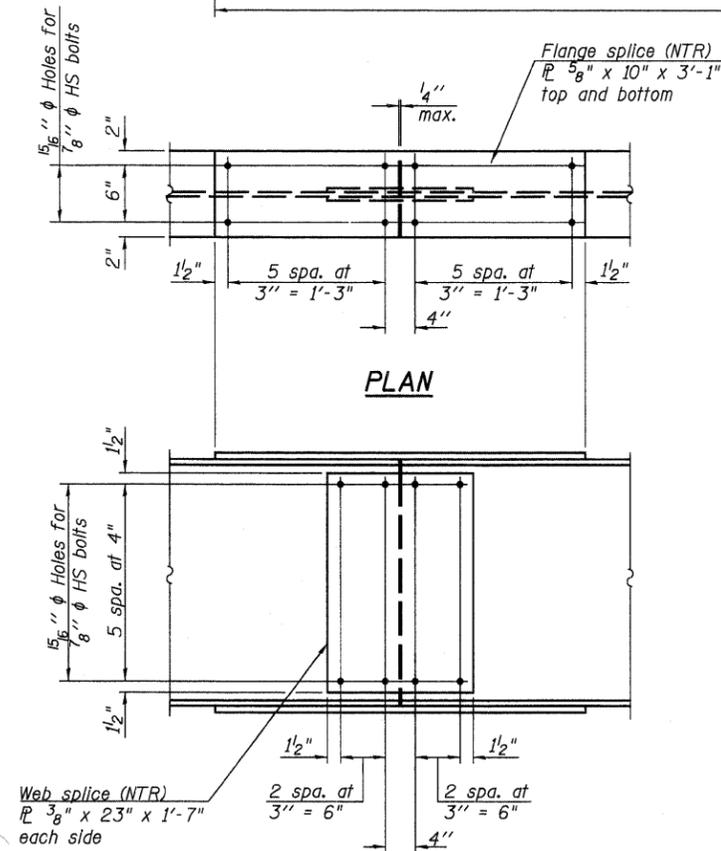
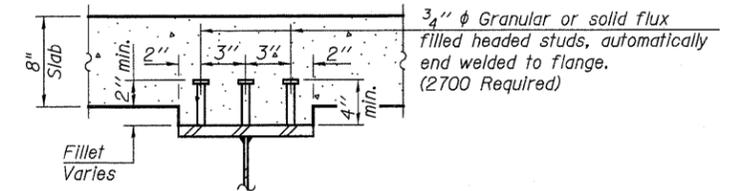
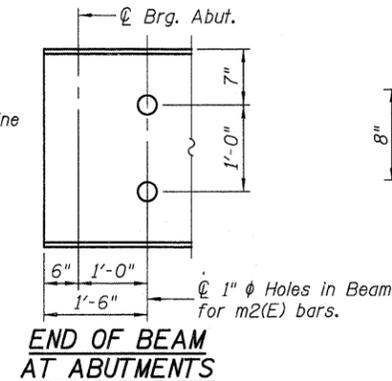
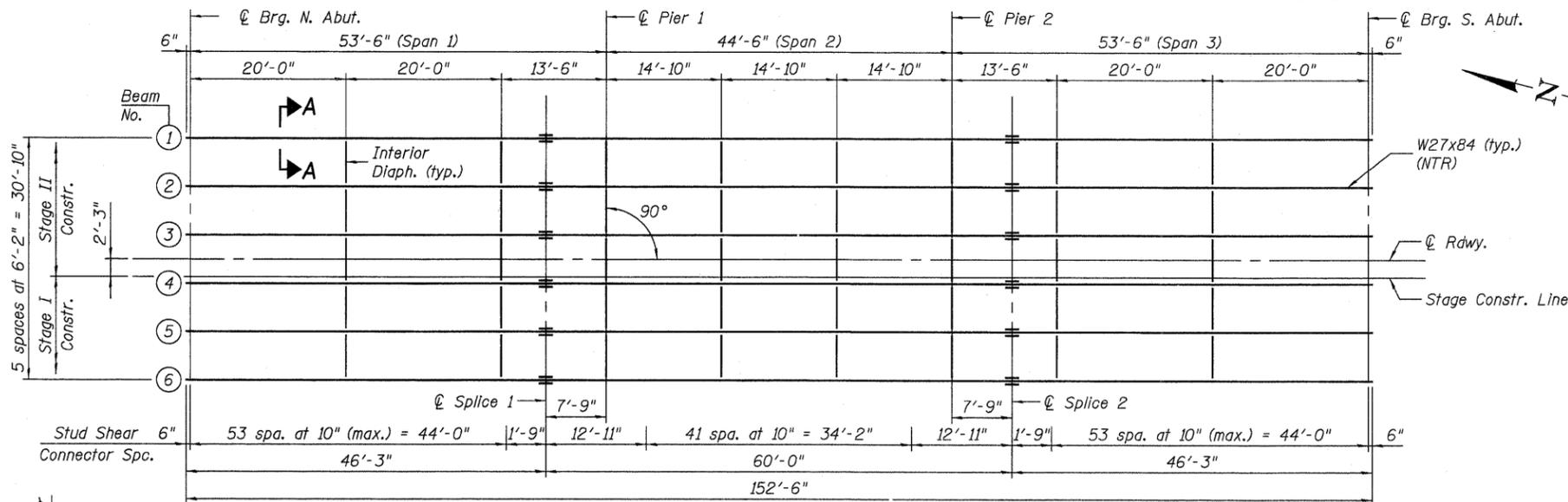


STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

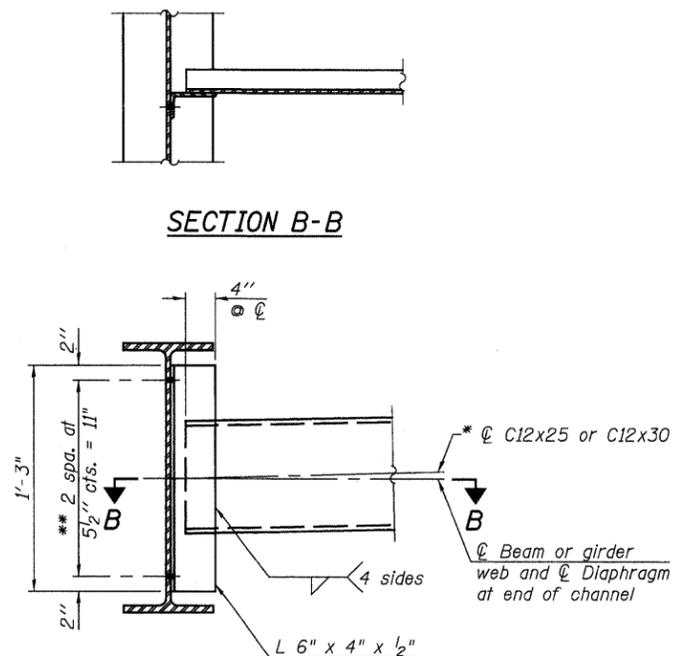
TOP OF BEAM ELEVATIONS*

| Location | Beam 1 | Beam 2 | Beam 3 | Beam 4 | Beam 5 | Beam 6 |
|-----------------|--------|--------|--------|--------|--------|--------|
| ℄ Brg. N. Abut. | 508.59 | 508.70 | 508.80 | 508.80 | 508.70 | 508.59 |
| ℄ Splice 1 | 509.43 | 509.54 | 509.63 | 509.63 | 509.54 | 509.43 |
| ℄ Pier 1 | 509.58 | 509.69 | 509.78 | 509.78 | 509.69 | 509.58 |
| ℄ Pier 2 | 510.43 | 510.54 | 510.63 | 510.63 | 510.54 | 510.43 |
| ℄ Splice 2 | 510.58 | 510.69 | 510.78 | 510.78 | 510.69 | 510.58 |
| ℄ Brg. S. Abut. | 511.50 | 511.61 | 511.70 | 511.70 | 511.61 | 511.50 |

* For Fabrication only. (Theoretical elevations before dead load deflection.)



SPLICE DETAIL
(12 Required)



Note:
Two hardened washers required for each set of oversized holes.

