



Original Report Date:	10-15-19	Proposed SN:	038-0226	Route:	FAP 332 (IL 1)
Revised Date:		Existing SN:	038-0020	Section:	4 BR
Geotechnical Engineer:	Terry McCleary of McCleary Engineering			County:	Iroquois
Structural Engineer:	Michael Haley of Lin Engineering, Ltd.			Contract:	66959

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): Proposed SN 038-0226 is a 3 span structure replacing SN 038-0020 on the same alignment that carries IL Route 1 over Pike Creek at sta. 273+22.00. There is no existing or proposed skew. The 15 inch reinforced concrete deck will be supported by integral abutments and pile bent piers encased with a solid wall. The out to out superstructure width is 34.83 ft. and the back to back abutment length is 91.0 ft. The factored loading is 540.0 kips for the abutments and 1250.0 kips for the piers. The vertical profile of the roadway at the bridge will be raised a maximum of about 1.9 ft. See the attached TS&L drawing for further information.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): Two borings were taken in October 2006 on the north and south sides of the side of the structure. Both borings reported a very similar profile. Below approximately 7 ft. of loose to medium loamy Sand fill, both borings show 2 to 3 ft. of loose to medium alluvial Sand. Below the Sand layer was approximately 55 ft. of stiff to very stiff Silty Clay, Clay, and Silty Clay Till. Seams and ribbons of Silt were present. Below Elevations 562.63 in Boring #1 on the south side and 565.04 in Boring #2 on the north side was hard gray brittle Silty Clay Loam Till and Sandy Clay Loam Till. Boring #2 reported Cobble and Boulder sized rocks in the till. Boring #2 reported auger refusal at 69 ft. due to Boulder obstruction. See attached 2006 borings and the Subsurface Profile Plot.

The existing 3 span structure, SN 038-0020, was built in 1955. Both abutments are supported on spread footings bearing on soil. Both piers are supported on concrete pile bents; the 1955 plans show 35 ft. long tapered concrete piles. The previous 3 span structure, built in 1921, was supported by spread footings. A general plan and elevation drawing provided by the 2006 BCR consultant shows a profile of the proposed structure, SN 038-0226, superimposed over the profiles of the previous 2 structures. It shows a conflict at Pier 2—the 1921 footing conflicts with the proposed pile bent, requiring either footing removal or coring through the spread footing. The current TS&L also shows near conflicts with both proposed piers and may require mitigation.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The rise in the profile at the abutments is expected to be a little less than 1.9 ft. and will consist of a thicker pavement structure plus some additional aggregate fill. The existing embankment is over 60 years old and show no signs of any settlement problems. There is expected to be little or no settlement;

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure.

Indicate if further testing, analysis or ground improvement/treatment is necessary: The proposed roadway maintains the same horizontal alignment. There will be no new cuts or fill slopes; the re-graded ditch height will vary from 6 ft. to 10 ft.. A worst case scenario was analyzed for the temporary 2:1 end slope: the factor of safety against a slope failure is 1.578. Some flattening (2:1 is recommended) of the temporary slope behind the abutment may be required because of the sandy soils. See attached slope stability analysis. No further testing is necessary.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design

scour elevations: No scour was accounted for at the abutments per IDOT policy. The Thalweg elevation at the structure is 613.8. The maximum design scour depth (4.81 ft.) was caused by the Q200 flood. A 25% reduction (1.2 ft.) in the scour depth for cohesive soils was allowed for soft to stiff cohesive soils (Qu between 0.5 to 1.5 tsf). An adjusted scour depth of 3.6 ft. was used to determine the design scour elevations in the table below.

Event/Limit	Design Scour Elevations (ft.)				Item
State	S. Abut	Pier 1	Pier 2	N. Abut.	113
Q100	-	610.2	610.2	-	8
Q200	-	610.2	610.2	-	
Design	622.93	610.2	610.2	623.03	
Check	622.93	610.2	610.2	623.03	

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable: This site has a soil site class of "C", the seismic performance zone, SPZ = 1. The SDS = 0.127 g and the SD1 = 0.076 g. Because the SD1 is less than 0.15 g, a liquification analysis is NOT required.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed: Data from two October 2016 borings, Boring #1: SE Quad: S Abut and Boring #2: NW Quad: N Abut were used to populate the data fields in the Estimated Pile Length spreadsheets. These 2 borings satisfactorily represent soil layers at the proposed substructure locations.

We recommend the use of metal shell piles with a wall thickness of 0.312 Inches or greater driven to bearing. Boring #1 shows a layer with high unconfined compressive strengths between the elevations of 595 and 586. Although the soils ranged from very stiff to hard, blow counts were less than 14. MS 14 w/ 0.312 walls or larger metal shell piling should be used; care should be taken to not damage them while driving. Metal shoes are recommended. Pile length spreadsheets for all the applicable sizes and wall thicknesses of metal shell piles are included in the appendix. The calculated settlement is negligible, therefore, down drag was not used in the analysis. Also, the site is in a SPZ 1, therefore, liquefaction was not considered. Two test piles are recommended, one should be driven at an abutment and the other at the pier farthest from the abutment.

Integral Abutments – The updated draft version of the Integral Abutment Spreadsheet was used for this analysis. We used the information from Boring 01 (N.E. Quad.) and Boring 02 (S.W. Quad.) to populate the fields in the integral abutment worksheet. The results show the abutment soils would allow the required movement for integral abutments and no remediation is required.

Assumptions used for the pile length analysis include:

- Bottom of North and South Abutment Elevation = 623.03 ft. and 622.93 ft. (respectively)
- The factored loading for the Abutments is 540 kips and 1250 kips for the pier.
- The bottom of the Pier footing is 610.20
- The pile cutoff elevation allows for a 2 ft. embedment into concrete for the abutments, 1 ft. for the pier.
- A 25% geotechnical reduction (1.2 ft.) in the scour depth of 4.8 ft. is allowed. Therefore the bottom elevation of the encasement can be raised to an elevation of 610.20 ft.
- No other geotechnical losses were accounted for in the analysis.

PILE LENGTH/RESISTANCE TABLES USING SOIL DATA for Abutments and Piers

South Abutment, Using Boring #1: SE Quad			South Pier, Using Boring #1: SE Quad		
Nominal Required Bearing (KIPS)	Factored Resistance Available (KIPS)	Estimated Pile Length (Ft.)	Nominal Required Bearing (KIPS)	Factored Resistance Available (KIPS)	Estimated Pile Length (Ft.)
MS 14 with 0.312" wall			MS 14 with 0.312" wall		
91	50	15	209	115	35
113	62	20	202	111	40
144	79	25	231	127	45
216	119	30	250	137	50
262	144	38	281	155	55
570	313	58	570	313	58
MS 16 with 0.312" wall			MS 16 with 0.312" wall		
107	59	15	176	97	30
131	72	20	249	137	35
167	92	25	233	128	40
256	141	30	267	147	45
328	181	35	288	158	50
654	360	58	654	360	58
MS 16 with 0.375" wall			MS 16 with 0.375" wall		
107	59	15	176	97	30
131	72	20	249	137	35
167	92	25	233	128	40
256	141	30	267	147	45
328	181	35	288	158	50
782	430	58	782	430	58
North Pier, Using Boring #2: NW Quad			North Abutment, Using Boring #2: NW Quad		
MS 14 with 0.312" wall			MS 14 with 0.312" wall		
166	91	38	80	44	15
172	95	40	98	54	21
204	112	45	127	70	26
229	126	50	202	111	33
257	141	55	230	126	39
570	313	58	570	313	58
MS 16 with 0.312" wall			MS 16 with 0.312" wall		
194	107	38	94	52	15
199	109	40	114	62	21
237	130	45	147	81	26
265	145	50	238	131	33
296	163	55	265	146	39
654	360	58	654	360	58
MS 16 with 0.375" wall			MS 16 with 0.375" wall		
194	107	38	94	52	15
199	109	40	114	62	21
237	130	45	147	81	26
265	145	50	238	131	33
296	163	55	265	146	39
782	430	60	782	430	58

Estimated Lateral Load Soil Parameters

Soil Type	Angle of Internal Friction (degrees)	Average Undrained Cohesion (ksf)	Static Soil Modulus k (pci)	Soil Strain Parameter E50	Total Unit Wt. (pcf)	Effective Unit Wt. (pcf)
Loose loamy sand	28	-	25	-	100	37.6
Very Stiff Silty Clay	-	2.1	1000	0.005	125	62.6
Stiff Clay and Silty Clay	-	1.5	500	0.007	120	57.6
Hard gray Silty Clay and Sandy Loam Till	-	4.3	2000	0.004	130	67.6

See attached Pile Length Estimating Spreadsheets, 2016 Boring logs, selected 1955 as-built plan sheets, loading documentation, and integral abutment spreadsheet.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: The E.W.S.E. is 618.04, the bottom of encasement is 610.2, therefore type 2 cofferdams are required. The soils are not permeable and seal coat should not be required.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: At this time we anticipate the structure to be built under staged construction conditions, therefore, Temporary Sheet Piling will be required at the stage line. From the data shown in the boring logs the author does not anticipate any problems driving the sheets to the design depth. The substructures shall be removed as per Section 501 if the 2016 IDOT Standard Specifications for Road and Bridge Construction.

Prepared by: McCleary Engineering
 Author: Terrence L. McCleary, P.E.
 Email: terry@mcclearyengineering.com
 Phone: (815) 780-8486



Project Location Map

FAP 332 (IL 1)

Section 4 BR

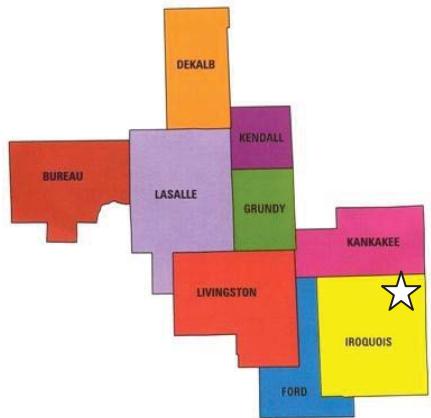
Iroquois County

Removal and replacement of S.N. 038-0020
carrying IL 1 over Pike Creek located 0.2
mi. north of U.S. 52

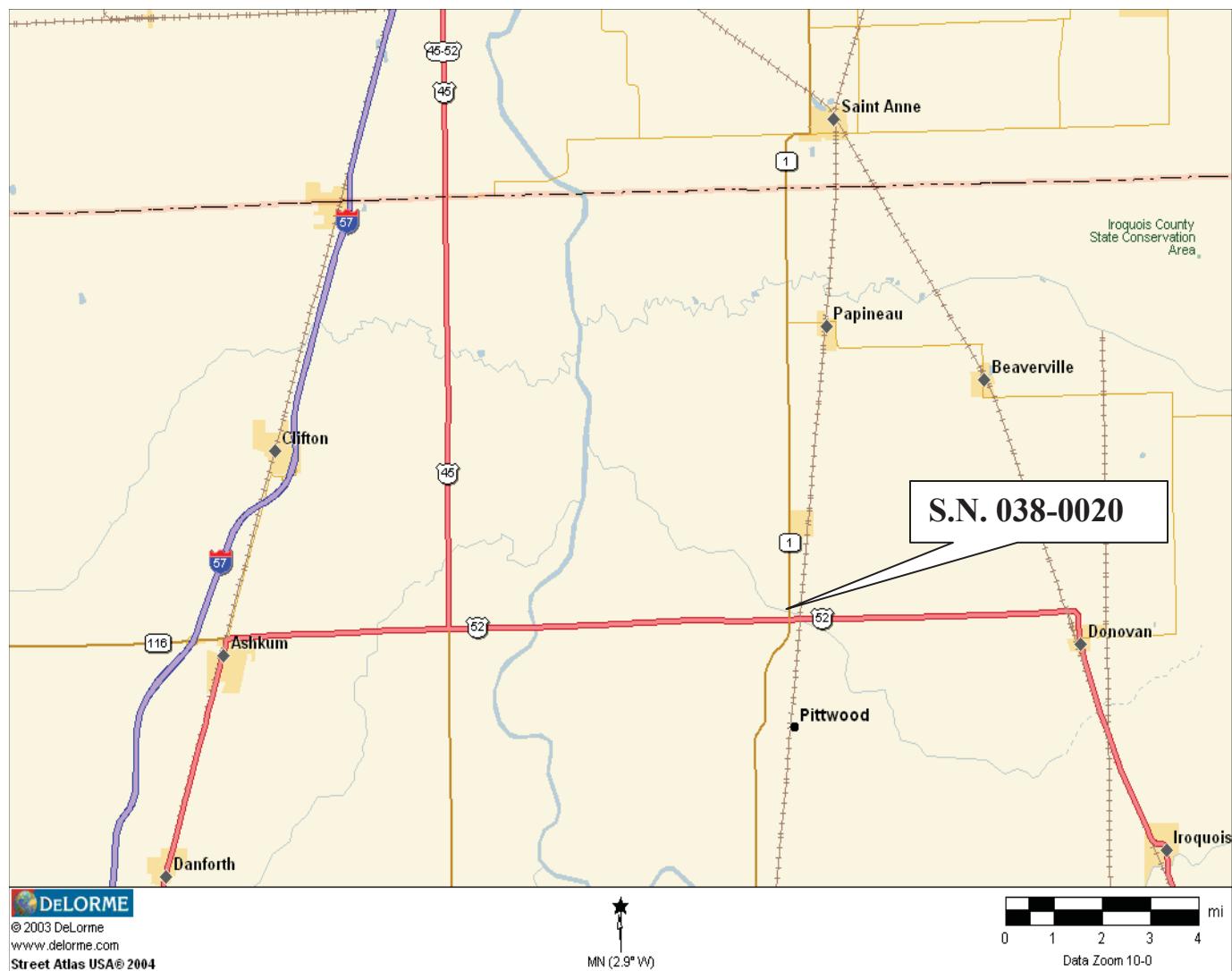
D3 No. 1134

P-93-044-00

Contract No. 66959



Project Area =



Benchmarks: BM #1 - Railroad Spike in Power Pole, Sta. 267+39.37
82.04 Lt., Elev. 626.56

BM #3 - Chiseled "□" in N.E. Wing Wall, Sta. 273+62.00,
39.00 Rt., Elev. 626.55

Existing Structure: S.N. 038-0020 originally constructed in 1918, replaced in 1954 as a cast-in-place three-span slab bridge with gravity abutments and solid wall encased pile bent piers supported on concrete piles. Back-to-Back abutment length is 81'-2" and out-to-out width of deck is 34'-4". The wearing surface was replaced in 1970 and a new thrie beam bridge rail was installed in 1984. The bridge is to be fully replaced.

Stage construction will be utilized to maintain one signalized lane of traffic.

