

**FRAMING PLAN**

"D" denotes Interior Diaphragm. See Sheet 13 of 19.

INTERIOR GIRDER MOMENT TABLE		0.5 Sp. 1
$I_s$	(in <sup>4</sup> )	4580
$I_c(n)$	(in <sup>4</sup> )	12,295
$I_c(3n)$	(in <sup>4</sup> )	8,940
$I_c(cr)$	(in <sup>4</sup> )	
$S_s$	(in <sup>3</sup> )	371
$S_c(n)$	(in <sup>3</sup> )	540
$S_c(3n)$	(in <sup>3</sup> )	486
$S_c(cr)$	(in <sup>3</sup> )	
DC1	(k/')	0.875
M <sub>DC1</sub>	(k)	336.9
DC2	(k/')	0.04
M <sub>DC2</sub>	(k)	15.4
DW	(k/')	0.35
M <sub>DW</sub>	(k)	134.8
$M_{\ell} + IM$	(k)	765.2
$M_u$ (Strength I)	(k)	1982
$\phi_r M_n$	(k)	2551
$f_s$ DC1	(ksi)	10.90
$f_s$ DC2	(ksi)	0.38
$f_s$ DW	(ksi)	3.33
$f_s$ ( $\ell + IM$ )	(ksi)	18.89
$f_s$ (Service II)	(ksi)	39.17
$0.95R_h F_y f$	(ksi)	47.5
$f_s$ (Total)(Strength I)	(ksi)	
$\phi_r F_n$	(ksi)	
$V_r$	(k)	22.2

INTERIOR GIRDER REACTION TABLE		Abut.
R <sub>DC1</sub>	(k)	24.3
R <sub>DC2</sub>	(k)	1.1
R <sub>DW</sub>	(k)	9.7
R $\ell + IM$	(k)	57.2
R <sub>Total</sub>	(k)	92.3

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) in uncracked sections, due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(cr), S_c(cr)$ : Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing  $f_s$  (Total-Strength I and Service II) in cracked sections, due to both short-term composite live loads and long-term composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

DC1: Un-factored non-composite dead load (kips/ft.).

M<sub>DC1</sub>: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

M<sub>DC2</sub>: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

M<sub>DW</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

$M_{\ell} + IM$ : Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).

$M_u$  (Strength I): Factored design moment (kip-ft.).

$1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_{\ell} + IM$

$\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).

$f_s$  DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi).

$M_{DC1} / S_{nc}$

$f_s$  DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).

$M_{DC2} / S_c(3n)$  or  $M_{DC2} / S_c(cr)$  as applicable.

$f_s$  DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).

$M_{DW} / S_c(3n)$  or  $M_{DW} / S_c(cr)$  as applicable.

$f_s$  ( $\ell + IM$ ): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).

$M_{\ell} + IM / S_c(3n)$  or  $M_{\ell} + IM / S_c(cr)$  as applicable.

$f_s$  (Service II): Sum of stresses as computed below (ksi).

$f_s DC1 + f_s DC2 + f_s DW + 1.3 f_s (\ell + IM)$

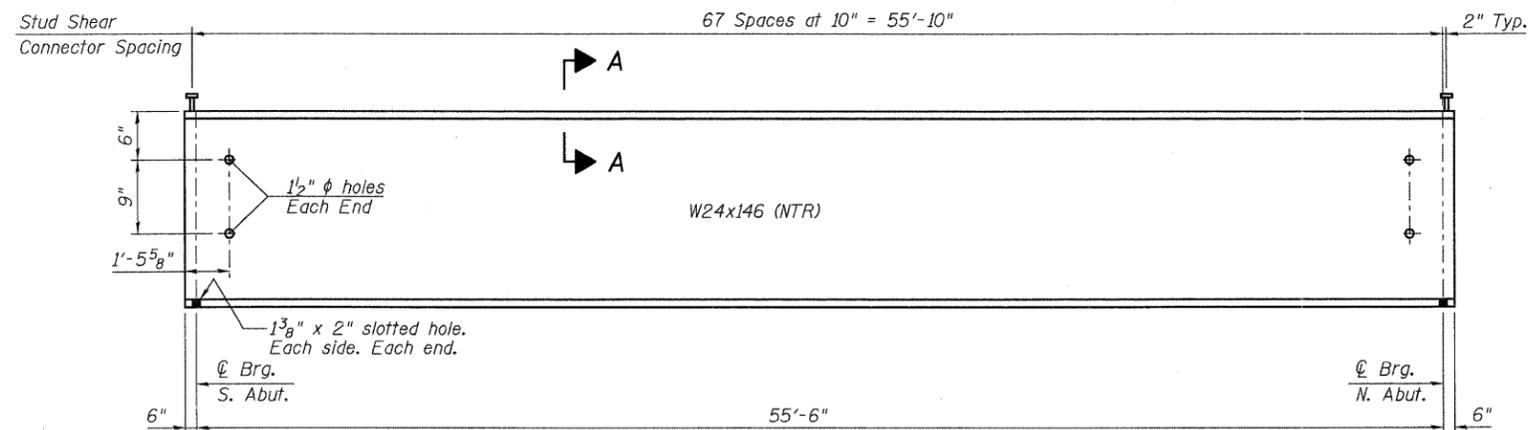
$0.95R_h F_y f$ : Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

$f_s$  (Total)(Strength I): Sum of stresses as computed below on non-compact section (ksi).

$1.25 (f_s DC1 + f_s DC2) + 1.5 f_s DW + 1.75 f_s (\ell + IM)$

$\phi_r F_n$ : Non-Compact composite positive or negative stress capacity for Strength I loading according to Article 6.10.7.2 (ksi).

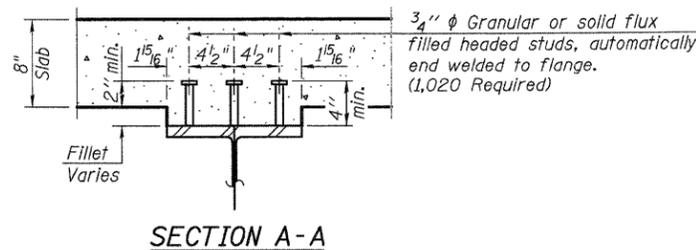
$V_r$ : Maximum factored shear range in composite portion of span computed according to Article 6.10.10.



**ELEVATION**

**TOP OF BEAM ELEVATIONS**  
(For Fabrication Only)

Location	Beam 1	Beam 2	Beam 3	Beam 4	Beam 5
Centerline S. Abut.	765.06	764.93	764.79	764.65	764.51
Centerline N. Abut.	763.96	763.82	763.68	763.54	763.40



**SECTION A-A**

**NOTES:**

All beams shall be W24x146 AASHTO M270 Grade 50W (NTR). All diaphragms and connecting angles shall be AASHTO M270 Grade 50W. All bearing plates shall be AASHTO M270 Grade 50W. All diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted. Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.

FILE NAME: W:\Projects\2010\100025 BurrFerson\1\add\Structural\Drawn\4453889-013-Structural Steel.dgn



USER NAME = nporris	DESIGNED - HLF	REVISED -
PLOT SCALE =	CHECKED - AEU	REVISED -
PLOT DATE = 10/18/2011	DRAWN - HLF	REVISED -
	CHECKED - AEU	REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

STRUCTURAL STEEL  
STRUCTURE NO. 045-3080

SHEET NO. 13 OF 20 SHEETS

T.R. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
0194	08-14117-00-BR	KANE	76	46
FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT			CONTRACT NO. 63645	