (Blows/ft.) Soil Site Class C
 s_u (bar): 3.63 (ksf) Soil Site Class C <----Controls



SEISMIC SITE CLASS DETERMINATION

PROJECT TITLE=====**I-72 over I-57 (SN 010-0035)**

Substructure 1

Base of Substruct. Elev. (or ground surf for bents) **753.87** ft.
 Pile or Shaft Dia. **12** inches
 Boring Number **0035-WB-1**
 Top of Boring Elev. **760.6** ft.

Approximate Fixity Elev. **747.87** ft.

Individual Site Class Definition:

N (bar): **20** (Blows/ft.) Soil Site Class D
 N_{ch} (bar): **NA** (Blows/ft.) NA
 s_u (bar): **2.11** (ksf) Soil Site Class C <----Controls

Seismic Soil Column	Bot. Of Sample Elevation (ft)	Thick. (ft)	Sample		Layer Description
			N (tsf)	Qu (tsf)	
	758.1	2.50	10	2.10	B
	755.6	2.50	9	4.00	
	753.1	2.50	12	3.50	
	750.6	2.50	10	3.70	B
2.3	745.6	5.00	15	3.20	B
4.8	743.1	2.50	10	5.30	
7.3	740.6	2.50	9	2.80	
9.8	738.1	2.50	8	3.80	
12.3	735.6	2.50	7	2.70	B
14.8	733.1	2.50	21	9.60	
17.3	730.6	2.50	18	4.50	B
22.3	725.6	5.00	16	7.20	
27.3	720.6	5.00	13	2.30	
32.3	715.6	5.00	11	2.90	
37.3	710.6	5.00	12	2.80	B
42.3	705.6	5.00	11	0.20	B
47.3	700.6	5.00	30		B
52.3	695.6	5.00	24	4.90	
57.3	690.6	5.00	16		
62.3	685.6	5.00	15		B
67.3	680.6	5.00	51	8.70	B
72.3	675.6	5.00	64	10.90	
77.3	670.6	5.00	53	12.10	
82.3	665.6	5.00	53	12.10	
86.8	661.1	4.50	100	9.30	
91.8	656.1	5.00	100		
96.8	651.1	5.00	100		
100.0	647.9	3.20			B

Substructure 2

Base of Substruct. Elev. (or ground surf for bents) **731.67** ft.
 Pile or Shaft Dia. _____ inches
 Boring Number **0035-WB-2**
 Top of Boring Elev. **740.1** ft.

Approximate Fixity Elev. **731.67** ft.

Individual Site Class Definition:

N (bar): **32** (Blows/ft.) Soil Site Class D
 N_{ch} (bar): **NA** (Blows/ft.) NA
 s_u (bar): **3.85** (ksf) Soil Site Class C <----Controls

Seismic Soil Column	Bot. Of Sample Elevation (ft)	Thick. (ft)	Sample		Layer Description
			N (tsf)	Qu (tsf)	
	737.6	2.50	12		B
	735.1	2.50	10	3.40	
	732.6	2.50	15	5.50	
1.6	730.1	2.50	12	3.60	
6.6	725.1	5.00	19	7.00	
9.1	722.6	2.50	17	3.30	
11.6	720.1	2.50	17	3.40	
14.1	717.6	2.50	18	4.60	
16.6	715.1	2.50	17	4.70	B
19.1	712.6	2.50	17		B
21.6	710.1	2.50	20	6.60	
26.6	705.1	5.00	18	0.60	B
31.6	700.1	5.00	30		B
36.6	695.1	5.00	25	4.50	
41.6	690.1	5.00	28	5.10	
46.6	685.1	5.00	23	5.00	
51.6	680.1	5.00	62	10.10	
56.6	675.1	5.00	100	12.10	
61.6	670.1	5.00	71	12.10	
66.6	665.1	5.00	50	7.70	B
70.6	661.1	4.00	10		B
76.6	655.1	6.00	44	2.80	
81.6	650.1	5.00	100	5.50	
86.6	645.1	5.00	100	1.40	
90.6	641.1	4.00	100		
95.6	636.1	5.00	100		
100.0	631.7	4.40	100		B

Substructure 3

Base of Substruct. Elev. (or ground surf for bents) **731.51** ft.
 Pile or Shaft Dia. _____ inches
 Boring Number **0035-WB-3**
 Top of Boring Elev. **739.9** ft.

Approximate Fixity Elev. **731.51** ft.

Individual Site Class Definition:

N (bar): **28** (Blows/ft.) Soil Site Class D
 N_{ch} (bar): **100** (Blows/ft.) Soil Site Class C
 s_u (bar): **4.38** (ksf) Soil Site Class C <----Controls