Salvage: None

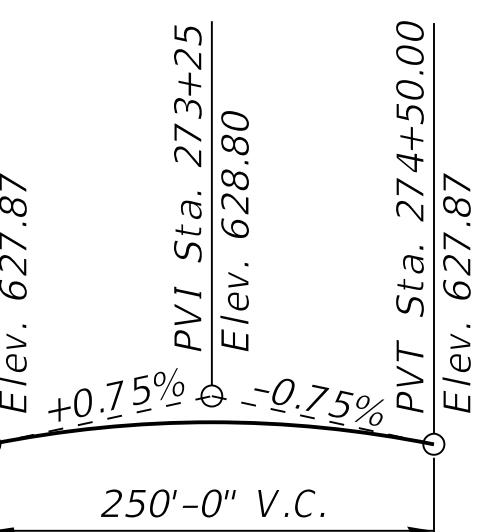
WATERWAY INFORMATION

Drainage Area = 21 sq. mi.			Low Grade Elev. 624.99 @ Sta. 281+50					
Flood	Freq. Yr.	Q C.F.S.	Opening Ft ²	Nat. Exist.	Head - Ft.	Headwater El.	Exist.	Prop.
	10	1120	360	469	623.6	0.2	0.0	623.7 623.6
Design	50	1750	436	547	624.6	0.3	0.1	624.9 624.7
Ex. Overtopping	65	1870	449	560	624.8	0.5	0.1	625.3 624.9
Base/Scour Des.	100	2030	457	588	625.1	0.5	0.2	625.6 625.4
Scour Check	200	2320	457	625	625.6	0.5	0.3	626.1 625.9
Max. Calc.	500	2710	457	646	625.8	0.5	0.3	626.4 626.1

10-Yr. Velocity through Existing Structure = 3.2 fps
10-Yr. Velocity through Proposed Structure = 2.4 fps

DESIGN SCOUR ELEVATION TABLE

Event / Limit State	Design Scour Elevations (ft.)			
	S. Abut.	Pier 1	Pier 2	N. Abut.
Q100	-	610.20	610.20	-
Q200	-	610.20	610.20	-
Design	622.93	610.20	610.20	623.03
Check	622.93	610.20	610.20	623.03



PROFILE GRADE

(Along Q Roadway)

SEISMIC DATA

Seismic Performance Zone (SPZ) = 1

Design Spectral Acceleration at 1.0 sec. (SD1) = 0.076 g

Design Spectral Acceleration at 0.2 sec. (SDS) = 0.127 g

Soil Site Class = C

DESIGN SPECIFICATIONS

2017 AASHTO LRFD Bridge Design
Specifications, 8th Edition

DESIGN STRESSES

FIELD UNITS

f'c = 3,500 psi

f'c = 4,000 psi (Superstructure)

fy = 60,000 psi (Reinforcement)

LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

HIGHWAY CLASSIFICATION

F.A.P. Rte. 332 - IL Rte. 1

Functional Class: Other Principal Arterial

ADT: 2,450 (2017); 2,295 (2032)

ADTT: 270 (2017); 253 (2032)

DHV: 302

Design Speed: 55 m.p.h.

Posted Speed: 55 m.p.h.

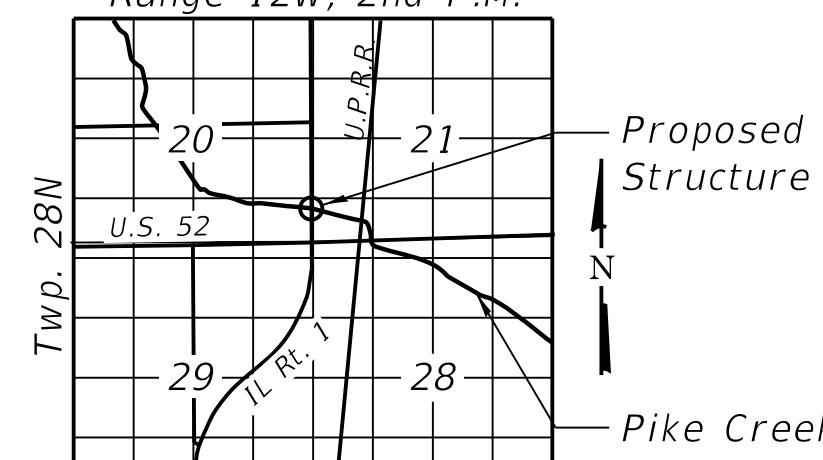
Two-Way Traffic

LEGEND

Channel Excavation

Soil Boring

Range 12W, 2nd P.M.



LOCATION SKETCH

GENERAL PLAN

ILLINOIS ROUTE 1 OVER PIKE CREEK

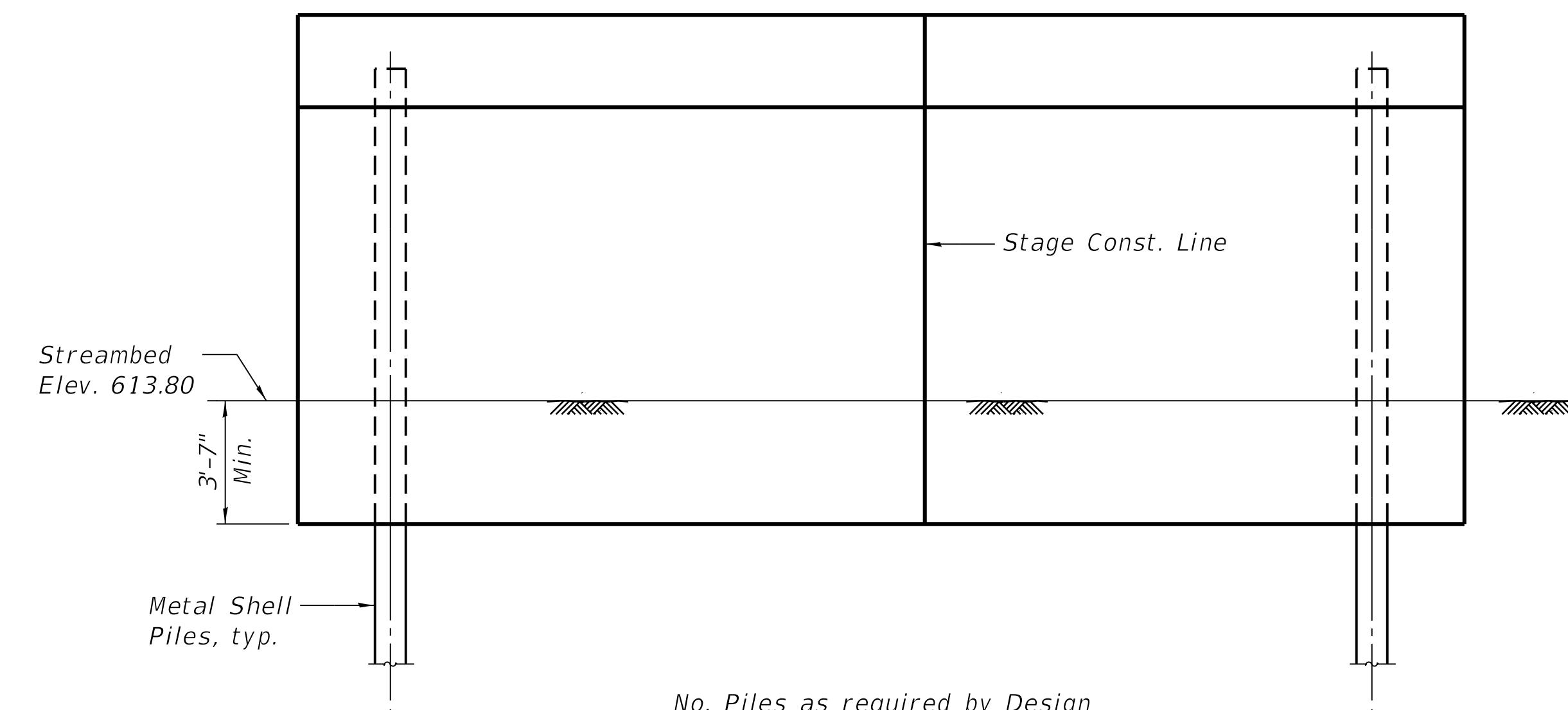
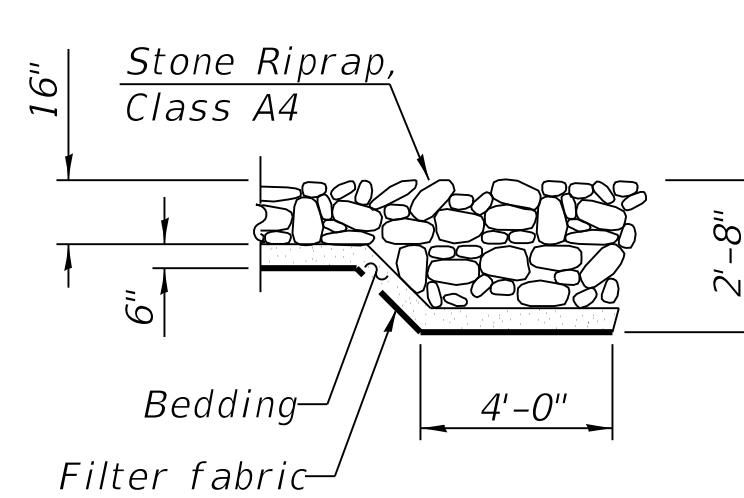
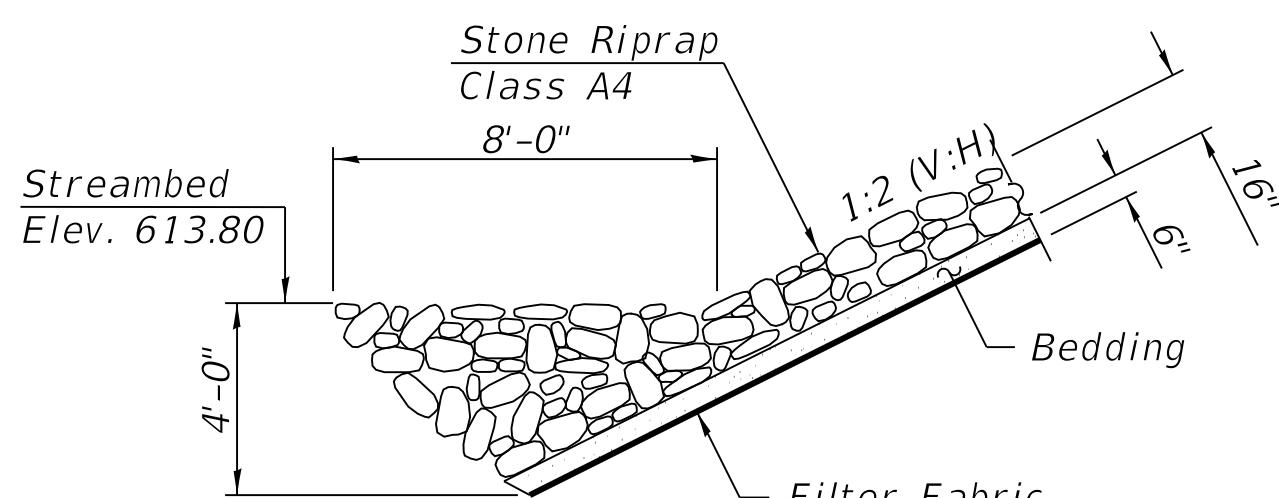
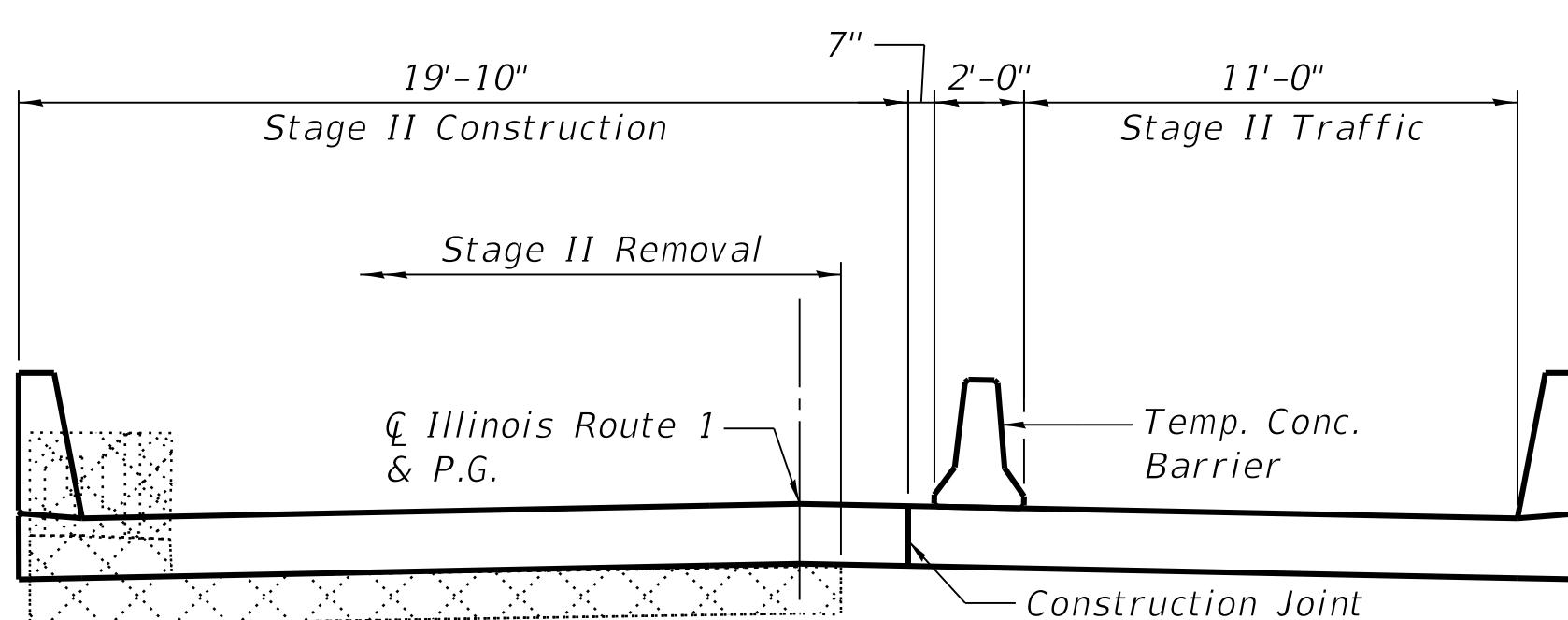
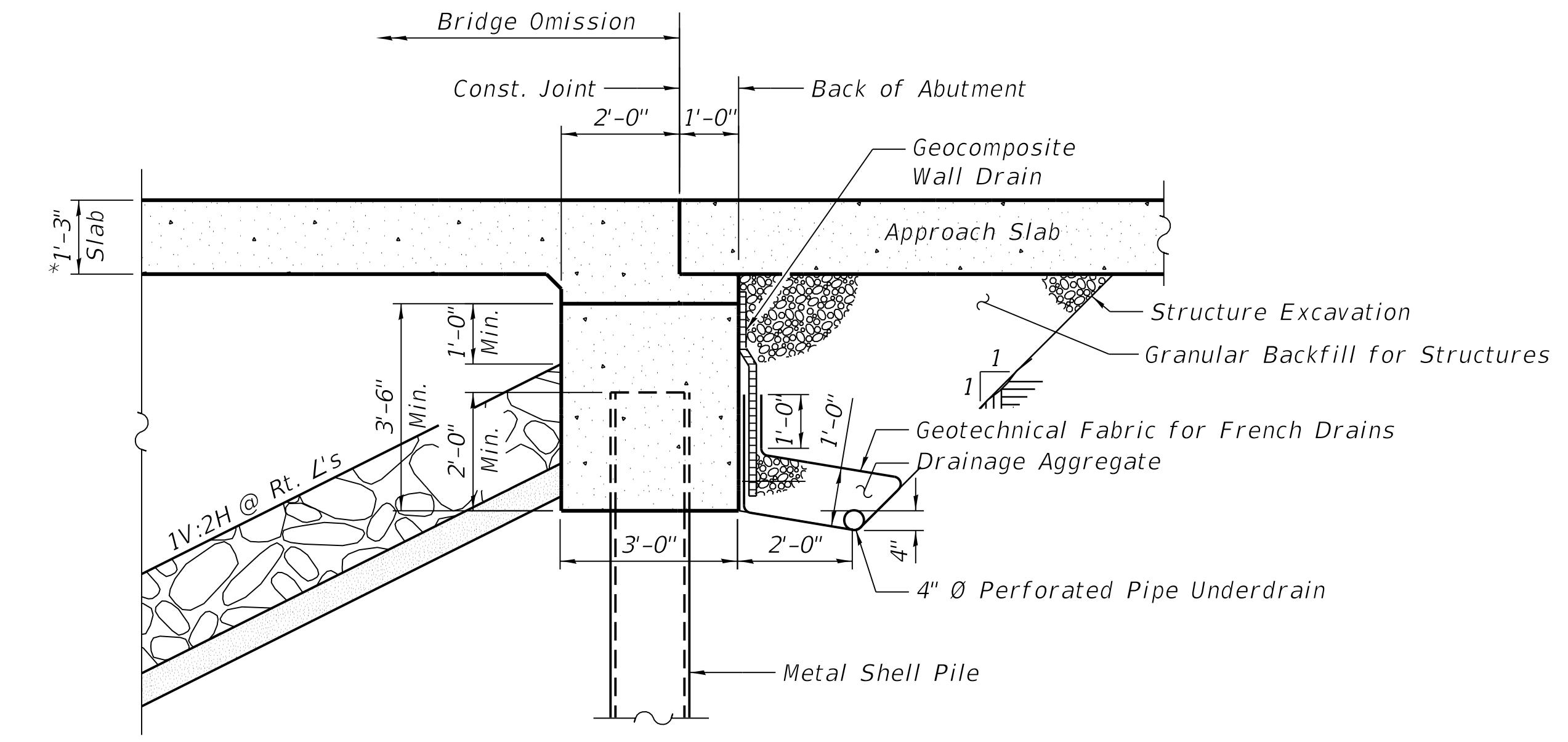
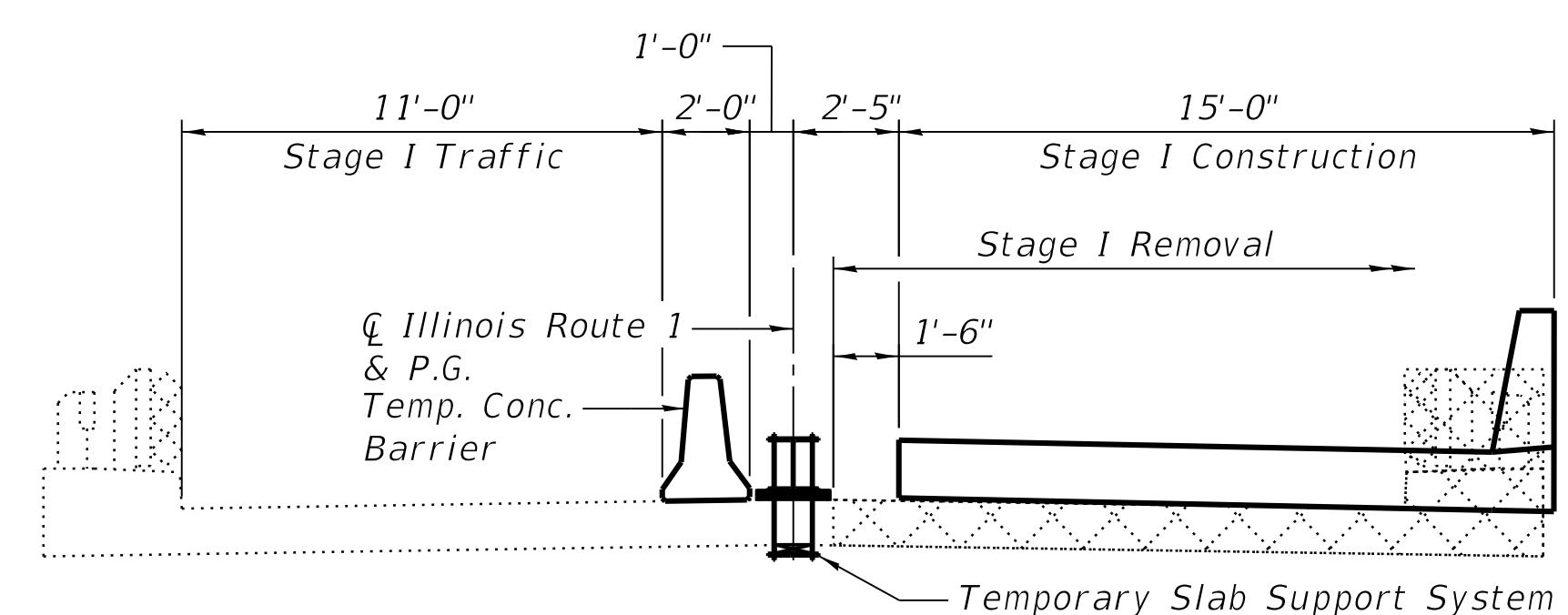
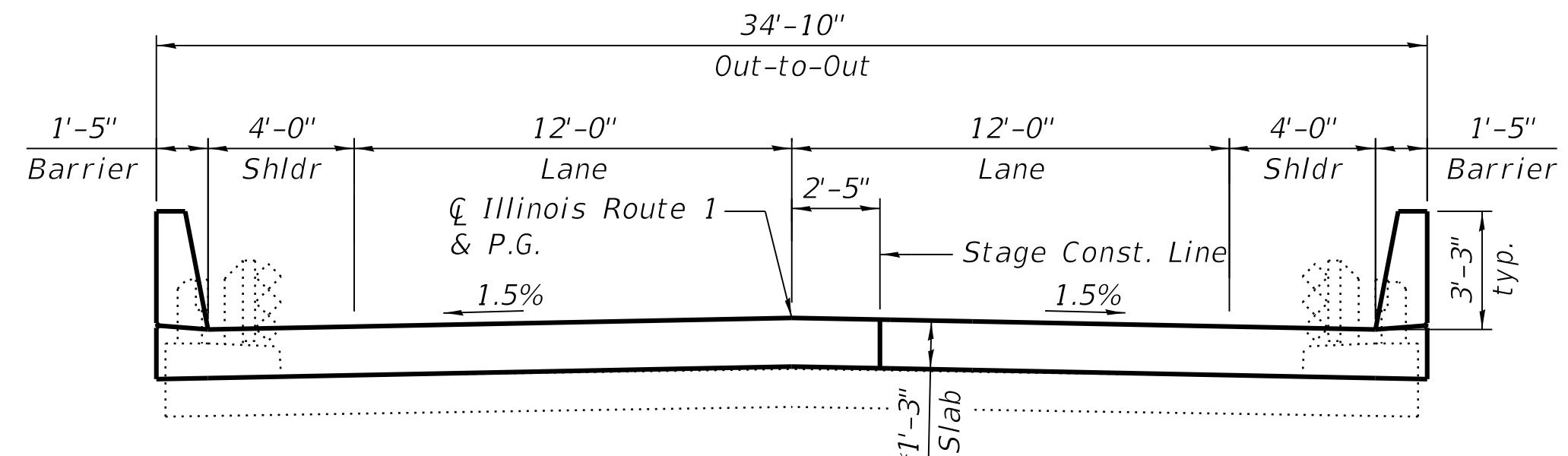
F.A.P. RTE. 332 - SEC. 4-BR

