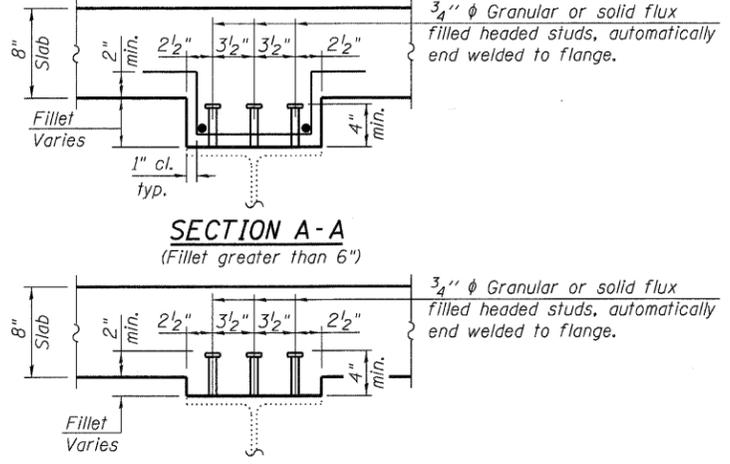


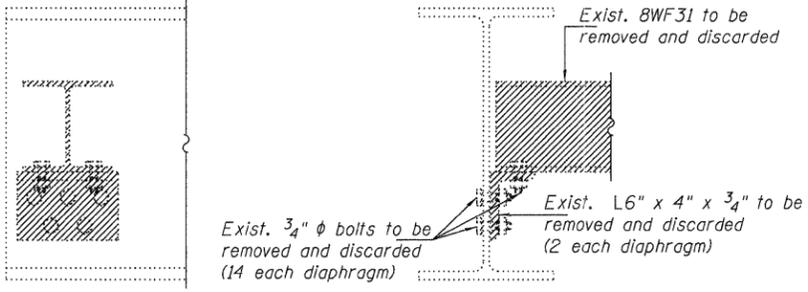
BEAM ELEVATION



SECTION A-A
(Fillet greater than 6")

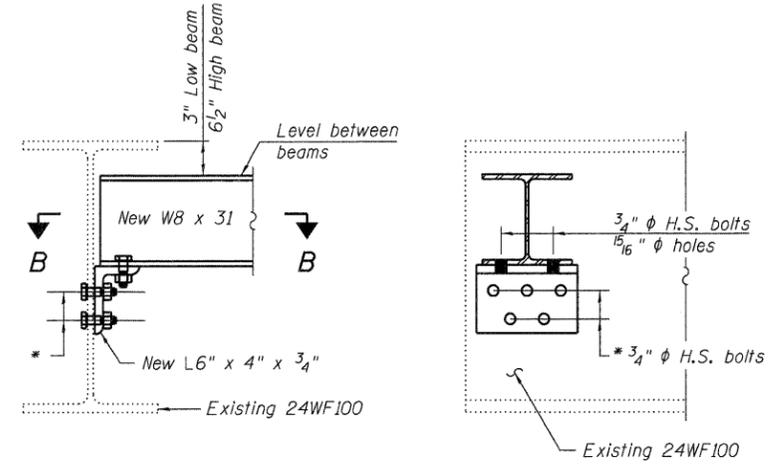
SECTION A-A
(Fillet less than 6")

Note:
Stud Shear Connectors required = 2,574/Bridge.



END DIAPHRAGM "D" REMOVAL DETAIL

(Total 20 Diaphragms to be removed. Cost included with Structural Steel Removal.)



END DIAPHRAGM "D"

(Total 16 required)

* Field drill 1 5/16" diameter holes in new connector angle L6" x 4" x 3/4" and connect with 3/4" diameter H.S. bolts. Use existing holes in beam web as a template. Cost included with Furnishing and Erecting Structural Steel.

Notes:
Two hardened washers shall be required over all oversized holes in diaphragms.

INTERIOR GIRDER MOMENT TABLE				
		0.4 Sp. 1 or 0.6 Sp. 3	Pier 1 & 2	0.5 Sp. 2
I_s	(in ⁴)	2987.3	2987.3	2987.3
$I_c(n)$	(in ⁴)	11962.5		11962.5
$I_c(3n)$	(in ⁴)	8468.6	8468.6	8468.6
$I_c(cr)$	(in ⁴)		5230.3	
S_s	(in ³)	248.9	248.9	248.9
$S_c(n)$	(in ³)	455.2		455.2
$S_c(3n)$	(in ³)	405.5	405.5	405.5
$S_c(cr)$	(in ³)		292.7	
Z	(in ³)			
ρ	(k/')	0.855	0.855	0.855
$M\rho$	(k)	98	156	72
$s\rho$	(k/')	0.310	0.310	0.310
$M_s\rho$	(k)	35	57	26
M_l	(k)	203	156	196
M_{I1}	(k)	61	47	57
$^{5/3}[M_l + i]$	(k)	439	338	422
M_o	(k)	744	717	676
M_u	(k)	1255		1284
$f_s \rho$ non-comp	(ksi)	4.7	7.5	3.5
$f_s \rho$ (comp)	(ksi)	1.0	2.3	0.8
$f_s (^{5/3}[M_l + M_{I1}])$	(ksi)	11.6	13.9	11.1
f_s (Overload)	(ksi)	17.3	23.7	15.4
f_s (Total)	(ksi)		30.8	
VR	(k)	29.6	53.4	31.2

I_s, S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total and Overload) due to non-composite dead loads (in⁴ and in³).

$I_c(n), S_c(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total and Overload) due to short-term composite live loads (in⁴ and in³).

$I_c(3n), S_c(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total and Overload) due to long-term composite (superimposed) dead loads (in⁴ and in³).

$I_c(cr), S_c(cr)$: Composite moment of inertia and section modulus of the steel and deck based upon the cracked concrete section with negative moment reinforcement. Used for computing f_s (Total and Overload) due to short and long-term composite dead and live loads in the negative moment region.

Z : Plastic Section Modulus of the steel section in non-composite areas (in³).

ρ : Un-factored non-composite dead load (kips/ft.).

$M\rho$: Un-factored moment due to non-composite dead load (kip-ft.).

$s\rho$: Un-factored long-term composite (superimposed) dead load (kips/ft.).

$M_s\rho$: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).

M_l : Un-factored live load moment (kip-ft.).

M_{I1} : Un-factored moment due to impact (kip-ft.).

M_o : Factored design moment (kip-ft.).

$1.3 [M\rho + M_s\rho + \frac{5}{3}(M_l + M_{I1})]$

M_u : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).

f_s (Overload): Sum of stresses as computed from the moments below (ksi).

$M\rho + M_s\rho + \frac{5}{3}(M_l + M_{I1})$

f_s (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).

$1.3 [M\rho + M_s\rho + \frac{5}{3}(M_l + M_{I1})]$

VR: Maximum $\frac{1}{2}$ + impact shear range within the composite portion of the span for stud shear connector design (kips).

INTERIOR GIRDER REACTION TABLE			
	W. Abut. & E. Abut.	Pier 1 & 2	
$R\rho$	(k)	46.7	55.3
R_l	(k)	34.1	42.1
R_I	(k)	10.2	10.0
R_{Total}	(k)	91.0	107.4

* Compact section
** Braced non-compact and partially braced section
*** Includes Approach Slab dead load reaction at Abutments.

BILL OF MATERIAL

Item	Unit	Total
Furnishing and Erecting Structural Steel	Pound	4,160
Structural Steel Removal	Pound	5,170
Stud Shear Connectors	Each	5,148