Seismic Soil Column	Bot. Of Sample Elevation (ft)	Thick. (ft)	Sample		Layer Description
			N (tsf)	Qu (tsf)	
	737.4	2.50	14	2.40	B
	734.9	2.50	21		B
	732.4	2.50	8	2.60	
1.6	729.9	2.50	12	2.50	
6.6	724.9	5.00	13	5.50	
9.1	722.4	2.50	12	6.20	
11.6	719.9	2.50	8	6.00	
14.1	717.4	2.50	12	6.50	
16.6	714.9	2.50	14	4.50	
19.1	712.4	2.50	12	2.80	
21.6	709.9	2.50	12	3.30	
26.6	704.9	5.00	11	5.90	B
31.6	699.9	5.00	12		B
36.6	694.9	5.00	14	3.00	
41.6	689.9	5.00	17	4.30	
46.6	684.9	5.00	10	4.00	
51.6	679.9	5.00	77	8.00	
56.6	674.9	5.00	90	6.70	
61.6	669.9	5.00	63	11.10	
65.1	666.4	3.50	100	4.50	
69.6	659.9	6.50	100	8.00	
76.6	654.9	5.00	68	6.50	
81.6	649.9	5.00	100	3.30	B
86.6	644.9	5.00	100		B
90.6	640.9	4.00	100		
95.6	635.9	5.00	100		
100.0	631.5	4.40	100		B

Substructure 4

Base of Substruct. Elev. (or ground surf for bents) **731.3** ft.
 Pile or Shaft Dia. _____ inches
 Boring Number **0035-WB-4**
 Top of Boring Elev. **740** ft.

Approximate Fixity Elev. **731.3** ft.

Individual Site Class Definition:

N (bar): **28** (Blows/ft.) Soil Site Class D
 N_{ch} (bar): **NA** (Blows/ft.) NA
 s_u (bar): **3.96** (ksf) Soil Site Class C <----Controls

Seismic Soil Column	Bot. Of Sample Elevation (ft)	Thick. (ft)	Sample		Layer Description
			N (tsf)	Qu (tsf)	
	737.5	2.50	10	3.40	
	735.0	2.50	7	1.50	
	732.5	2.50	7	1.20	
1.3	730.0	2.50	10	3.50	
6.3	725.0	5.00	12	4.00	
8.8	722.5	2.50	15	4.60	
11.3	720.0	2.50	17	4.60	
13.8	717.5	2.50	15	3.70	
16.3	715.0	2.50	12	2.90	
18.8	712.5	2.50	15	3.60	
21.3	710.0	2.50	16	2.50	
26.3	705.0	5.00	14	3.90	
31.3	700.0	5.00	17	5.10	B
36.3	695.0	5.00	13		B
41.3	690.0	5.00	24	4.70	
46.3	685.0	5.00	35	3.50	B
51.3	680.0	5.00	75	11.00	
56.3	675.0	5.00	100	12.10	
61.3	670.0	5.00	100	12.10	
66.3	665.0	5.00	71	10.30	B
69.8	661.5	3.50	100		
74.8	656.5	5.00	100		
80.3	651.0	5.50	100		B
85.8	645.5	5.50	100	4.20	B
90.8	640.5	5.00	100	4.60	
95.8	635.5	5.00	100		
100.0	631.3	4.20	100		B

Global Site Class Definition: Substructures 1 through 5

N (bar): **27** (Blows/ft.) Soil Site Class D
 N_{ch} (bar): **NA** (Blows/ft.) NA, H < 0.1*H (Total)
 s_u (bar): **3.5** (ksf) Soil Site Class C <----Controls

Appendix F

Integral Abutment Feasibility Analysis





GENERAL DATA

STRUCTURE NUMBER=====010-0296 (EB)
 STRUCTURE TYPE =====MULTI-SPAN
 STRUCTURE SKEW=====0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1

TOTAL STRUCTURE LENGTH=====272.33 FT
 NUMBER OF SPANS =====4
 END SPAN LENGTH =====51.83 FT
 ADJACENT INTERIOR SPAN LENGTH =====84.33 FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)	
BEAM TYPE =====	WIDE FLANGE
WIDE FLANGE =====	W33X130
BEAM SPACING PERP. TO CL =====	7.08 FT
SLAB THICKNESS =====	8.00 IN
SLAB F'C =====	4.00 KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)	
WIDE FLANGE =====	W33X130
BEAM SPACING PERP. TO CL =====	7.08 FT
SLAB THICKNESS =====	8.00 IN
SLAB F'C =====	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME =====	West
ABUTMENT REFERENCE BORING =====	EB-1
BOTTOM OF ABUTMENT ELEVATION =====	753.81 FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	9
PILE SPACING PERP. TO CL =====	7.08 FT

ABUTMENT #2 DATA	
ABUTMENT NAME =====	East
ABUTMENT REFERENCE BORING =====	EB-5
BOTTOM OF ABUTMENT ELEVATION =====	753.56 FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	9
PILE SPACING PERP. TO CL =====	7.08 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
752.00	1.81	4.0		
750.50	1.50	4.0		
748.00	2.50	2.3		
745.50	2.50	4.1		
743.81	1.69	4.1		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
751.06	2.50	4.9		
748.56	2.50	5.7		
746.06	2.50	3.4		
743.56	2.50	3.40		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1=====: 3.62 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2=====: 4.35 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*3.62])===== 2.74