IROQUOIS COUNTY

STA. 273+22.00

STRUCTURE NO. 038-0226

NOTE:
1. See Sheet 2 for Sections A-A and B-B



DETAILS
ILLINOIS ROUTE 1 OVER PIKE CREEK
F.A.P. RTE. 332 - SEC. 4-BR
IROQUOIS COUNTY
STA. 273+22.00
STRUCTURE NO. 038-0226



STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS NO.
332	4-BR	IROQUOIS	2 2

CONTRACT NO. 66959
ILLINOIS FED. AID PROJECT



ROUTE SBI-1 (IL 1) **DESCRIPTION** IL 1 over Pike Creek **LOGGED BY** Larry Myers

SECTION 4-BR LOCATION SE 1/4, SEC. 20, TWP. 28N, RNG. 12W, 2nd PM

COUNTY Iroquois **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

STRUCT. NO. 038-0020
Station 273+22

D E P T H	B L O W S	U C S W Qu	M O I S T	Surface Water Elev. _____ ft Stream Bed Elev. _____ ft Groundwater Elev.: First Encounter _____ ft Upon Completion _____ ft ▽ After _____ Hrs. _____ ft	D E P T H	B L O W S	U C S W Qu	M O I S T
(ft)	(/6")	(tsf)	(%)		(ft)	(/6")	(tsf)	(%)

BORING NO. #1: SE Quad: S Abut
Station 272+46
Offset 10.00ft Right
Ground Surface Elev. 628.63

Augered, bituminous pavement, white CA06						
626.63						
Loose, brown and black, very loamy, fine to coarse, Sand - fill (borderline loam)		5				
		5		12.4		
		5				
		-5	2			
		2		19.1		
		3				
621.63						
Loose to medium, brown gray, fine, Sand, Silt, Clay layers (alluvial)		2				
		2	1.0	23.8		
		3	P			
619.63						
Very stiff, gray, Silty Clay		-10	2			
		3	2.1	23.0		
		5	B			
		3				
		4	2.3	22.9		
		5	B			
		-15	3			
		3	2.1	23.3		
		5	B			
612.13						
Stiff, gray, Clay with layers of gray, Silty Clay with thin Silt seams @ 30.5' (somewhat varved)		1				
		3	1.7	26.2		
		5	S			
-20						
Stiff, gray, Clay with layers of gray, Silty Clay with thin Silt seams @ 30.5' (somewhat varved)		1				
597.13						
Very stiff, dark gray, Silty Clay, Clay and Silt pockets- some small scale varved, Clay 1-2" thick						
594.63						
Hard, gray, Silty Clay, Clay, Silt seams - varved, Clay layers						
-35						
		4				
		6	4.7	23.4		
		8	S			
		5				
		6	4.0	24.7		
		7	S			
589.63						
Stiff, gray, Clay with minor, Silt ribbons						
-40						
		4				

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer). The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206).



Illinois Department of Transportation

**Division of Highways
District #3, Ottawa**

SOIL BORING LOG

Page 2 of 3

Date 10/19/06

ROUTE SBI-1 (IL 1) DESCRIPTION IL 1 over Pike Creek LOGGED BY Larry Myers

SECTION _____ **4-BR** _____ **LOCATION** **SE 1/4, SEC. 20, TWP. 28N, RNG. 12W, 2nd PM**

COUNTY Iroquois **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

STRUCT. NO. 038-0020
Station 273+22

BORING NO. #1: SE Quad: S Abut
Station 272+46
Offset 10.00ft Right
Ground Surface Elev. 628.63

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer). The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206).

BBS, from 137 (Rev. 8-99)



**Illinois Department
of Transportation**

Division of Highways
District #3, Ottawa

SOIL BORING LOG

Page 3 of 3

Date 10/19/06

ROUTE SBI-1 (IL 1) DESCRIPTION IL 1 over Pike Creek LOGGED BY Larry Myers

SECTION 4-BR LOCATION SE 1/4, SEC. 20, TWP. 28N, RNG. 12W, 2nd PM

COUNTY Iroquois DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 038-0020
Station 273+22

BORING NO. #1: SE Quad: S Abut
Station 272+46
Offset 10.00ft Right
Ground Surface Elev. 628.63 ft

D	B	U	M
E	L	C	O
P	O	S	I
T	W	Qu	S
H	S		T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. 618.31 ft
Stream Bed Elev. _____ ft

Groundwater Elev.:
First Encounter _____ ft
Upon Completion 604.6 ft ▽
After _____ Hrs. _____ ft

Hard, gray, Sandy Clay Loam Till
(brittle) (continued)
547.63

90 >4.5 7.1
100/3" P

End of Boring

-85
-90
-95
-100

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, from 137 (Rev. 8-99)



ROUTE SBI-1 (IL 1) **DESCRIPTION** IL 1 over Pike Creek **LOGGED BY** Larry Myers

SECTION 4-BR **LOCATION** SE 1/4, SEC. 20, TWP. 28N, RNG. 12W, 2nd PM

COUNTY Iroquois **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

STRUCT. NO. 038-0020
Station 273+22

BORING NO. #2: NW Quad: N Abut
Station 273+97
Offset 11.00ft Left
Ground Surface Elev. 628.54

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer). The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206).



ROUTE SBI-1 (IL 1) **DESCRIPTION** IL 1 over Pike Creek **LOGGED BY** Larry Myers

SECTION 4-BR LOCATION SE 1/4, SEC. 20, TWP. 28N, RNG. 12W, 2nd PM

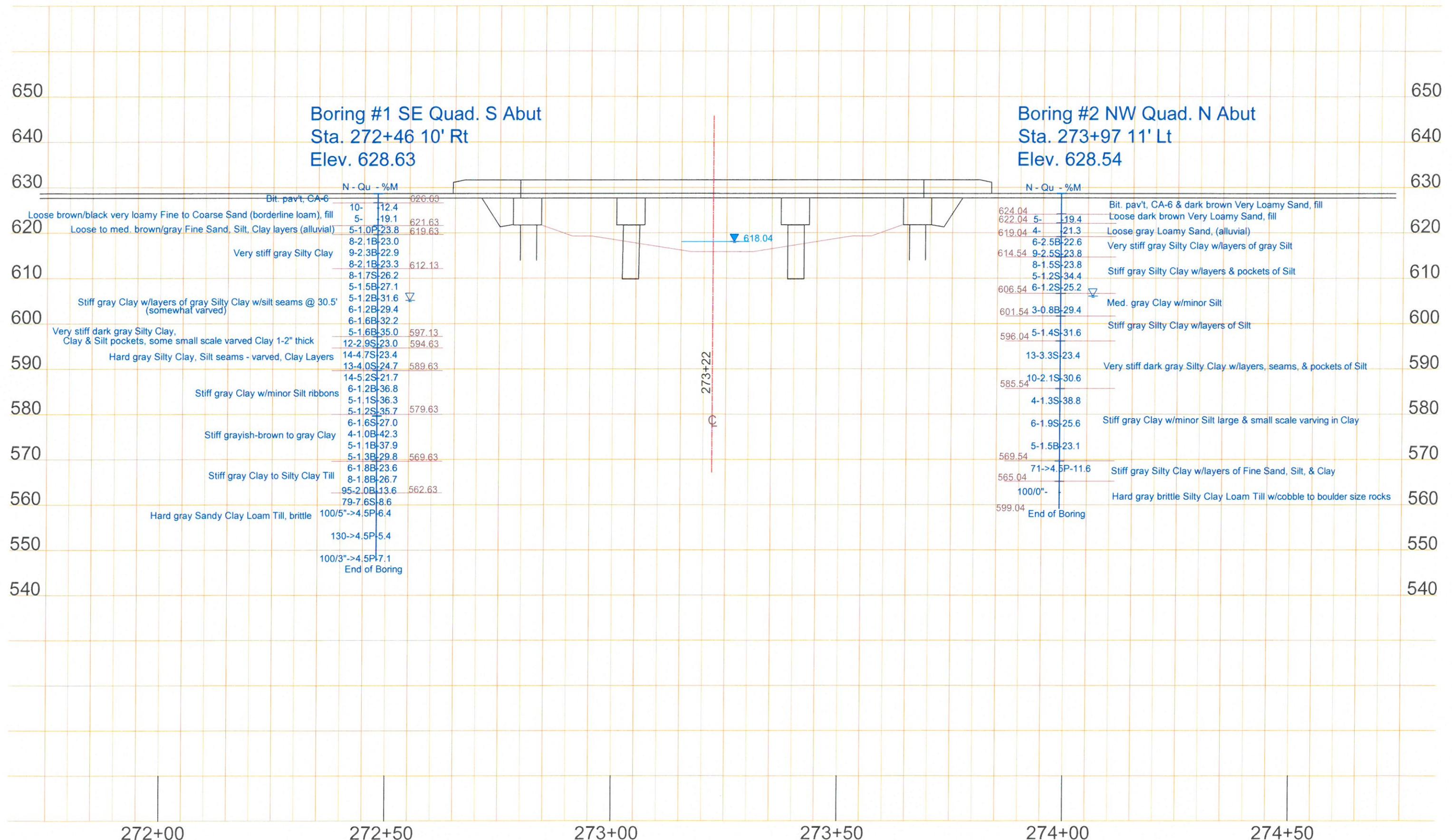
COUNTY Iroquois **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