* Alternate channels are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section.
** 3/4" ϕ HS bolts, 15/16" ϕ holes

| | INTERIOR GIRDER MOMENT TABLE | | |
|--------------------------------|------------------------------|-------------|------------|
| | 0.4 Sp. 1 or 0.6 Sp. 3 | Pier 1 or 2 | 0.5 Span 2 |
| I_s | (in ⁴) 2850 | 2850 | 2850 |
| $I_o(n)$ | (in ⁴) 8510 | 2850 | 8510 |
| $I_o(3n)$ | (in ⁴) 6391 | 2850 | 6391 |
| S_s | (in ³) 213 | 213 | 213 |
| $S_o(n)$ | (in ³) 327 | 213 | 327 |
| $S_o(3n)$ | (in ³) 296 | 213 | 296 |
| Z | (in ³) --- | --- | --- |
| DC1 | (k/ft) 0.724 | 0.724 | 0.724 |
| MDC1 | (k) 176 | 182 | -2 |
| DC2 | (k/ft) 0.150 | 0.150 | 0.150 |
| MDC2 | (k) 41 | 28 | 10 |
| DW | (k/ft) 0.275 | 0.275 | 0.275 |
| MDW | (k) 74 | 51 | 17 |
| $M_k + IM$ | (k) 566 | 274 | 391 |
| M_u (Strength I) | (k) 1373 | 819 | 720 |
| $\phi_r M_n$, $\phi_r M_{nc}$ | (k) 1773 | 973 | 1773 |
| f_s DC1 | (ksi) 9.9 | 10.3 | -0.1 |
| f_s DC2 | (ksi) 1.7 | 1.6 | 0.4 |
| f_s DW | (ksi) 3.0 | 2.9 | 0.7 |
| f_s 1.3($k + IM$) | (ksi) 27.0 | 20.1 | 18.7 |
| f_s (Service II) | (ksi) 41.6 | 34.9 | 19.7 |
| ** f_s (Total)(Strength I) | (ksi) --- | --- | --- |
| V_r | (k) 23.4 | --- | 20.6 |

* Compact sections
** Non-Compact and slender sections

| | INTERIOR GIRDER REACTION TABLE | |
|-------------|--------------------------------|-------|
| | Abut. | Pier |
| R_{DC1} | (k) 16.0 | 38.8 |
| R_{DC2} | (k) 3.5 | 7.9 |
| R_{DW} | (k) 6.4 | 14.4 |
| $R_k + IM$ | (k) 63.0 | 85.5 |
| R_{Total} | (k) 88.9 | 146.6 |

Note:
All structural steel shall be AASHTO M270 Gr. 50W.
Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.
All cross frames or diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted. Individual cross frames or diaphragms at supports may be temporarily disconnected to install bearing anchor rods.

I_s , S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total-Strength I, and Service II) due to non-composite dead loads (in⁴ and in³).
 $I_o(n)$, $S_o(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total-Strength I, and Service II) due to short-term composite live loads (in⁴ and in³).
 $I_o(3n)$, $S_o(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in⁴ and in³).
Z: Plastic Section Modulus of the steel section in non-composite areas. Omit line in Moment Table if not used in design calculations (in³).
DC1: Un-factored non-composite dead load (kips/ft.).
MDC1: Un-factored moment due to non-composite dead load (kip-ft.).
DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).
MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).
DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).
MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).
 $M_k + IM$: Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).
 M_u (Strength I): Factored design moment (kip-ft.).
1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 $M_k + IM$
 $\phi_r M_n$: Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).
 $\phi_r M_{nc}$: Compact non-composite negative moment capacity computed according to Article A6.1.1 (kip-ft.).
 f_s (Service II): Sum of stresses as computed from the moments below (ksi).
 f_s (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi).
1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 $M_k + IM$
 V_r : Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

STRUCTURAL STEEL & FRAMING PLAN
ILLINOIS 267 OVER
TAYLOR CREEK
STRUCTURE NO. 031-0043

Johnson, Depp & Quisenberry
CONSULTING ENGINEERS
Springfield, Illinois

| | |
|---------------|--------------|
| DESIGNED: JDQ | DRAWN: SJS |
| CHECKED: DCD | CHECKED: DCD |

| | | | | | |
|---------------------|---------------|---------------------------|--------------------|--------------|-----------|
| SHEET 11 OF 19 | F.A.P. RTE. | SECTION | COUNTY | TOTAL SHEETS | SHEET NO. |
| | 10 | 410BR-1 | GREENE | 37 | 23 |
| | STA. 85+20.50 | | CONTRACT NO. 76B58 | | |
| FED. ROAD DIST. NO. | | ILLINOIS FED. AID PROJECT | | | |