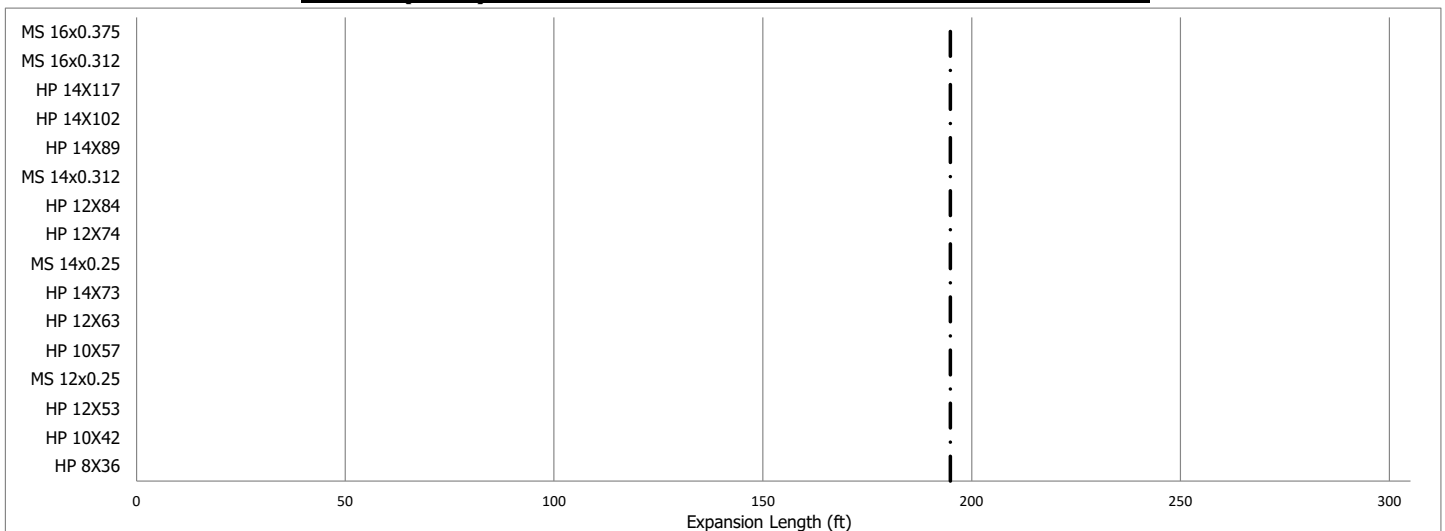
PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*4.35])===== 6.90

WEIGHTED AVG. Qu > 3.0 TSF WITH TRIB. LENGTH > 20%, INTEGRAL ABUTMENT STRUCTURE NOT ALLOWED

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [2.74*9*0+6.9*9*272.33]/[2.74*9+6.9*9]===== 194.89 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [6.9*9*0+2.74*9*272.33]/[6.9*9+2.74*9]===== 77.44 FT

ABUT 1 (West) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)



GENERAL DATA

STRUCTURE NUMBER=====010-0297 (WB)
 STRUCTURE TYPE =====MULTI-SPAN
 STRUCTURE SKEW=====0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1

TOTAL STRUCTURE LENGTH=====272.33 FT
 NUMBER OF SPANS =====4
 END SPAN LENGTH =====51.83 FT
 ADJACENT INTERIOR SPAN LENGTH =====84.33 FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)	
BEAM TYPE =====	WIDE FLANGE
WIDE FLANGE =====	W33X130
BEAM SPACING PERP. TO CL =====	7.08 FT
SLAB THICKNESS =====	8.00 IN
SLAB F'C =====	4.00 KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)	
WIDE FLANGE =====	W33X130
BEAM SPACING PERP. TO CL =====	7.08 FT
SLAB THICKNESS =====	8.00 IN
SLAB F'C =====	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME =====	West
ABUTMENT REFERENCE BORING =====	WB-1
BOTTOM OF ABUTMENT ELEVATION =====	753.87 FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	9
PILE SPACING PERP. TO CL =====	7.08 FT

ABUTMENT #2 DATA	
ABUTMENT NAME =====	East
ABUTMENT REFERENCE BORING =====	WB-5
BOTTOM OF ABUTMENT ELEVATION =====	753.52 FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	9
PILE SPACING PERP. TO CL =====	7.08 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUITV. FOR N VALUE (TSF)
752.00	1.87	3.5		
750.50	1.50	3.7		
748.00	2.50	3.2		
745.50	2.50	3.2		
743.87	1.63	5.3		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUITV. FOR N VALUE (TSF)
752.00	1.52	1.4		
750.50	1.50	2.8		
748.00	2.50	4.1		
745.50	2.50	5.20		
743.52	1.98	5.00		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 3.67 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 3.95 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*3.67])===== 2.87