STRUCT. NO. 038-0020
Station 273+22

BORING NO. #2: NW Quad: N Abut
Station 273+97
Offset 11.00ft Left
Ground Surface Elev. 628.54

STRUCT. NO.	038-0020				D E P T H	B L O W S	U C S	M O I S T	Surface Water Elev.	618.31 ft		D E P T H	B L O W S	U C S	M O I S T		
Station	273+22								Stream Bed Elev.								
BORING NO.	#2: NW Quad: N Abut								Groundwater Elev.:								
Station	273+97								First Encounter	ft							
Offset	11.00ft Left								Upon Completion	605.5 ft							
Ground Surface Elev.	628.54 ft				(ft)	(/6")	(tsf)	(%)	After Hrs.			(ft)	(/6")	(tsf)	(%)		
Very stiff, dark gray, Silty Clay with layers, seams, and pockets of Silt (continued)					4	2.1	30.6		Stiff, gray, Silty Clay with layers of fine, Sand, Silt, and Clay (continued)				2	1.5	23.1		
					6	S							3	B			
Stiff, gray, Clay with minor, Silt-large and small scale varving in Clay									565.04								
									Hard, gray, brittle, Silty Clay Loam Till , with Cobble to Boulder size rocks				-65	7			
									64.5'- Washed Interval				-58	13	>4.5		
									Auger refusal @ 69': Boulder obstruction						11.6		
									559.04								
									End of Boring				-70	100/0"			
Stiff, gray, Silty Clay with layers of fine, Sand, Silt, and Clay																	
569.54																	

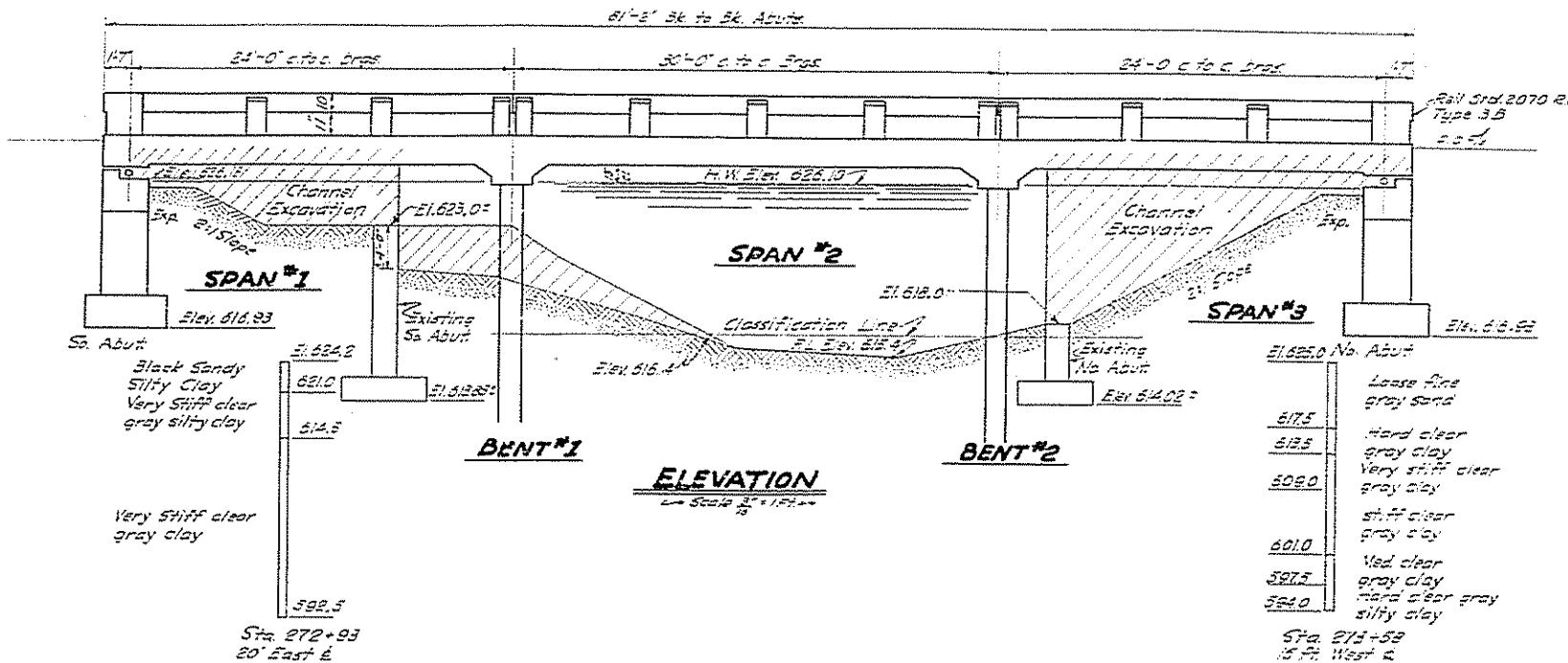
The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



*E.M. Top N.W. Wing Existing Bridge Elek 628.02
Existing Structure: 40' R.C. Thru Girder and portions of R.C.
closed Abutments to be removed by Bridge Contractor.*

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BUILDINGS
DIVISION OF HIGHWAYS

NAME	GRADE	CLASS	SEX	AGE	TELEGRAM
ROBERT HARVEY	32	12	M	32	R-32-12-7
					R-32-12-7



GENERAL NOTES

Glass X Concrete shall be used throughout except as noted
Horizontal Concrete shall be less than 20% of **Perimeter**
The concrete floor slab shall be finished in accordance
with the provisions of Article 20 of the **SAC Spec.**
All bearing plates, rollers, rockers, anchor bolts, etc.
and plates shall be included for payment as **Structural SCA**
and shall be set in accordance with Art 5, 14 Oct 2000^{ed}
of structural steel included in **bill of material**.

Structural Steel shall receive one shop coat of red lead paint and two field coats of aluminum paint. Paint shall be furnished and applied by Contractor.

All reinforcement bars shall conform to A.S.T.M. designation A-305 and the bar number is the number of inches in the nominal diameter.

The boring data are given on the plots only as a guide to bidders in estimating the types of soil which may be encountered.

One test pile shall be driven in a permanent site location before casting remainder of piles.

Consequently, the author of *Deinde* was probably the same person as the author of *Deinde*.

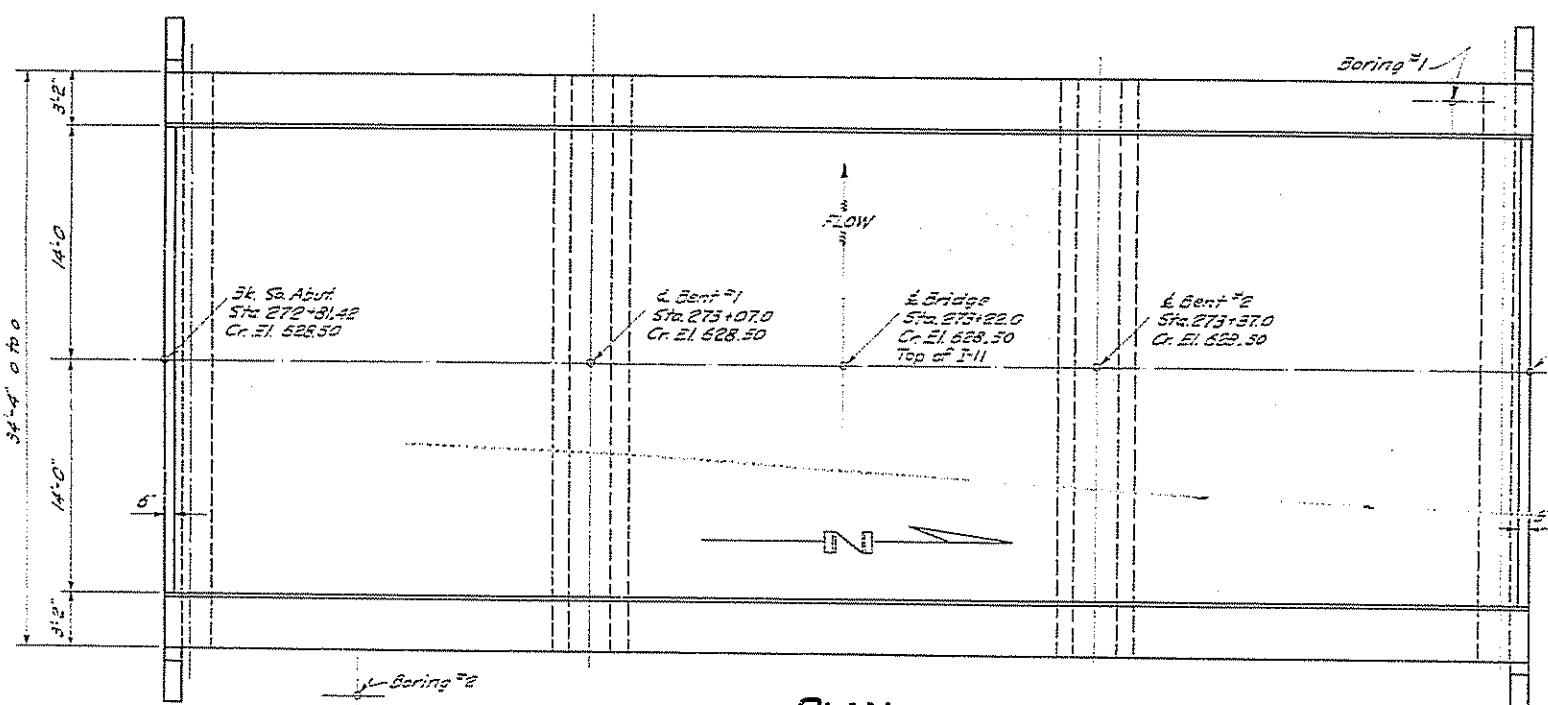
TOTAL BILL OF MATERIAL

Item	Estimate	Actual	Total
Class X Concrete	2000	333	26.6
General Concrete	2000	20	2.0
Reinforcement Bars	100	EC100	34100
Structural Steel	100	6650	6650
Precast Concrete Pile(100 ft)	1000	335	335
Name Plates	50	1	1
Bit. Concrete Surface Course (100 ft)	1000	210	21.0
Bit. Material - Prime Cost	500	25	2.5
Channel excavator	1000	-	335
Removal of existing Structure	50	-	1
Test Piles	50	-	1
Class A Excavation for Structure	1000	-	335

**STATION 279+22
BUILT 195 BY
STATE OF ILLINOIS
J.B.I.R.T. 1 SEC 4-BR
F.A. PROJECT F-2(2)
LOADING H2O-S16**

LETTERING FOR NAME PLATE

Page 53 of 263



WATERWAY INFORMATION

Drainage Area	5,200 Acres
Character	Level, Cultivated
Present Opening	313°
Regd. Opening (C. falcons = 0.2)	313°
Proposed Opening	437°

DESIGNED Harry P. Graham
CHECKED Murphy Howard
DRAWN Singer H. Ford
PRACTICED Murphy Howard

STRESSES

<i>F3</i>	=	15,000 $\frac{7}{15}$ " Struct.
<i>F5</i>	=	20,000 $\frac{7}{15}$ " resin
<i>F7</i>	=	1,400 $\frac{7}{15}$ " superstr.
<i>F8</i>	=	800 $\frac{7}{15}$ " substr.
<i>n</i>	=	10

Loadding H2O S-15-44

PROJECT F-2(23)

GENERAL PLAN ELEVATION

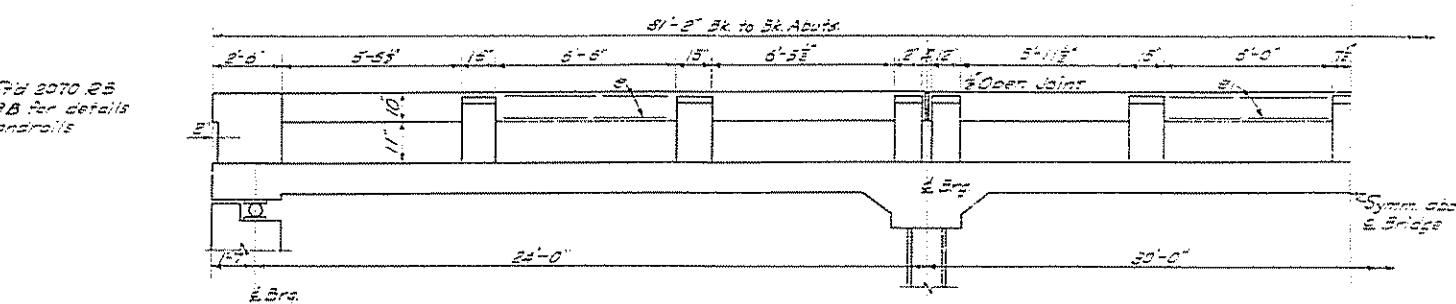
S.B.I.R.T.1 SECTION 4-BR

IROQUOIS COUNTY

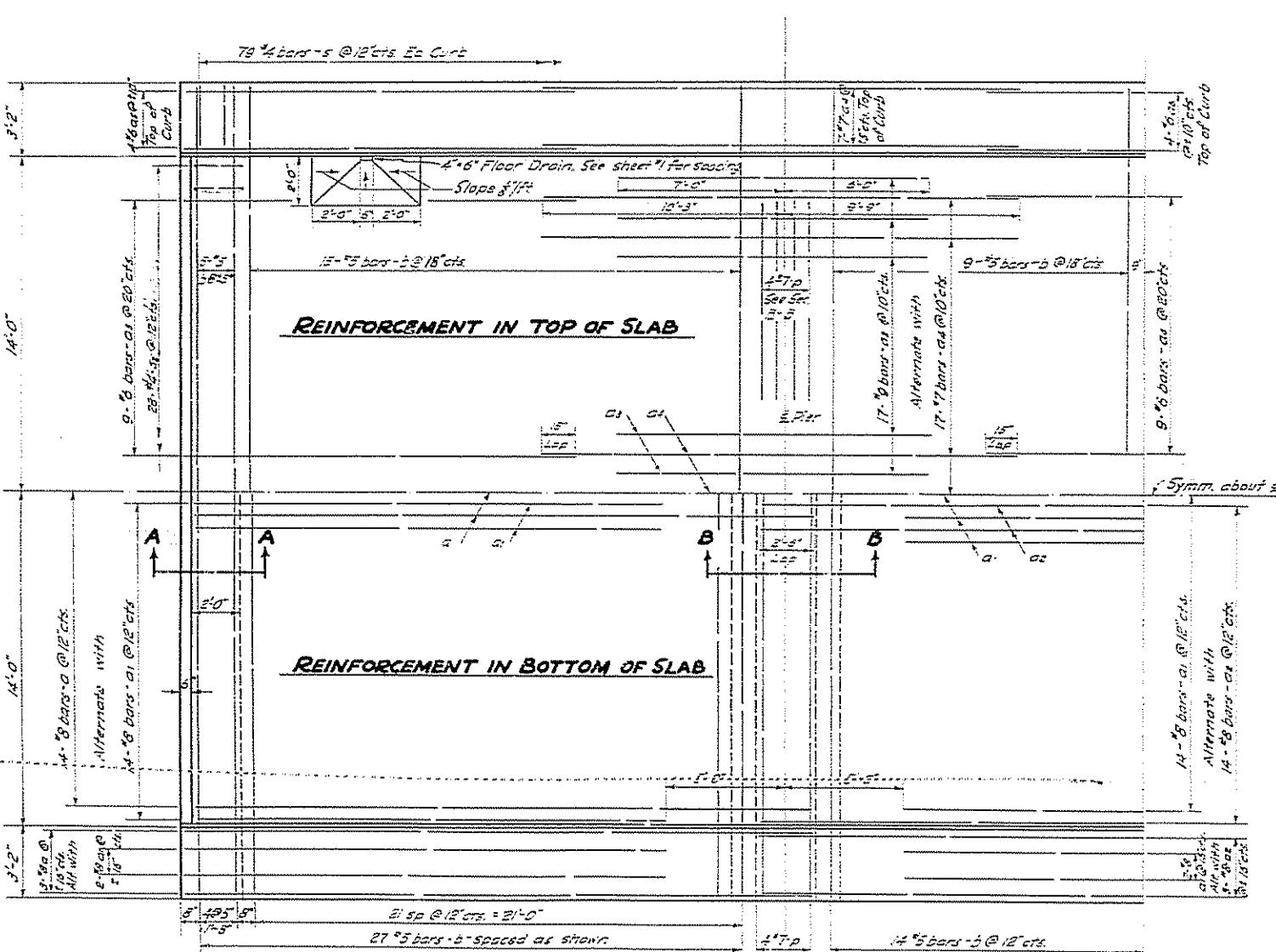
STA. 273+22

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BUILDINGS
DIVISION OF HIGHWAYS