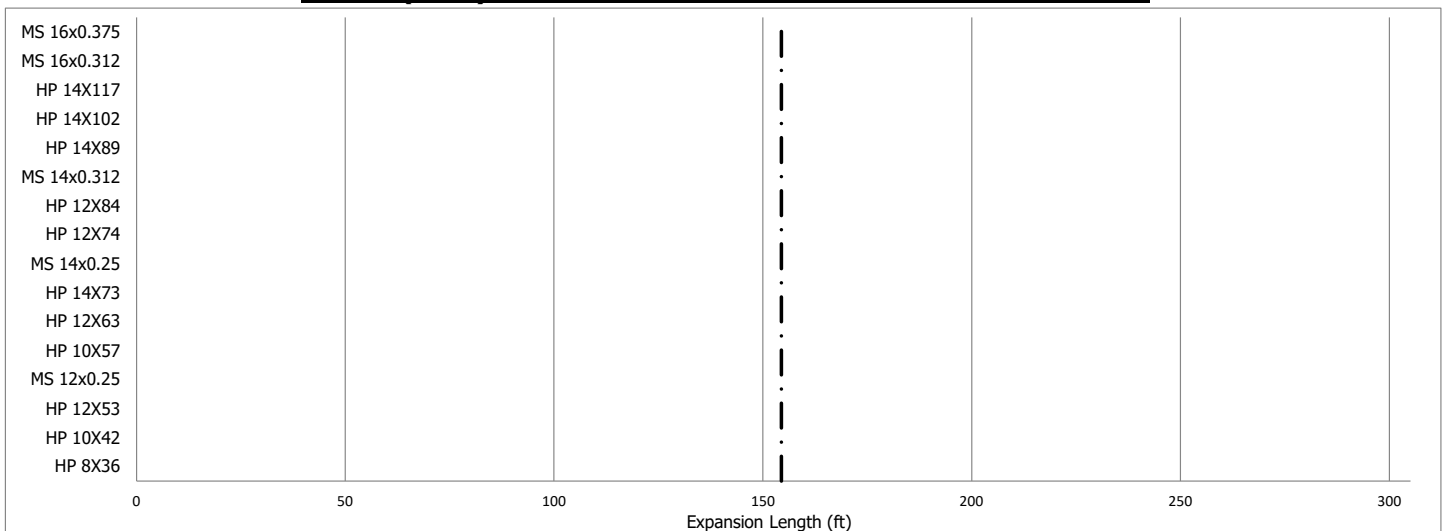
PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*3.95])===== 3.76

WEIGHTED AVG. Qu > 3.0 TSF WITH TRIB. LENGTH > 20%, INTEGRAL ABUTMENT STRUCTURE NOT ALLOWED

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [2.87*9*0+3.76*9*272.33]/[2.87*9+3.76*9]===== 154.43 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [3.76*9*0+2.87*9*272.33]/[3.76*9+2.87*9]===== 117.90 FT

ABUT 1 (West) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



--- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)



GENERAL DATA

STRUCTURE NUMBER=====010-0296/0297
 STRUCTURE TYPE =====MULTI-SPAN
 STRUCTURE SKEW=====0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1

TOTAL STRUCTURE LENGTH=====272.33 FT
 NUMBER OF SPANS =====4
 END SPAN LENGTH =====51.83 FT
 ADJACENT INTERIOR SPAN LENGTH =====84.33 FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)	
BEAM TYPE =====	WIDE FLANGE
WIDE FLANGE =====	W33X130
BEAM SPACING PERP. TO CL =====	7.08 FT
SLAB THICKNESS =====	8.00 IN
SLAB F'C =====	4.00 KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)	
WIDE FLANGE =====	W33X130
BEAM SPACING PERP. TO CL =====	7.08 FT
SLAB THICKNESS =====	8.00 IN
SLAB F'C =====	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME =====	West
ABUTMENT REFERENCE BORING =====	EB-1
BOTTOM OF ABUTMENT ELEVATION =====	753.81 FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	9
PILE SPACING PERP. TO CL =====	7.08 FT

ABUTMENT #2 DATA	
ABUTMENT NAME =====	East
ABUTMENT REFERENCE BORING =====	EB-5
BOTTOM OF ABUTMENT ELEVATION =====	753.56 FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	9
PILE SPACING PERP. TO CL =====	7.08 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
751.31	2.50	1.5		
748.81	2.50	1.5		
746.31	2.50	1.5		
743.81	2.50	1.5		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
751.06	2.50	1.5		
748.56	2.50	1.5		
746.06	2.50	1.5		
743.56	2.50	1.50		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1=====: 1.50 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2=====: 1.50 TSF

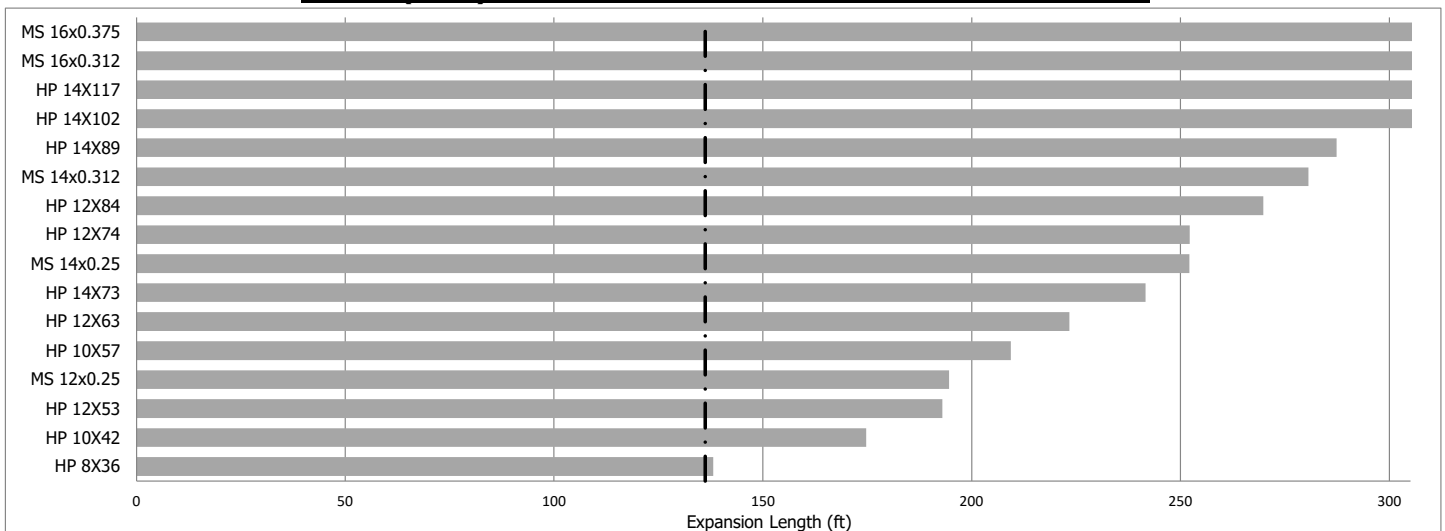
PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*1.5])===== 1.00

PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*1.5])===== 1.00

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [1*9*0+1*9*272.33]/[1*9+1*9]===== 136.17 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [1*9*0+1*9*272.33]/[1*9+1*9]===== 136.17 FT

ABUT 1 (West) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)

Appendix G

Driven Pile Analysis



SUBSTRUCTURE===== **West Abutment - 0296**
 REFERENCE BORING ===== **EB-1**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **755.81** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **743.81** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1550** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **62.83** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 197.36 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 74.01 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	447 KIPS	246 KIPS	59 FT.

PILE TYPE AND SIZE ===== **Metal Shell 14"Φ w/.25" walls**
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
742.00	1.81	4.10	11		20.1		62.3	62	0	0	34	14
740.50	1.50	3.60	11		15.1	42.2	66.8	67	0	0	37	15
738.00	2.50	2.70			20.4	31.7	75.4	75	0	0	41	18
735.50	2.50	1.70			15.0	19.9	131.5	131	0	0	72	20
732.00	3.50	5.20	13		41.7	61.0	168.5	169	0	0	93	24
727.00	5.00	4.80	14		59.6	56.3	196.5	197	0	0	108	29
724.25	2.75	2.10			18.9	24.6	224.8	225	0	0	124	32
720.50	3.75	2.90			32.1	34.0	257.0	257	0	0	141	35
717.00	3.50	2.90			30.0	34.0	290.5	290	0	0	160	39
712.00	5.00	3.20	8		46.0	37.5	318.9	319	0	0	175	44
707.00	5.00	1.70			30.0	19.9	348.9	349	0	0	192	49
702.00	5.00	1.70			30.0	19.9	398.9	399	0	0	219	54
697.00	5.00	3.40	13		48.1	39.9	447.0	447	0	0	246	59
692.00	5.00	3.40	10		48.1	39.9	477.5	477	0	0	263	64
687.00	5.00	1.90			32.3	22.3	509.8	510	0	0	280	69
682.00	5.00	1.90			32.3	22.3	526.8	527	0	0	290	74
677.00	5.00	0.60			13.2	7.0	550.6	551	0	0	303	79
674.25	2.75	1.50			15.2	17.6	1052.9	4053	0	0	579	82
670.75	3.50		100	Hard Till	139.7	504.7	1192.6	4193	0	0	656	85
667.25	3.50		100	Hard Till	139.7	504.7	1236.4	4236	0	0	680	89
662.25	5.00		81	Hard Till	134.6	408.8	1466.9	4467	0	0	807	94
657.25	5.00		100	Hard Till		504.7			0	0		



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== East Abutment - 0296
 REFERENCE BORING ===== EB-5
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 755.56 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 743.56 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1550 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 58.83 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 210.78 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 79.04 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	451 KIPS	248 KIPS	54 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
742.00	1.56	6.60	13		18.6		72.5	73	0	0	40	14
739.50	2.50	4.60	17		29.8	53.9	95.3	95	0	0	52	16
737.00	2.50	4.00	14		27.2	46.9	130.7	131	0	0	72	19
734.50	2.50	4.70	12		29.8	55.1	139.4	139	0	0	77	21
731.00	3.50	2.90			30.0	34.0	176.5	176	0	0	97	25
728.50	2.50	3.50	8		24.6	41.0	188.1	188	0	0	103	27
726.00	2.50	2.40			18.8	28.1	224.5	225	0	0	123	30
721.00	5.00	3.90	11		53.3	45.7	261.4	261	0	0	144	35
718.25	2.75	2.50			21.3	29.3	253.4	253	0	0	139	37
713.25	5.00		11	Fine Sand	0.0	0.0	305.0	305	0	0	168	42
709.75	3.50	4.40	11		41.0	51.6	346.0	346	0	0	190	46
706.25	3.50	4.40	11		41.0	51.6	389.3	389	0	0	214	49
701.25	5.00	4.60	10		59.6	53.9	451.3	451	0	0	248	54
696.25	5.00	4.80	12		59.6	56.3	522.7	523	0	0	287	59
691.25	5.00	5.80	13		59.6	68.0	584.6	585	0	0	322	64
686.25	5.00	6.00	17		59.6	70.4	653.6	654	0	0	360	69
681.25	5.00	6.80	21		59.6	79.7	698.0	698	0	0	384	74
676.25	5.00	5.50	17		59.6	64.5	693.2	693	0	0	384	79
673.25	3.00		79	Hard Till	0.0	0.0	693.2	693	0	0	384	82
668.25	5.00		59	Hard Till	0.0	0.0	1026.3	1026	0	0	564	87
663.25	5.00		66	Hard Till	93.3	333.1	786.4	786	0	0	433	92
659.75	3.50		100	Hard Till	0.0	0.0	786.4	786	0	0	433	96
654.75	5.00		100	Fine Sand		0.0						

SUBSTRUCTURE===== **West Abutment - 0297**
 REFERENCE BORING ===== **WB-1**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **755.87** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **743.87** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1550** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **58.83** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 210.78 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 79.04 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	335 KIPS	185 KIPS	47 FT.

PILE TYPE AND SIZE ===== **Metal Shell 14"Φ w/.25" walls**
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
743.00	0.87	5.30	10		10.4		43.2	43	0	0	24	13
740.50	2.50	2.80			20.9	32.8	75.8	76	0	0	42	15
738.00	2.50	3.80	8		26.1	44.6	89.1	89	0	0	49	18
735.50	2.50	2.70			20.4	31.7	190.3	190	0	0	105	20
732.50	3.00	9.60	21		35.8	112.6	166.3	166	0	0	91	23
729.25	3.25	4.50	18		38.8	52.8	236.7	237	0	0	130	27
724.25	5.00	7.20	16		59.6	84.4	238.9	239	0	0	131	32
719.25	5.00	2.30			36.5	27.0	282.5	282	0	0	155	37
714.25	5.00	2.90			42.8	34.0	324.2	324	0	0	178	42
709.25	5.00	2.80			41.8	32.8	335.5	335	0	0	185	47
704.25	5.00	0.20			4.7	2.3	539.7	540	0	0	297	52
701.75	2.50		30	Fine Sand	24.0	201.9	563.7	564	0	0	310	54
699.25	2.50		30	Fine Sand	24.0	201.9	443.2	443	0	0	244	57
694.25	5.00	4.90	24		59.6	57.5	502.9	503	0	0	277	62
689.25	5.00	4.90	16		59.6	57.5	562.5	562	0	0	309	67
684.25	5.00	4.90	15		59.6	57.5	564.7	565	0	0	311	72
679.25	5.00		51	Hard Till	0.0	0.0	887.7	888	0	0	488	77
674.25	5.00		64	Hard Till	88.4	323.0	920.6	921	0	0	506	82
669.25	5.00		53	Hard Till	64.6	267.5	985.2	985	0	0	542	87
664.25	5.00		53	Hard Till	64.6	267.5	782.3	782	0	0	430	92
659.25	5.00		100	Hard Till		0.0						

SUBSTRUCTURE===== **East Abutment - 0297**
 REFERENCE BORING ===== **WB-5**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **755.52** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **743.52** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1550** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **62.83** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 197.36 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 74.01 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	434 KIPS	239 KIPS	53 FT.