See SPB 2070-25
Type 3B for details
of Handrolls



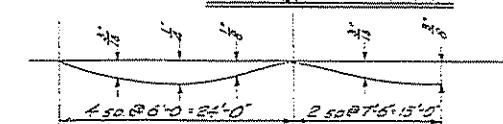
HALF ELEVATION



REINFORCEMENT IN TOP OF SLAB

REINFORCEMENT IN BOTTOM OF SLAB

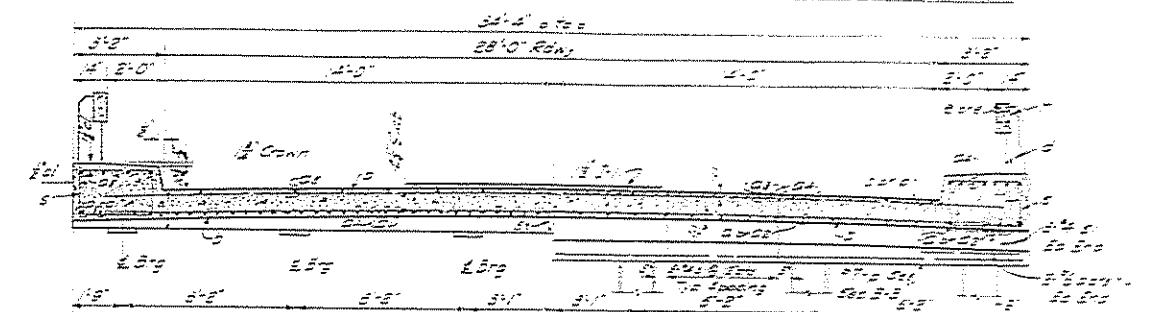
HALF PLAN



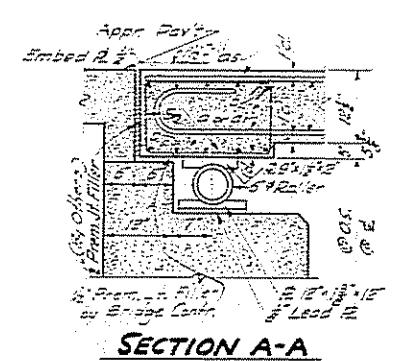
DEAD LOAD DEFLECTION DIAGRAM
In addition to D.L. deflection the contractor shall make
allowance for shrinkage & settlement of falsework.

DESIGNED	Henry P. Parker
CHECKED	Burkhardt Ormond
APPROVED	Burkhardt Ormond

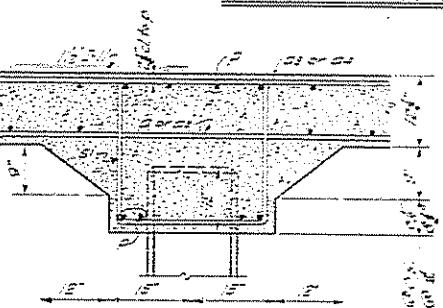
Type 7	Rev. 7-25-57
EXAMINED	J. E. H. 7-25-57
PASSED	J. E. H. 7-25-57
APPROVED	J. M. Parker



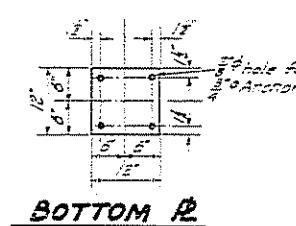
CROSS SECTION



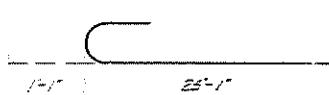
SECTION A-A



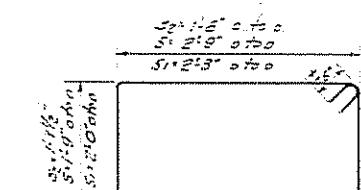
SECTION B-B



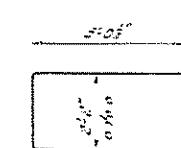
BOTTOM PLATE



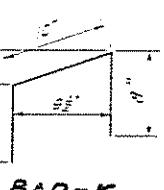
BAR-C



BARS-S & S1



BAR-U



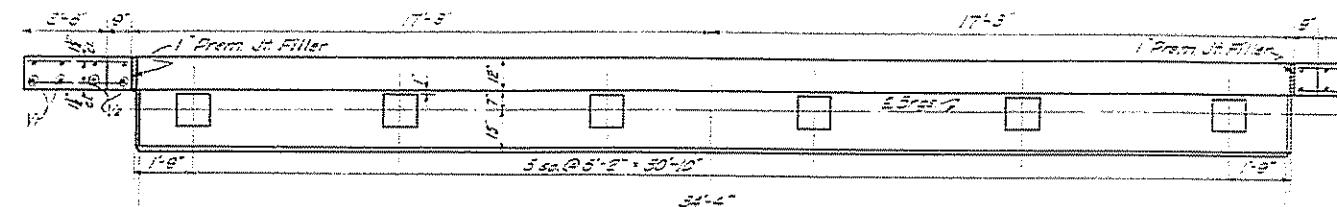
BAR-D

BILL OF MATERIAL-SUPER			
ITEM	DESCRIPTION	QUANTITY	SIZE
E	#2 1/2" E.P.C.	1	1/2"
G	#2 1/2" E.P.C.	1	1/2"
H	#2 1/2" E.P.C.	1	1/2"
I	#2 1/2" E.P.C.	1	1/2"
J	#2 1/2" E.P.C.	1	1/2"
K	#2 1/2" E.P.C.	1	1/2"
L	#2 1/2" E.P.C.	1	1/2"
M	#2 1/2" E.P.C.	1	1/2"
N	#2 1/2" E.P.C.	1	1/2"
O	#2 1/2" E.P.C.	1	1/2"
P	#2 1/2" E.P.C.	1	1/2"
Q	#2 1/2" E.P.C.	1	1/2"
R	#2 1/2" E.P.C.	1	1/2"
S	#2 1/2" E.P.C.	1	1/2"
T	#2 1/2" E.P.C.	1	1/2"
U	#2 1/2" E.P.C.	1	1/2"
V	#2 1/2" E.P.C.	1	1/2"
W	#2 1/2" E.P.C.	1	1/2"
X	#2 1/2" E.P.C.	1	1/2"
Y	#2 1/2" E.P.C.	1	1/2"
Z	#2 1/2" E.P.C.	1	1/2"
A	Class X Concrete	1	1/2"
B	Standard Concrete	1	1/2"
C	Reinforcement Bars	1	1/2"
D	Structural Steel	1	1/2"
E	St. Zinc Exterior Paint	1	1/2"
F	St. Material (Paint & Coats)	1	1/2"

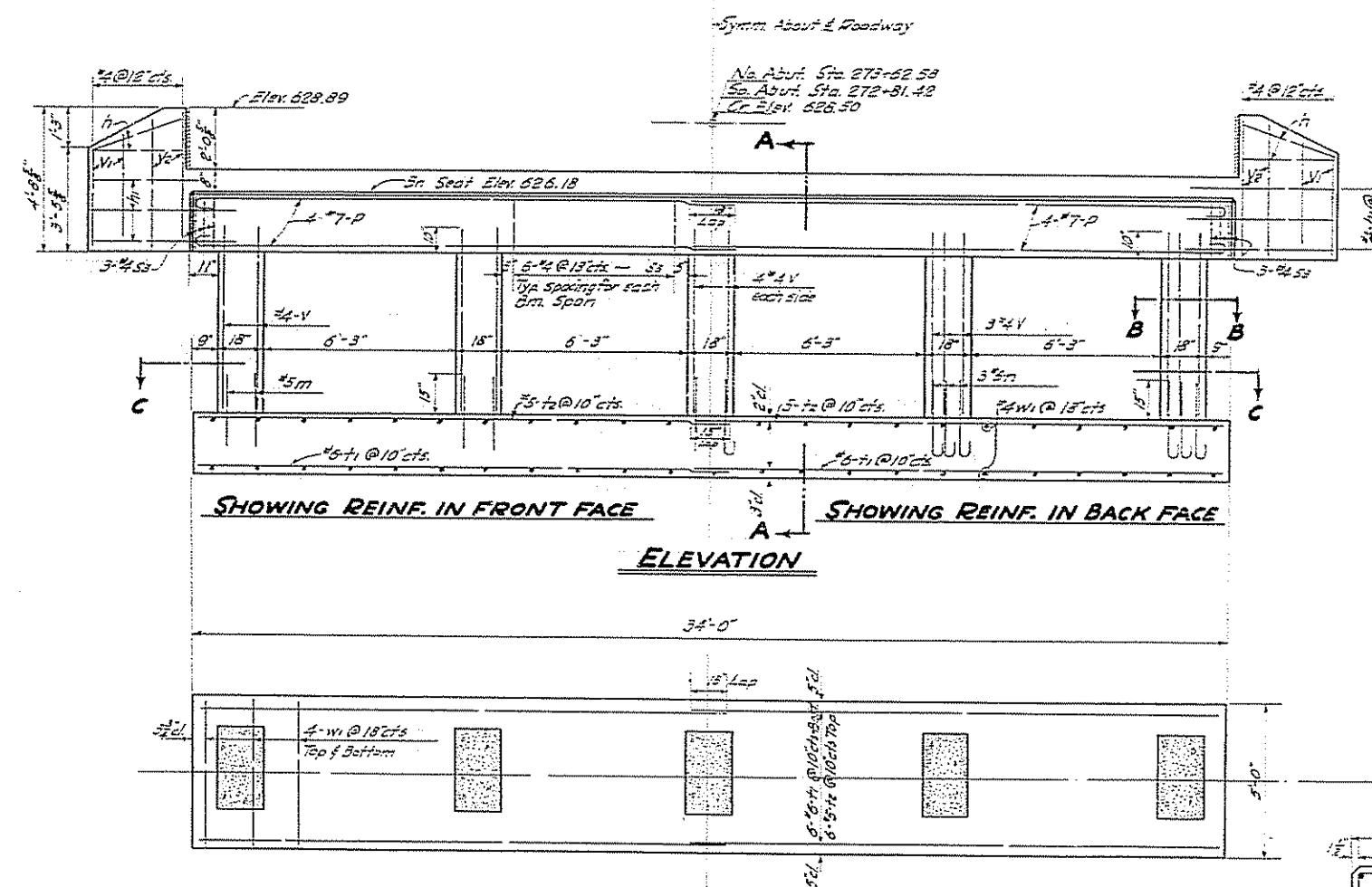
SUPERSTRUCTURE
S.B.I.R.T.1 SECTION 4 B-2
IROQUOIS COUNTY
STA. 273 +22

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BUILDINGS
DIVISION OF HIGHWAYS

Project No.	Section No.	Date	Check No.
SP-100	SECTION A-A	2-1-50	2-1-50



ABUT. PLAN

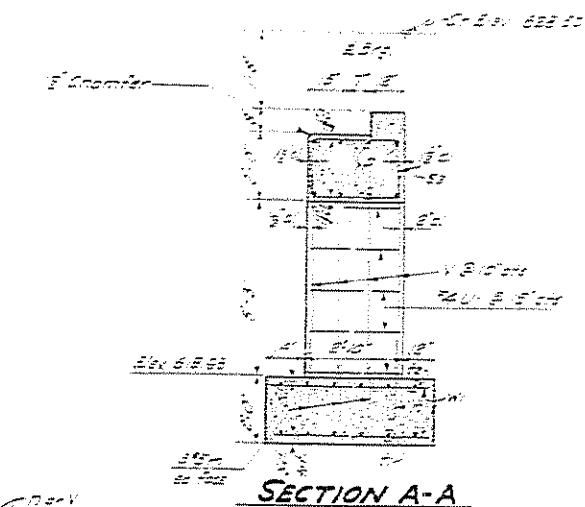


ELEVATION

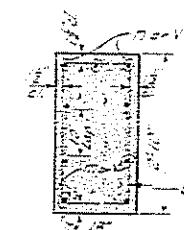
DESIGNED	W. E. Johnson
CHECKED	H. P. Carlson
REVIEWED	S. B. T. R. I. I.
APPROVED	J. M. Parker

DESIGNED	W. E. Johnson
CHECKED	H. P. Carlson
REVIEWED	S. B. T. R. I. I.
APPROVED	J. M. Parker

SECTION C-C



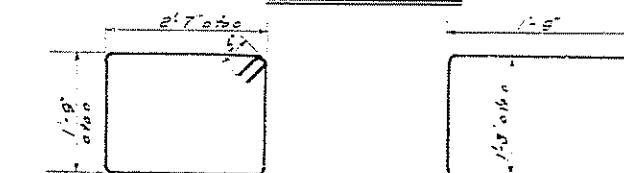
SECTION A-A



SECTION B-B



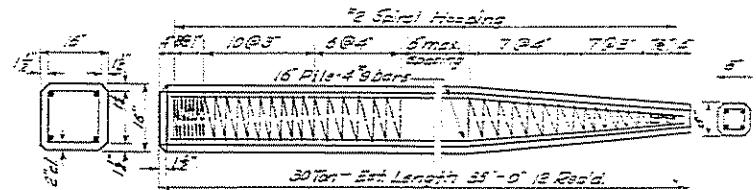
BAR-N&P



BAR-53



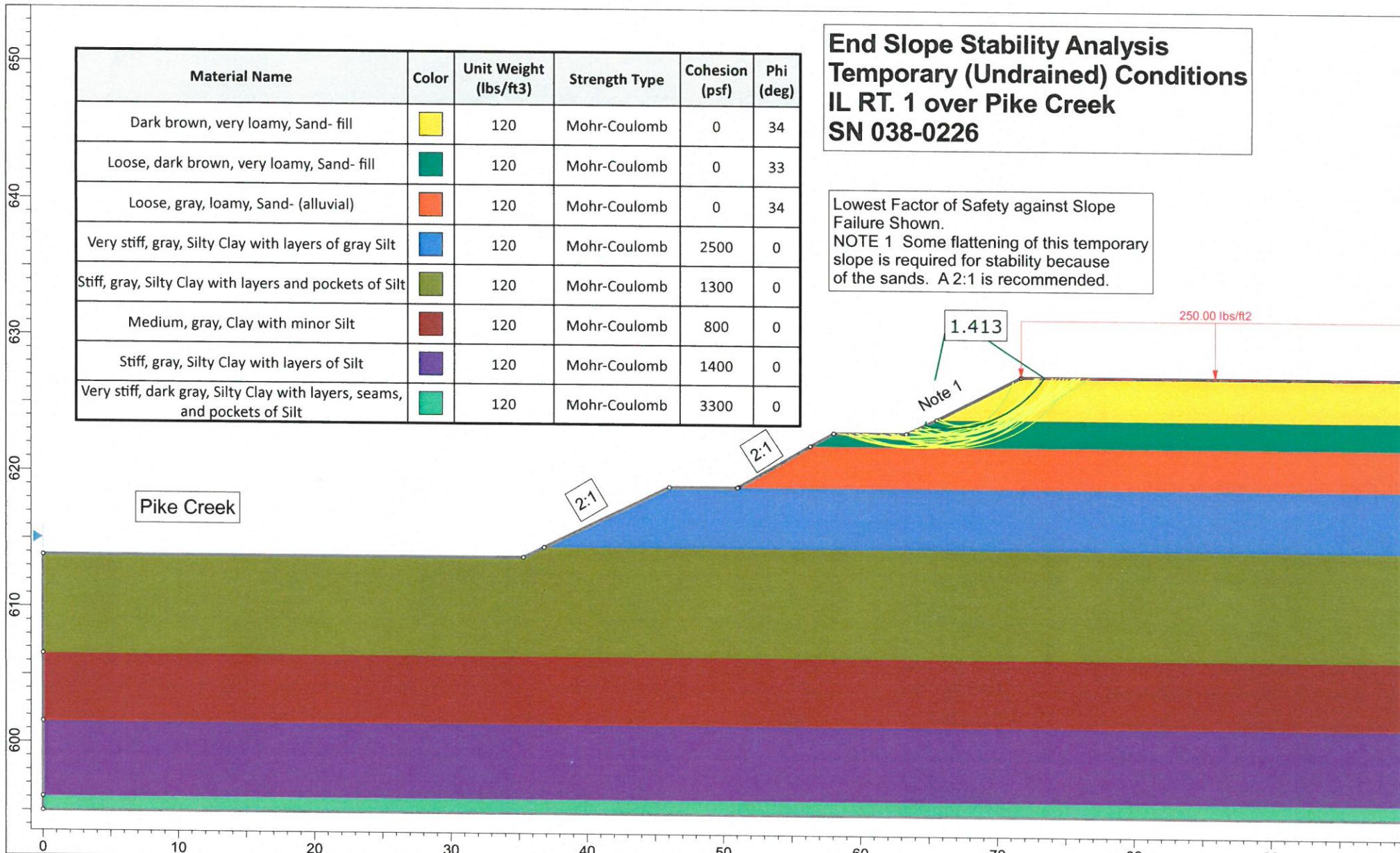
BAR-U1



DETAIL OF PRECAST CONCRETE PILES

BILL OF MATERIAL - SUBSTR

BAR	NO.	SIZE	LENGTH	SHAPE
V	80	22	3'-0"	
W	12	22	3'-0"	
Z	12	22	2'-5"	
A	16	22	3'-0"	
B	80	22	3'-0"	
C	12	22	3'-0"	
D	12	22	3'-0"	
E	12	22	3'-0"	
F	12	22	3'-0"	
G	12	22	3'-0"	
H	12	22	3'-0"	
I	12	22	3'-0"	
J	12	22	3'-0"	
K	12	22	3'-0"	
L	12	22	3'-0"	
M	12	22	3'-0"	
N	12	22	3'-0"	
O	12	22	3'-0"	
P	12	22	3'-0"	
Q	12	22	3'-0"	
R	12	22	3'-0"	
S	12	22	3'-0"	
T	12	22	3'-0"	
U	12	22	3'-0"	
V	12	22	3'-0"	
W	12	22	3'-0"	
X	12	22	3'-0"	
Y	12	22	3'-0"	
Z	12	22	3'-0"	
AA	12	22	3'-0"	
BB	12	22	3'-0"	
CC	12	22	3'-0"	
DD	12	22	3'-0"	
EE	12	22	3'-0"	
FF	12	22	3'-0"	
GG	12	22	3'-0"	
HH	12	22	3'-0"	
II	12	22	3'-0"	
JJ	12	22	3'-0"	
KK	12	22	3'-0"	
LL	12	22	3'-0"	
MM	12	22	3'-0"	
NN	12	22	3'-0"	
OO	12	22	3'-0"	
PP	12	22	3'-0"	
QQ	12	22	3'-0"	
RR	12	22	3'-0"	
SS	12	22	3'-0"	
TT	12	22	3'-0"	
UU	12	22	3'-0"	
VV	12	22	3'-0"	
WW	12	22	3'-0"	
XX	12	22	3'-0"	
YY	12	22	3'-0"	
ZZ	12	22	3'-0"	
AA	12	22	3'-0"	
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TT	12	22	3'-0"	
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FF	12	22	3'-0"	
GG	12	22	3'-0"	
HH	12	22	3'-0"	
II	12	22	3'-0"	
JJ	12	22	3'-0"	
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UU	12	22	3'-0"	
VV	12	22	3'-0"	
WW	12	22	3'-0"	
XX	12	22	3'-0"	
YY	12	22	3'-0"	
ZZ	12	22	3'-0"	
AA	12	22	3'-0"	
BB	12	22	3'-0"	
CC				



 McCleary Engineering	Project	IL 1 over Pike Creek (SN 038-0226) Slope Stability Analysis		
	Analysis Method	SLIDEINTERPRET 8.028 Bishop simplified		
	Drawn By	MEJ	Scale	1:117
	Date	10/10/2019		Company
				McCleary Engineering
SLIDEINTERPRET 8.028		File Name		Pike Creek Temporary (Undrained) Conditions.slmd

Final Scour Results - SN 038-0020

	Existing											
	50 yr			100 yr			200 yr			500 yr		
	LT	Channel	RT	LT	Channel	RT	LT	Channel	RT	LT	Channel	RT
Abutment	0		1.9	0		3.55	3.52		4.46	3.83		5.03
Pier		4.38			4.23			3.89			3.84	
Contraction	0	0	0	0	1.2	0.01	0	1.19	0.25	0	0.56	0.6
Pressure		2.52			4.51			4.91			4.66	
TOTAL Pier + Contraction*		6.90			8.74			8.80			8.50	
TOTAL Abut. + Contraction	0		1.9	0		3.56	3.52		4.71	3.83		5.63
D50 Used							0.2 mm Sand					

	Proposed											
	50 yr			100 yr			200 yr			500 yr		
	LT	Channel	RT	LT	Channel	RT	LT	Channel	RT	LT	Channel	RT
Abutment	0		0	0		0	0		0.59	1.25		1.67
Pier		4.8			4.8			4.8			4.8	
Contraction	0	0	0	0	0	0	0	0.01	0	0	0.01	0
Pressure		0			0			0			0	
TOTAL Pier + Contraction*		4.8			4.8			4.81			4.81	
TOTAL Abut. + Contraction	0		0	0		0	0		0.59	1.25		1.67
D50 Used							0.2 mm Sand					

*Pier scour used is greater of pier or pressure scour

Characteristic Soil D50 Sizes		
Sand	0.074 - 2.0	mm
Silt	0.002 - 0.074	mm
Clay	< 0.002	mm

1. Largest stone in mix no greater than 1.5 x D50
2. Thickness of layer 2.25 x D50

Common D50 sizes			
RipRap	Ibs	cube	mm
RR 1		1.5"	38
RR 2		2"	50
RR 3	10-12	4-5"	127
RR 4	40-50	7-8"	200
RR 5	90-170	10-12"	300
RR 6	300	15"	381
RR 7	400-1000	16-22"	457

JSON Raw Data Headers

Save Copy Collapse All Expand All

Filter JSON

SEISMIC DETERMINATION

```

request:
  date: "2019-10-04T17:06:20.344Z"
  referenceDocument: "AASHTO-2009"
  status: "success"
  url: "https://earthquake.usgs.gov/ws/designmaps/aashto-2009.json?Latitude=40.892&Longitude=-87.731&siteClass=C&title=SN0380226proposed"

parameters:
  latitude: 40.892
  longitude: -87.731
  siteClass: "C"
  title: "SN0380226proposed"

response:
  data:
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    fpga: 1.2
    as: 0.055
    ss: 0.106
    fa: 1.2
    sds: 0.127
    s1: 0.044
    fv: 1.7
    sd1: 0.076
    sdc: "A"
    ts: 0.594
    t0: 0.119

    sdSpectrum:
      0:
        0: 0
        1: 0.055
      1:
        0: 0.025
        1: 0.07
      2:
        0: 0.05
        1: 0.085
      3:
        0: 0.1
        1: 0.116
      4:
        0: 0.119
        1: 0.127
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        0: 0.15
        1: 0.127
      6:
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        1: 0.127
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        0: 0.3
        1: 0.127
      9:
        0: 0.35
        1: 0.127

```

SN 038-0226 (PROP)



**Illinois Department
of Transportation**

PROJECT TITLE==== IL 1 over Pike Creek SN 038-0226 (Prop)

SEISMIC SITE CLASS DETERMINATION

Substructure 1			
Base of Substruct. Elev. (or ground surf for bents)	622.93	ft.	
Pile or Shaft Dia.	12	inches	
Boring Number	#1: SE Quad: S Abut		
Top of Boring Elev.	628.63	ft.	
Approximate Fixity Elev.	616.93	ft.	

Individual Site Class Definition:

N (bar): 13 (Blows/ft.) Soil Site Class E
N_{ch} (bar): (Blows/ft.) NA
s_v (bar): 2.46 (ksf) Soil Site Class C <---Controls

Seismic Soil Column Depth	Bot. Of Sample Elevation	Layer			
		Sample Thickness (ft.)	N (ft.)	Qu (tsf)	Boundary
	626.6	2.00			B
	624.1	2.50	10		
	621.6	2.50	5		B
	619.6	2.00	5	1.00	B
	617.1	2.50	8	2.10	
2.3	614.6	2.50	9	2.30	
4.8	612.1	2.50	8	2.10	B
7.3	609.6	2.50	8	1.70	
9.8	607.1	2.50	5	1.50	
12.3	604.6	2.50	5	1.20	
14.8	602.1	2.50	6	1.20	
17.3	599.6	2.50	6	1.60	
19.8	597.1	2.50	5	1.60	B
22.3	594.6	2.50	12	2.90	B
24.8	592.1	2.50	14	4.70	
27.3	589.6	2.50	13	4.00	B
29.8	587.1	2.50	14	5.20	
32.3	584.6	2.50	6	1.20	
34.8	582.1	2.50	5	1.10	
37.3	579.6	2.50	5	1.20	B
39.8	577.1	2.50	6	1.60	
42.3	574.6	2.50	4	1.00	
44.8	572.1	2.50	5	1.10	
47.3	569.6	2.50	5	1.30	B
49.8	567.1	2.50	6	1.80	
52.3	564.6	2.50	8	1.80	
54.3	562.6	2.00	95	2.00	B
56.8	560.1	2.50	79	7.60	
59.3	557.6	2.50	240	4.60	
61.8	555.1	2.50	240	4.60	
64.3	552.6	2.50	130	4.60	
66.8	550.1	2.50	130	4.60	
69.3	547.6	2.50	400	4.60	
100.0	516.9	30.70	220	4.60	

Substructure 2			
Base of Substruct. Elev. (or ground surf for bents)	610.2	ft.	
Pile or Shaft Dia.	12	inches	
Boring Number	#1: SE Quad: S Abut		
Top of Boring Elev.	628.63	ft.	
Approximate Fixity Elev.	604.2	ft.	

Individual Site Class Definition:

N (bar): 17 (Blows/ft.) Soil Site Class D
N_{ch} (bar): (Blows/ft.) NA
s_v (bar): 2.79 (ksf) Soil Site Class C <---Controls

Seismic Soil Column Depth	Bot. Of Sample Elevation	Layer			
		Sample Thickness (ft.)	N (ft.)	Qu (tsf)	Boundary
	626.6	2.00			B
	624.1	2.50	10		
	621.6	2.50	5		B
	619.6	2.00	5	1.00	B
	617.1	2.50	8	2.10	
2.3	614.6	2.50	9	2.30	
4.8	612.1	2.50	8	2.10	B
7.3	609.6	2.50	8	1.70	
9.8	607.1	2.50	5	1.50	
12.3	604.6	2.50	5	1.20	
14.8	602.1	2.50	6	1.20	
17.3	599.6	2.50	6	1.60	
19.8	597.1	2.50	5	1.60	B
22.3	594.6	2.50	12	2.90	B
24.8	592.1	2.50	14	4.70	
27.3	589.6	2.50	13	4.00	B
29.8	587.1	2.50	14	5.20	
32.3	584.6	2.50	6	1.20	
34.8	582.1	2.50	5	1.10	
37.3	579.6	2.50	5	1.20	B
39.8	577.1	2.50	6	1.60	
42.3	574.6	2.50	4	1.00	
44.8	572.1	2.50	5	1.10	
47.3	569.6	2.50	5	1.30	B
49.8	567.1	2.50	6	1.80	
52.3	564.6	2.50	8	1.80	
54.3	562.6	2.00	95	2.00	B
56.8	560.1	2.50	79	7.60	
59.3	557.6	2.50	240	4.60	
61.8	555.1	2.50	240	4.60	
64.3	552.6	2.50	130	4.60	
66.8	550.1	2.50	130	4.60	
69.3	547.6	2.50	400	4.60	
100.0	504.3	43.30	220	4.60	

Substructure 3			
Base of Substruct. Elev. (or ground surf for bents)	610.2	ft.	
Pile or Shaft Dia.	12	inches	
Boring Number	#1: SE Quad: S Abut		
Top of Boring Elev.	628.63	ft.	
Approximate Fixity Elev.	604.2	ft.	

Individual Site Class Definition:

N (bar): 13 (Blows/ft.) Soil Site Class E
N_{ch} (bar): (Blows/ft.) NA
s_v (bar): 2.63 (ksf) Soil Site Class C <---Controls

Seismic Soil Column Depth	Bot. Of Sample Elevation	Layer			
		Sample Thickness (ft.)	N (ft.)	Qu (tsf)	Boundary
	626.0	2.50			
	624.0	2.00			B
	622.0	2.00	5		
	620.5	1.50	4		
	619.0	1.50	4		B
	616.5	2.50	6	2.50	
	614.5	2.00	9	2.50	B
	612.0	2.50	8	1.50	
	609.5	2.50	5	1.20	
	606.5	3.00	6	1.20	B
	604.0	2.50	3	0.80	
0.5	601.5	2.50	3	0.80	B
2.5	614.5	2.00	9	2.50	B
5.0	612.0	2.50	8	1.50	
7.5	609.5	2.50	5	1.20	
10.5	606.5	3.00	6	1.20	B
13.0	604.0	2.50	3	0.80	
15.5	601.5	2.50	3	0.80	B
18.0	599.0	2.50	5	1.40	
21.0	596.0	3.00	5	1.40	B
22.5	594.5	1.50	13	3.30	
25.0	592.0	2.50	13	3.30	
27.5	589.5	2.50	13	3.30	
30.0	587.0	2.50	10	2.10	
31.5	585.5	1.50	10	2.10	B
32.5	584.5	1.00	4	1.30	
35.0	582.0	2.50	4	1.30	
37.5	579.5	2.50	4	1.30	
40.0	577.0	2.50	6	1.90	
42.5	574.5	2.50	6	1.90	
45.0	572.0	2.50	5	1.30	
47.5	569.5	2.50	5	1.30	B
50.0	567.0	2.50	5	1.50	
52.0	565.0	2.00	5	1.50	B
54.5	562.5	2.50	71	4.60	
57.0	560.0	2.50	71	4.60	
58.0	559.0	1.00	71	4.60	
100.0	517.0	42.00	71	4.60	

Substructure 4			
Base of Substruct. Elev. (or ground surf for bents)	623.03	ft.	
Pile or Shaft Dia.	12	inches	
Boring Number	#2: NW Quad: N Abut		
Top of Boring Elev.	628.54	ft.	
Approximate Fixity Elev.	617.03	ft.	