PILE TYPE AND SIZE ===== **Metal Shell 14"Φ w/.25" walls**
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
743.00	0.52	5.00	12		6.2		30.8	31	0	0	17	13
738.00	5.00	2.10			34.4	24.6	77.0	77	0	0	42	18
735.50	2.50	3.10	13		22.5	36.3	98.3	98	0	0	54	20
733.00	2.50	3.00	9		21.9	35.2	112.0	112	0	0	62	23
730.50	2.50	2.30			18.3	27.0	125.6	126	0	0	69	25
728.00	2.50	1.90			16.2	22.3	146.5	146	0	0	81	28
723.00	5.00	2.30	10		36.5	27.0	224.0	224	0	0	123	33
718.00	5.00	5.80	20		59.6	68.0	276.6	277	0	0	152	38
713.00	5.00	5.20	16		59.6	61.0	323.4	323	0	0	178	43
708.00	5.00	4.10	13		55.4	48.1	378.8	379	0	0	208	48
703.00	5.00	4.10	18		55.4	48.1	434.2	434	0	0	239	53
698.00	5.00	4.10	18		55.4	48.1	489.7	490	0	0	269	58
693.00	5.00	4.10	22		55.4	48.1	545.1	545	0	0	300	63
688.00	5.00	4.10	20		55.4	48.1	552.5	552	0	0	304	68
683.00	5.00		49	Hard Till	0.0	0.0	597.0	597	0	0	328	73
678.00	5.00	3.80	16		52.3	44.6	604.7	605	0	0	333	78
673.00	5.00		92	Hard Till	0.0	0.0	604.7	605	0	0	333	83
668.50	4.50		100	Hard Till	0.0	0.0	907.6	908	0	0	499	87
663.00	5.50		60	Hard Till	87.1	302.8	691.9	692	0	0	384	93
658.50	4.50		100	Hard Till	0.0	0.0	691.9	692	0	0	384	97
654.00	4.50		100	Hard Till		0.0						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 1 - 0296
 REFERENCE BORING ===== EB-2
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 732.50 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 731.50 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3000 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 55.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 2
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 218.18 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 81.82 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	416 KIPS	229 KIPS	37 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
730.80	0.70	6.10	14		8.3		81.0	81	0	0	45	2
725.80	5.00	6.20	9		59.6	72.7	163.0	163	0	0	90	7
723.30	2.50	8.10	20		29.8	95.0	159.9	160	0	0	88	9
720.80	2.50	5.30	17		29.8	62.1	185.1	185	0	0	102	12
718.30	2.50	4.90	17		29.8	57.5	213.7	214	0	0	118	14
715.80	2.50	4.80	15		29.8	56.3	247.0	247	0	0	136	17
713.30	2.50	5.10	17		29.8	59.8	256.9	257	0	0	141	19
710.80	2.50	3.40	16		24.0	39.9	331.4	331	0	0	182	22
705.80	5.00	7.70	23		59.6	90.3	359.4	359	0	0	198	27
700.80	5.00	5.00	20		59.6	58.6	383.8	384	0	0	211	32
695.80	5.00	2.00			33.4	23.5	416.0	416	0	0	229	37
690.80	5.00	1.90			32.3	22.3	488.2	488	0	0	269	42
685.80	5.00	5.30	20		59.6	62.1	547.9	548	0	0	304	47
680.80	5.00	5.30	25		59.6	62.1	1014.7	1015	0	0	558	52
675.80	5.00		93	Hard Till	174.0	469.4	1224.1	1224	0	0	673	57
670.80	5.00		100	Hard Till	199.6	504.7	1287.4	1287	0	0	708	62
665.80	5.00		73	Hard Till	111.5	368.4	1535.1	1535	0	0	844	67
660.80	5.00		100	Hard Till	199.6	504.7	1734.7	1735	0	0	954	72
655.80	5.00		100	Hard Till		504.7						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 2 - 0296
 REFERENCE BORING ===== EB-3
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 732.50 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 731.50 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3400 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 55.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 2
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 247.27 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 92.73 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	409 KIPS	225 KIPS	49 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
731.20	0.30	3.30	9		2.8		50.9	51	0	0	28	1
728.70	2.50	4.10	10		27.7	48.1	102.1	102	0	0	56	4
726.20	2.50	6.10	12		29.8	71.5	117.8	118	0	0	65	6
723.70	2.50	4.90	11		29.8	57.5	147.6	148	0	0	81	9
721.20	2.50	4.90	11		29.8	57.5	154.0	154	0	0	85	11
718.70	2.50	2.90			21.4	34.0	190.7	191	0	0	105	14
716.20	2.50	4.20	16		28.2	49.2	229.4	229	0	0	126	16
713.70	2.50	5.10	13		29.8	59.8	220.6	221	0	0	121	19
711.20	2.50	1.80			15.6	21.1	251.4	251	0	0	138	21
708.70	2.50	3.10	9		22.5	36.3	279.7	280	0	0	154	24
703.70	5.00	3.60	11		50.2	42.2	293.6	294	0	0	161	29
698.70	5.00	0.50			11.2	5.9	309.5	309	0	0	170	34
693.70	5.00	0.90			18.7	10.6	335.2	335	0	0	184	39
688.70	5.00	1.50			27.6	17.6	379.2	379	0	0	209	44
683.70	5.00	2.90			42.8	34.0	409.1	409	0	0	225	49
678.70	5.00	1.80			31.2	21.1	853.3	853	0	0	469	54
673.70	5.00		86	Hard Till	150.3	434.0	837.0	837	0	0	460	59
668.70	5.00		53	Hard Till	64.6	267.5	851.2	851	0	0	468	64
663.70	5.00		43	Hard Till	47.1	217.0	1185.9	1186	0	0	652	69
658.70	5.00		100	Hard Till	199.6	504.7	1553.7	1554	0	0	855	74
653.70	5.00		100	Fine Sand		672.9						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 3 - 0296
 REFERENCE BORING ===== EB-4
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 732.50 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 731.50 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3000 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 55.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 2
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 218.18 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 81.82 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	391 KIPS	215 KIPS	47 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
730.80	0.70	3.10	12		6.3		40.3	40	0	0	22	2
728.30	2.50	2.90			21.4	34.0	61.7	62	0	0	34	4
725.80	2.50	2.90			21.4	34.0	94.9	95	0	0	52	7
723.30	2.50	3.90	12		26.7	45.7	109.8	110	0	0	60	9
720.80	2.50	2.90			21.4	34.0	125.4	125	0	0	69	12
718.30	2.50	2.40			18.8	28.1	137.1	137	0	0	75	14
715.80	2.50	1.80			15.6	21.1	151.5	152	0	0	83	17
713.30	2.50	1.70			15.0	19.9	168.9	169	0	0	93	19
710.80	2.50	1.90			16.2	22.3	179.2	179	0	0	99	22
705.80	5.00	1.40			26.3	16.4	205.5	206	0	0	113	27
700.80	5.00	1.40			26.3	16.4	262.3	262	0	0	144	32
695.80	5.00	4.00	17		54.4	46.9	292.1	292	0	0	161	37
690.80	5.00	1.90			32.3	22.3	373.6	374	0	0	205	42
685.80	5.00	6.10	26		59.6	71.5	391.1	391	0	0	215	47
680.80	5.00	2.50			38.6	29.3	768.8	769	0	0	423	52
675.80	5.00		73	Hard Till	111.5	368.4	824.8	825	0	0	454	57
670.80	5.00		62	Hard Till	83.7	312.9	928.7	929	0	0	511	62
665.80	5.00		66	Hard Till	93.3	333.1	1133.0	1133	0	0	623	67
660.80	5.00		88	Hard Till		444.1						