Individual Site Class Definition:

N (bar): 10 (Blows/ft.) Soil Site Class E
N_{ch} (bar): (Blows/ft.) NA
s_v (bar): 2.2 (ksf) Soil Site Class C <---Controls

Seismic Soil Column Depth	Bot. Of Sample Elevation	Layer			
		Sample Thickness (ft.)	N (ft.)	Qu (tsf)	Boundary
	626.0	2.50			
	624.0	2.00			B
	622.0	2.00	5		
	620.5	1.50	4		
	619.0	1.50	4		B
	616.5	2.50	6	2.50	
	614.5	2.00	9	2.50	B
	612.0	2.50	8	1.50	
	609.5	2.50	5	1.20	
	606.5	3.00	6	1.20	B
	604.0	2.50	3	0.80	
0.5	601.5	2.50	3	0.80	B
2.5	614.5	2.00	9	2.50	B
5.0	612.0	2.50	8	1.50	
7.5	609.5	2.50	5	1.20	
10.5	606.5	3.00	6	1.20	B
13.0	604.0	2.50	3	0.80	
15.5	601.5	2.50	3	0.80	B
18.0	599.0	2.50	5	1.40	
21.0	596.0	3.00	5	1.40	B
22.5	594.5	1.50	13	3.30	
25.0	592.0	2.50	13	3.30	
27.5	589.5	2.50	13	3.30	
30.0	587.0	2.50	10	2.10	
31.5	585.5	1.50	10	2.10	B
32.5	584.5	1.00	4	1.30	
35.0	582.0	2.50	4	1.30	
37.5	579.5	2.50	4	1.30	
40.0	577.0	2.50	6	1.90	
42.5	574.5	2.50	6	1.90	
45.0	572.0	2.50	5	1.30	
47.5	569.5	2.50	5	1.	

GENERAL DATA

STRUCTURE NUMBER ===== 038-0226
 STRUCTURE TYPE ===== MULTI-SPAN
 STRUCTURE SKEW===== 0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA === ABUT 1

TOTAL STRUCTURE LENGTH===== 91.00 FT
 NUMBER OF SPANS ===== 3
 END SPAN LENGTH ===== 26.50 FT
 ADJACENT INTERIOR SPAN LENGTH ===== 34.00 FT

SUPERSTRUCTURE DATA (END OR MAIN SPAN)

BEAM TYPE ===== SLAB BRIDGE

SLAB THICKNESS ===== 15.00 IN
 SLAB F'C ===== 4.00 KSI

SUPERSTRUCTURE DATA (ADJACENT SPAN)

SLAB THICKNESS ===== 15.00 IN
 SLAB F'C ===== 4.00 KSI

ABUTMENT #1 DATA

ABUTMENT NAME ===== South
 ABUTMENT REFERENCE BORING ===== #1: SE Quad: S Abut
 BOTTOM OF ABUTMENT ELEVATION ===== 622.93 FT
 ESTIMATED NUMBER OF PILES AT ABUT. ===== 10
 PILE SPACING PERP. TO CL ===== 3.5 FT

ABUTMENT #2 DATA

ABUTMENT NAME ===== East
 ABUTMENT REFERENCE BORING ===== #2: NW Quad: N Abut
 BOTTOM OF ABUTMENT ELEVATION ===== 623.03 FT
 ESTIMATED NUMBER OF PILES AT ABUT. ===== 10
 PILE SPACING PERP. TO CL ===== 3.5 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1

BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
621.63	1.30	1.5		
619.63	2.00	1.0		
617.13	2.50	2.1		
614.63	2.50	2.3		
612.93	1.70	2.1		

10.00 FT = TOTAL DEPTH ENTERED

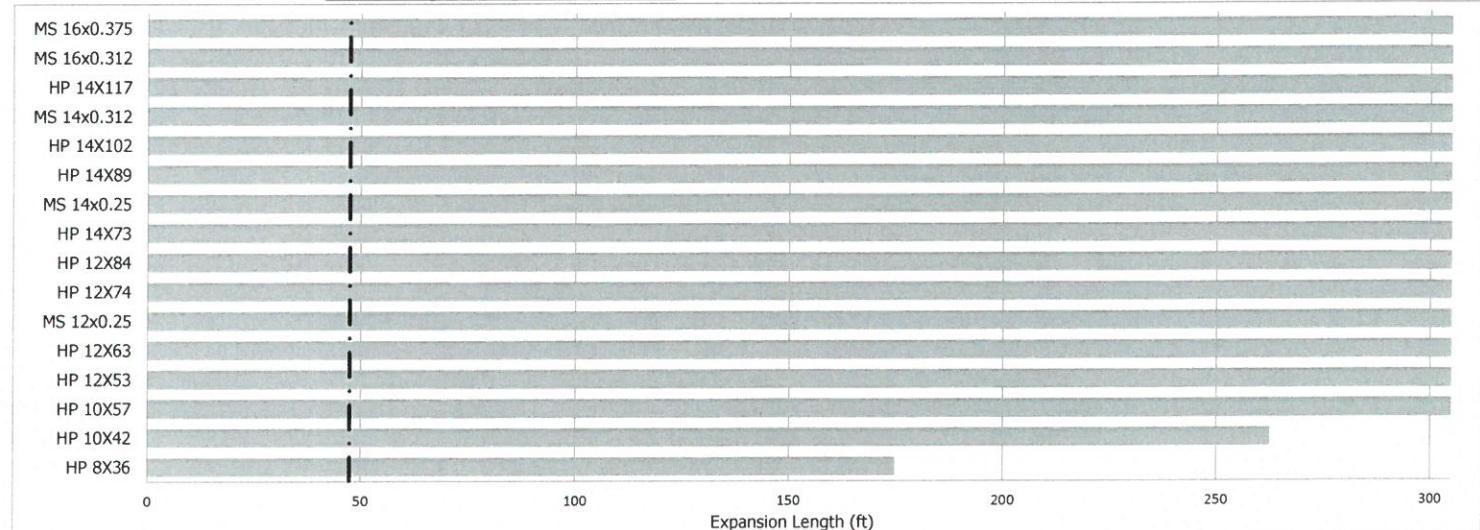
WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 1.85 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 $= 1/(1.45-[0.3*1.85]) = 1.12$ **SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2**

BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
622.04	0.99		5	1.9
620.04	2.00		5	1.9
618.54	1.50		4	1.7
617.04	1.50		4	1.7
614.54	2.50	2.50		
613.03	1.51	2.50		

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 2.09 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 $= 1/(1.45-[0.3*2.09]) = 1.22$ DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = $[1.12*10*0+1.22*10*91]/[1.12*10+1.22*10] = 47.43$ FTDISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = $[1.22*10*0+1.12*10*91]/[1.22*10+1.12*10] = 43.57$ FT**ABUT 1 (South) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW**

= Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)

	CLIENT:	IDOT - District 3	MADE BY:	CHK'D BY:	PROJ. NO.
	PROJECT:	IL 1 over Pike Creek - Bridge Replacement	JMP	JRM	P401190086
	SUBJECT:	Preliminary Foundation Loads	DATE:	DATE:	REV. NO.
			8/22/2019	8/22/2019	0

SUMMARY - PRELIMINARY FOUNDATION LOADS

Table 1 - Service Loads

	Abutment	Pier
LL	180.0 k	280.0 k
DC	160.0 k	530.0 k
DW	20.0 k	70.0 k
Total	360.0 k	880.0 k

Table 2 - Factored Loads

	Abutment	Pier
LL	310.0 k	490.0 k
DC	200.0 k	660.0 k
DW	30.0 k	100.0 k
Total	540.0 k	1250.0 k

Loads Reflect Bridge Width = 32ft
Assumes use of Integral Abutments

Pile Design Table for south abut. SN 038-0226 utilizing Boring ##1: SE Quad: S Abut

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Pile Length (ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Pile Length (ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Pile Length (ft.)
Steel HP 10 X 42								
77	42	23	77	42	18	77	42	18
85	47	25	85	47	20	86	47	20
106	58	28	106	55	23	100	55	23
135	74	30	135	61	25	110	61	25
146	80	33	146	77	28	140	77	28
152	83	38	152	96	30	174	96	30
157	87	40	157	106	38	192	106	38
165	91	43	165	109	40	199	109	40
175	96	45	175	114	43	208	114	43
178	98	48	178	122	45	222	122	45
185	102	50	185	123	48	224	123	48
193	106	53	193	128	50	233	128	50
205	113	55	205	134	53	243	134	53
214	118	58	214	143	55	260	143	55
318	175	60	318	149	58	271	149	58
319	175	62	319	220	60	401	220	60
Steel HP 10 X 57								
78	43	23	78	270	65	419	230	62
87	48	25	87	270	65	491	270	65
108	60	28	108	38	13	70	38	13
139	76	30	139	50	18	86	47	15
149	82	33	149	50	18	91	50	18
155	85	38	155	56	20	101	56	20
161	88	40	161	65	23	118	65	23
168	93	43	168	72	25	130	72	25
179	98	45	179	92	28	167	92	28
182	100	48	182	110	30	201	110	30
189	104	50	189	123	38	223	123	38
197	108	53	197	127	40	231	127	40
209	115	55	209	133	43	242	133	43
218	120	58	218	142	45	259	142	45
325	179	60	325	143	48	259	143	48
327	180	62	327	148	50	269	148	50
393	216	65	393	155	53	282	155	53
Steel HP 12 X 53								
82	45	20	82	166	55	302	166	55
96	53	23	96	173	58	315	173	58
106	58	25	106	254	60	461	254	60
134	74	28	134	266	62	484	266	62
166	91	30	166	304	65	553	304	65
Metal Shell 14"Φ w/.312" walls								
78	43	13	78	39	13	71	39	13
91	50	15	91	48	15	87	48	15
101	56	18	101	51	18	93	51	18
113	62	20	113	56	20	102	56	20
129	71	23	129	66	23	120	66	23
144	79	25	144	80	25	132	73	25
173	95	28	173	93	28	169	93	28
216	119	30	216	118	45	204	112	30
237	131	33	237	119	48	226	124	38
262	144	38	262	124	50	233	128	40
272	150	40	272	129	53	259	142	45
284	156	43	284	138	55	281	143	48
301	165	45	301	144	58	308	144	45
308	169	48	308	209	60	326	144	45
319	176	50	319	220	62	367	144	45
333	183	53	333	220	62	367	144	45
351	193	55	351	220	62	372	150	50
367	202	58	367	220	62	372	157	53
Metal Shell 16"Φ w/.312" walls								
79	43	10	79	25	55	306	168	55
92	51	13	92	28	58	319	175	58
107	59	15	107	30	60	470	259	60
118	65	18	118	33	62	493	271	62
131	72	20	131	38	65	572	314	65
151	83	23	151	40	13	72	40	13
167	92	25	167	45	15	88	49	15
204	112	28	204	48	18	94	52	18
256	141	30	256	50	20	104	57	20
279	153	33	279	53	23	122	67	23
301	166	38	301	55	25	134	73	25
313	172	40	313	58	28	172	95	28
327	180	43	327	60	30	207	114	30
347	191	45	347	62	38	228	125	38
354	195	48	354	65	40	236	130	40
367	202	50	367	65	45	247	136	43
383	211	53	383	68	50	265	146	48
405	223	55	405	70	55	276	152	50
423	232	58	423	75	58	289	159	53
Metal Shell 16"Φ w/.375" walls								
79	43	10	79	28	55	309	170	55
92	51	13	92	30	58	322	177	58
107	59	15	107	33	60	477	262	60
118	65	18	118	38	62	498	274	62
131	72	20	131	40	65	585	322	65
151	83	23	151	45	68	798	439	67
167	92	25	167	48	71	40	13	13
204	112	28	204	50	90	49	15	15
256	141	30	256	53	95	52	18	18
279	153	33	279	55	105	58	20	20
301	166	38	301	58	123	68	23	23
313	172	40	313	60	135	74	25	25
327	180	43	327	62	174	96	28	28
347	191	45	347	65	210	116	30	30
354	195	48	354	68	231	127	38	38
367	202	50	367	70	239	131	40	40
383	211	53	383	72	250	138	43	43
405	223	55	405	75	268	147	48	48
423	232	58	423	78	279	153	50	50
Steel HP 8 X 36								
62	45	28	62	53	55	292	161	53
104	57	30	104	64	55	313	172	55
113	62	33	113	74	58	326	179	58
122	67	38	122	85	60	486	267	60
127	70	40	127	96	62	507	279	62
133	73	43	133	108	65	603	332	65
141	77	45	141	121	68	817	450	67
144	79	48	144	121	71	83	46	10
149	82	50	149	121	74	99	55	13
156	86	53	156	121	78	115	64	15
165	91	55	165	121	81	129	71	18
172	95	58	172	121	84	144	79	20
245	135	62	245	121	88	164	90	23
						183	101	25
						221	121	28

Pile Design Table for Pier 1 SN 038-0226 utilizing Boring ##1: SE Quad: S Abut

Pile Design Table for Pier 2 SN 038-0226 utilizing Boring #2: NW Quad: N Abut

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
Steel HP 10 X 42			Steel HP 12 X 84			Steel HP 10 X 57		
			160	88	58	193	106	55
			235	129	60	203	112	58
			249	137	62	296	163	60
			261	143	65	313	172	62
			265	146	66	330	181	65
			274	151	68	337	185	66
			284	156	71	354	195	68
			293	161	73	371	204	71
			302	166	76	388	213	73
			312	172	78	403	222	76
			321	177	81	415	228	78
			331	182	83	427	235	81
Metal Shell 14"Φ w/.312" walls						438	241	83
	184	101	43			450	248	86
	204	112	45	163	90	58		
	220	121	48	240	132	60	186	102
	229	126	50	254	140	62	199	109
	242	133	53	268	147	65	200	110
	257	141	55	272	149	66	211	116
	270	149	58	281	155	68	225	124
Metal Shell 16"Φ w/.312" walls			291	160	71	235	130	58
	193	106	39	301	165	73	236	130
	199	109	40	310	171	76	340	187
	213	117	43	320	176	78	360	198
	237	130	45	330	181	81	380	209
	255	140	48	339	187	83	388	214
	265	145	50	349	192	86	408	225
Metal Shell 16"Φ w/.375" walls			351	173	65	428	236	71
	193	106	39	321	176	66	448	247
	199	109	40	337	186	68	468	258
	213	117	43	354	195	71	488	269
	237	130	45	371	204	73	508	280
	255	140	48	386	212	76	526	289
	265	145	50	397	218	78	539	296
	279	153	53	408	225	81	227	125
	296	163	55	314	173	65	239	131
	312	172	58	321	176	66	347	191
	770	423	60	337	186	68	368	202
Steel HP 8 X 36			354	195	71	388	213	65
	192	106	62	371	204	73	396	218
	200	110	65	386	212	76	416	229
	203	111	66	397	218	78	436	240
	210	116	68	408	225	81	456	251
	218	120	71	327	158	60	476	262
	226	124	73	332	160	62	496	273
	234	128	76	345	190	68	517	284
	241	133	78	366	201	71	533	293
	249	137	81	383	211	78	547	301
	257	141	83	396	218	76	555	305
	264	145	86	424	233	83	562	309
			436	240	86	572	287	81
Steel HP 12 X 63			443	244	86	584	297	83
Steel HP 12 X 74						595	305	86
	190	105	55	190	105	55	602	313
	200	110	58	204	112	58	615	324
	292	160	60	205	113	58	628	335
	309	170	62	216	119	53	641	346
	326	179	65	230	127	55	654	357
	332	183	66	242	133	58	667	368
	349	192	68	352	194	60	680	379
	366	201	71	372	205	62	693	390
	383	211	73	393	216	65	706	401
	396	218	76	401	220	66	719	421
	408	224	78	411	223	68	732	434
	420	231	81	461	254	73	745	446
	431	237	83	482	265	76	758	468
	443	244	86	502	276	78	771	489
Steel HP 14 X 89						784	309	86
Steel HP 14 X 102						797	317	86
			190	105	55	800	325	86
			204	112	58	813	336	86
			205	113	58	826	347	86
			216	119	53	839	358	86
			230	127	55	852	369	86
			242	133	58	865	380	86
			352	194	60	878	391	86
			372	205	62	891	402	86
			393	216	65	904	413	86
			401	220	66	917	424	86
			421	232	68	930	435	86
			441	243	71	943	446	86
			461	254	73	956	457	86
			482	265	76	969	468	86
			502	276	78	982	479	86
Steel HP 14 X 117						995	385	86
			193	106	45	1008	396	86
			206	114	48	1021	407	86
			208	114	50	1034	418	86
			218	120	53	1047	429	86
			233	128	55	1060	440	86
			245	135	58	1073	451	86
			359	197	60	1086	462	86
			379	209	62	1099	473	86
			400	220	65	1112	484	86
			408	224	66	1125	495	86
			428	236	68	1138	506	86
			449	247	71	1151	517	86
			469	258	73	1164	528	86
			489	269	76	1177	539	86
			510	280	78	1190	550	86
			530	292	81	1203	561	86
			548	302	83	1216	572	86
			562	309	86	1229	583	86
Precast 14"x 14"						1242	594	86
			190	104	35	1255	605	86
			211	116	38	1268	616	86
			213	117	39	1281	627	86
			219	120	40	1294	638	86
			235	129	43	1307	649	86
			260	143	45	1320	660	86

Pile Design Table for N Abut SN 038-0226 utilizing Boring ##2: NW Quad: N Abut



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== south abut. SN 038-0226
 REFERENCE BORING ===== #1: SE Quad: S Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 624.93 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 622.93 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 540 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 124.03 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 46.51 KIPS

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.312" walls

Pile Perimeter===== 3.665 FT.