SUBSTRUCTURE===== Pier 1 - 0297
 REFERENCE BORING ===== WB-2
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 732.50 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 731.50 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3000 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 55.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 2
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 218.18 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 81.82 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	411 KIPS	226 KIPS	41 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
731.10	0.40	5.50	15		4.8		47.0	47	0	0	26	1
726.10	5.00	3.60	12		50.2	42.2	137.0	137	0	0	75	6
723.60	2.50	7.00	19		29.8	82.1	123.5	123	0	0	68	9
721.10	2.50	3.30	17		23.5	38.7	148.2	148	0	0	81	11
718.60	2.50	3.40	17		24.0	39.9	186.3	186	0	0	102	14
716.10	2.50	4.60	18		29.8	53.9	217.3	217	0	0	119	16
714.60	1.50	4.70	17		17.9	55.1	294.4	294	0	0	162	18
712.10	2.50		17	Fine Sand	13.5	114.4	270.9	271	0	0	149	20
706.10	6.00	6.60	20		71.6	77.4	272.1	272	0	0	150	26
701.10	5.00	0.60			13.2	7.0	285.3	285	0	0	157	31
696.10	5.00	0.60			13.2	7.0	344.2	344	0	0	189	36
691.10	5.00	4.50	25		59.6	52.8	410.9	411	0	0	226	41
686.10	5.00	5.10	26		59.6	59.8	469.3	469	0	0	258	46
681.10	5.00	5.00	23		59.6	58.6	783.3	783	0	0	434	54
676.10	5.00		62	Hard Till	83.7	312.9	1038.6	1039	0	0	571	56
671.10	5.00		96	Hard Till	184.7	484.5	1097.2	1097	0	0	603	64
666.10	5.00		71	Hard Till	106.1	358.3	1097.2	1097	0	0	603	66
661.10	5.00		50	Hard Till		252.4						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 2 - 0297
 REFERENCE BORING ===== WB-3
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 732.50 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 731.50 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3400 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 55.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 2
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 247.27 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 92.73 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	425 KIPS	234 KIPS	42 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
730.90	0.60	2.60			4.8		34.1	34	0	0	19	2
728.40	2.50	2.50			19.3	29.3	53.4	53	0	0	29	4
725.90	2.50	2.50			19.3	29.3	107.9	108	0	0	59	7
723.40	2.50	5.50	13		29.8	64.5	145.9	146	0	0	80	9
720.90	2.50	6.20	12		29.8	72.7	173.4	173	0	0	95	12
718.40	2.50	6.00	8		29.8	70.4	209.1	209	0	0	115	14
715.90	2.50	6.50	12		29.8	76.2	215.4	215	0	0	118	17
713.40	2.50	4.50	14		29.8	52.8	225.3	225	0	0	124	19
710.90	2.50	2.80			20.9	32.8	252.1	252	0	0	139	22
705.90	5.00	3.30	12		47.0	38.7	329.6	330	0	0	181	27
703.15	2.75	5.90	11		32.8	69.2	374.0	374	0	0	206	29
698.15	5.00		12	Fine Sand	19.0	80.8	347.4	347	0	0	191	34
695.00	3.15	3.00			27.6	35.2	375.1	375	0	0	206	38
691.00	4.00	3.00			35.1	35.2	425.4	425	0	0	234	42
686.00	5.00	4.30	17		57.5	50.4	479.4	479	0	0	264	47
681.00	5.00	4.00	10		54.4	46.9	875.5	876	0	0	482	52
676.00	5.00		77	Hard Till	122.7	388.6	1063.9	4064	0	0	585	57
671.00	5.00		90	Hard Till	163.6	454.2	1091.2	4094	0	0	600	62
666.00	5.00		63	Hard Till	86.1	318.0	1364.0	4364	0	0	760	67
661.00	5.00		100	Hard Till		504.7						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 3 - 0297
 REFERENCE BORING ===== WB-4
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 732.50 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 731.50 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3000 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 55.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 2
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 218.18 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 81.82 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	459 KIPS	252 KIPS	43 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
731.00	0.50	1.20			2.4		43.4	43	0	0	24	2
728.50	2.50	3.50	10		24.6	41.0	68.0	68	0	0	37	4
726.00	2.50	3.50	10		24.6	41.0	98.4	98	0	0	54	7
723.50	2.50	4.00	12		27.2	46.9	132.6	133	0	0	73	9
721.00	2.50	4.60	15		29.8	53.9	162.4	162	0	0	89	12
718.50	2.50	4.60	17		29.8	53.9	181.7	182	0	0	100	14
716.00	2.50	3.70	15		25.6	43.4	197.9	198	0	0	109	17
713.50	2.50	2.90			21.4	34.0	227.6	228	0	0	125	19
711.00	2.50	3.60	15		25.1	42.2	239.8	240	0	0	132	22
706.00	5.00	2.50			38.6	29.3	294.8	295	0	0	162	27
701.00	5.00	3.90	14		53.3	45.7	362.2	362	0	0	199	32
698.25	2.75	5.10	17		32.8	59.8	422.7	423	0	0	232	34
693.25	5.00		13	Fine Sand	20.6	87.5	410.9	411	0	0	226	39
689.25	4.00	4.70	24		47.7	55.1	458.6	459	0	0	252	43
686.00	3.25	4.70	24		38.8	55.1	618.9	619	0	0	340	47
681.00	5.00		35	Hard Till	35.8	176.6	856.7	857	0	0	471	52
676.00	5.00		75	Hard Till	117.0	378.5	1099.8	1100	0	0	605	57
671.00	5.00		100	Hard Till	199.6	504.7	1299.4	1299	0	0	715	62
666.00	5.00		100	Hard Till		504.7						