Pile End Bearing Area===== 1.069 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
570 KIPS	367 KIPS	202 KIPS	58 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
621.63	1.30	5	Medium Sand	2.2	2.2	9.5	11.7	12	0	0	6	3
619.63	2.00	5	Fine Sand	3.2	3.2	30.0		30	0	0	16	5
617.13	2.50	2.10	8	17.2	24.6	49.6		50	0	0	27	8
614.63	2.50	2.30	9	18.3	27.0	65.5		65	0	0	36	10
612.13	2.50	2.10	8	17.2	24.6	78.0		78	0	0	43	13
609.63	2.50	1.70	8	15.0	19.9	90.7		91	0	0	50	15
607.13	2.50	1.50	5	13.8	17.6	101.0		101	0	0	56	18
604.63	2.50	1.20	5	11.8	14.1	112.7		113	0	0	62	20
602.13	2.50	1.20	6	11.8	14.1	129.2		129	0	0	71	23
599.63	2.50	1.60	6	14.4	18.8	143.6		144	0	0	79	25
597.13	2.50	1.60	5	14.4	18.8	173.2		173	0	0	95	28
594.63	2.50	2.90	12	21.4	34.0	215.8		216	0	0	119	30
592.13	2.50	4.70	14	29.8	55.1	237.4		237	0	0	131	33
589.63	2.50	4.00	13	27.2	46.9	278.6		279	0	0	153	35
587.13	2.50	5.20	14	29.8	61.0	261.5		262	0	0	144	38
584.63	2.50	1.20	6	11.8	14.1	272.1		272	0	0	150	40
582.13	2.50	1.10	5	11.0	12.9	284.3		284	0	0	156	43
579.63	2.50	1.20	5	11.8	14.1	300.7		301	0	0	165	45
577.13	2.50	1.60	6	14.4	18.8	308.1		308	0	0	169	48
574.63	2.50	1.00	4	10.2	11.7	319.5		319	0	0	176	50
572.13	2.50	1.10	5	11.0	12.9	332.8		333	0	0	183	53
569.63	2.50	1.30	5	12.5	15.2	351.2		351	0	0	193	55
567.13	2.50	1.80	6	15.6	21.1	366.8		367	0	0	202	58
564.63	2.50	1.80	8	15.6	21.1	840.7		841	0	0	462	60
562.63	2.00	95	Hard Till	72.4	479.5	832.4		832	0	0	458	62
560.13	2.50	79	Hard Till	64.3	398.7	1709.3		1709	0	0	940	65
557.63	2.50	240	Hard Till	557.6	1211.3	2266.9		2267	0	0	1247	67
555.13	2.50	240	Hard Till	557.6	1211.3	2269.3		2269	0	0	1248	70
552.63	2.50	130	Hard Till	165.5	656.1	2434.8		2435	0	0	1339	72
550.13	2.50	130	Hard Till	165.5	656.1	3963.1		3963	0	0	2180	75
547.63	2.50	400	Hard Till		2018.8							



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== south abut. SN 038-0226
 REFERENCE BORING ===== #1: SE Quad: S Abut
 LRFD or ASD or SEISMIC ===== LRF
 PILE CUTOFF ELEV. ===== 624.93 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 622.93 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 540 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 124.03 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 46.51 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.312" walls

Pile Perimeter===== 4.189 FT.
 Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
654 KIPS	423 KIPS	232 KIPS	58 FT.

BOT. OF LAYER (FT.)	UNCONF. LAYER THICK. (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
				SIDE	END BRG.	TOTAL RESIST. (KIPS)					
621.63	1.30	5	Medium Sand	2.5		14.9	15	0	0	8	3
619.63	2.00	5	Fine Sand	3.6	12.4	38.3	38	0	0	21	5
617.13	2.50	8		19.7	32.2	61.0	61	0	0	34	8
614.63	2.50	2.30		20.9	35.2	78.9	79	0	0	43	10
612.13	2.50	2.10		19.7	32.2	92.4	92	0	0	51	13
609.63	2.50	1.70		17.2	26.0	106.5	107	0	0	59	15
607.13	2.50	1.50		15.8	23.0	117.7	118	0	0	65	18
604.63	2.50	1.20		13.4	18.4	131.1	131	0	0	72	20
602.13	2.50	1.20		13.4	18.4	150.7	151	0	0	83	23
599.63	2.50	1.60		16.5	24.5	167.1	167	0	0	92	25
597.13	2.50	1.60		16.5	24.5	203.5	204	0	0	112	28
594.63	2.50	2.90		24.5	44.4	255.6	256	0	0	141	30
592.13	2.50	4.70		34.1	72.0	278.9	279	0	0	153	33
589.63	2.50	4.00		31.1	61.3	328.4	328	0	0	181	35
587.13	2.50	5.20		34.1	79.6	301.2	301	0	0	166	38
584.63	2.50	1.20		13.4	18.4	313.1	313	0	0	172	40
582.13	2.50	1.10		12.6	16.8	327.2	327	0	0	180	43
579.63	2.50	1.20		13.4	18.4	346.8	347	0	0	191	45
577.13	2.50	1.60		16.5	24.5	354.1	354	0	0	195	48
574.63	2.50	1.00		11.6	15.3	367.2	367	0	0	202	50
572.13	2.50	1.10		12.6	16.8	382.9	383	0	0	211	53
569.63	2.50	1.30		14.3	19.9	404.8	405	0	0	223	55
567.13	2.50	1.80		17.8	27.6	422.6	423	0	0	232	58
564.63	2.50	1.80		17.8	27.6	1039.1	1039	0	0	572	60
562.63	2.00	95	Hard Till	82.8	626.3	1016.4	1016	0	0	559	62
560.13	2.50	79	Hard Till	73.5	520.8	2151.2	2151	0	0	1183	65
557.63	2.50	240	Hard Till	637.3	1582.1	2788.5	2788	0	0	1534	67
555.13	2.50	240	Hard Till	637.3	1582.1	2700.6	2701	0	0	1485	70
552.63	2.50	130	Hard Till	189.2	857.0	2889.8	2890	0	0	1589	72
550.13	2.50	130	Hard Till	189.2	857.0	4858.9	4859	0	0	2672	75
547.63	2.50	400	Hard Till		2636.8						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== south abut. SN 038-0226
 REFERENCE BORING ===== #1: SE Quad: S Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 624.93 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 622.93 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 540 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 124.03 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 46.51 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.375" walls

Plugged Pile Perimeter===== 4.189 FT.

Plugged Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
782 KIPS	423 KIPS	232 KIPS	58 FT.

BOT. OF LAYER	UNCONF. THICK. LAYER (FT.)	S.P.T. N STRENGTH (TSF)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
				SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
621.63	1.30	5	Medium Sand	2.5	14.9		15	0	0	8	3
619.63	2.00	5	Fine Sand	3.6	12.4	38.3	38	0	0	21	5
617.13	2.50	8		19.7	32.2	61.0	61	0	0	34	8
614.63	2.50	9		20.9	35.2	78.9	79	0	0	43	10
612.13	2.50	8		19.7	32.2	92.4	92	0	0	51	13
609.63	2.50	8		17.2	26.0	106.5	107	0	0	59	15
607.13	2.50	5		15.8	23.0	117.7	118	0	0	65	18
604.63	2.50	5		13.4	18.4	131.1	131	0	0	72	20
602.13	2.50	6		13.4	18.4	150.7	151	0	0	83	23
599.63	2.50	6		16.5	24.5	167.1	167	0	0	92	25
597.13	2.50	5		16.5	24.5	203.5	204	0	0	112	28
594.63	2.50	12		24.5	44.4	255.6	256	0	0	141	30
592.13	2.50	14		34.1	72.0	278.9	279	0	0	153	33
589.63	2.50	13		31.1	61.3	328.4	328	0	0	181	35
587.13	2.50	14		34.1	79.6	301.2	301	0	0	166	38
584.63	2.50	6		13.4	18.4	313.1	313	0	0	172	40
582.13	2.50	5		12.6	16.8	327.2	327	0	0	180	43
579.63	2.50	5		13.4	18.4	346.8	347	0	0	191	45
577.13	2.50	6		16.5	24.5	354.1	354	0	0	195	48
574.63	2.50	4		11.6	15.3	367.2	367	0	0	202	50
572.13	2.50	5		12.6	16.8	382.9	383	0	0	211	53
569.63	2.50	5		14.3	19.9	404.8	405	0	0	223	55
567.13	2.50	6		17.8	27.6	422.6	423	0	0	232	58
564.63	2.50	8		17.8	27.6	1039.1	1039	0	0	572	60
562.63	2.00	95	Hard Till	82.8	626.3	1016.4	1016	0	0	559	62
560.13	2.50	79	Hard Till	73.5	520.8	2151.2	2151	0	0	1183	65
557.63	2.50	240	Hard Till	637.3	1582.1	2788.5	2788	0	0	1534	67
555.13	2.50	240	Hard Till	637.3	1582.1	2700.6	2701	0	0	1485	70
552.63	2.50	130	Hard Till	189.2	857.0	2889.8	2890	0	0	1689	72
550.13	2.50	130	Hard Till	189.2	857.0	4858.9	4859	0	0	2672	75
547.63	2.50	400	Hard Till		2636.8						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 1 SN 038-0226
 REFERENCE BORING ===== #1: SE Quad: S Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 624.96 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 610.20 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== Scour
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 610.20 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

Pier 1 SN 038-0226

#1: SE Quad: S Abut

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
570 KIPS	297 KIPS	163 KIPS	58 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1250 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 287.11 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 107.67 KIPS

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w. 312" walls

Pile Perimeter===== 3.665 FT.

Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
				SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
609.63	0.57	1.70	8	3.4	21.0		21	0	0	12	15
607.13	2.50	1.50	5	13.8	17.6	31.3	31	0	0	17	18
604.63	2.50	1.20	5	11.8	14.1	43.0	43	0	0	24	20
602.13	2.50	1.20	6	11.8	14.1	59.5	59	0	0	33	23
599.63	2.50	1.60	6	14.4	18.8	73.9	74	0	0	41	25
597.13	2.50	1.60	5	14.4	18.8	103.6	104	0	0	57	28
594.63	2.50	2.90	12	21.4	34.0	146.1	146	0	0	80	30
592.13	2.50	4.70	14	29.8	55.1	167.7	168	0	0	92	33
589.63	2.50	4.00	13	27.2	46.9	209.0	209	0	0	115	35
587.13	2.50	5.20	14	29.8	61.0	191.9	192	0	0	106	38
584.63	2.50	1.20	6	11.8	14.1	202.5	202	0	0	111	40
582.13	2.50	1.10	5	11.0	12.9	214.6	215	0	0	118	43
579.63	2.50	1.20	5	11.8	14.1	231.1	231	0	0	127	45
577.13	2.50	1.60	6	14.4	18.8	238.4	238	0	0	131	48
574.63	2.50	1.00	4	10.2	11.7	249.8	250	0	0	137	50
572.13	2.50	1.10	5	11.0	12.9	263.1	263	0	0	145	53
569.63	2.50	1.30	5	12.5	15.2	281.5	281	0	0	155	55
567.13	2.50	1.80	6	15.6	21.1	297.1	297	0	0	163	58
564.63	2.50	1.80	8	15.6	21.1	771.0	771	0	0	424	60
562.63	2.00	95	Hard Till	72.4	479.5	762.7	763	0	0	420	62
560.13	2.50	79	Hard Till	64.3	398.7	1639.6	1640	0	0	902	65
557.63	2.50	240	Hard Till	557.6	1211.3	2197.2	2197	0	0	1208	67
555.13	2.50	240	Hard Till	557.6	1211.3	2199.6	2200	0	0	1240	70
552.63	2.50	130	Hard Till	165.5	656.1	2365.2	2365	0	0	1301	72
550.13	2.50	130	Hard Till	165.5	656.1	3893.4	3893	0	0	2141	75
547.63	2.50	400	Hard Till		2018.8						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 1 SN 038-0226
 REFERENCE BORING ===== #1: SE Quad: S Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 624.96 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 610.20 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== Scour
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 610.20 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1250 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 287.11 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 107.67 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/ 312" walls

Pile Perimeter===== 4.189 FT.

Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
654 KIPS	343 KIPS	189 KIPS	58 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)	
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)						
609.63	0.57	1.70	8		3.9		26.9	27	0	0	15	15	
607.13	2.50	1.50	5		15.8	23.0	38.1	38	0	0	21	18	
604.63	2.50	1.20	5		13.4	18.4	51.5	51	0	0	28	20	
602.13	2.50	1.20	6		13.4	18.4	71.0	71	0	0	39	23	
599.63	2.50	1.60	6		16.5	24.5	87.5	88	0	0	48	25	
597.13	2.50	1.60	5		16.5	24.5	123.9	124	0	0	68	28	
594.63	2.50	2.90	12		24.5	44.4	176.0	176	0	0	97	30	
592.13	2.50	4.70	14		34.1	72.0	199.3	199	0	0	110	33	
589.63	2.50	4.00	13		31.1	61.3	248.8	249	0	0	137	35	
587.13	2.50	5.20	14		34.1	79.6	221.6	222	0	0	122	38	
584.63	2.50	1.20	6		13.4	18.4	233.5	233	0	0	128	40	
582.13	2.50	1.10	5		12.6	16.8	247.6	248	0	0	136	43	
579.63	2.50	1.20	5		13.4	18.4	267.1	267	0	0	147	45	
577.13	2.50	1.60	6		16.5	24.5	274.4	274	0	0	151	48	
574.63	2.50	1.00	4		11.6	15.3	287.6	288	0	0	158	50	
572.13	2.50	1.10	5		12.6	16.8	303.2	303	0	0	167	53	
569.63	2.50	1.30	5		14.3	19.9	325.1	325	0	0	179	55	
567.13	2.50	1.80	6		17.8	27.6	343.0	343	0	0	189	58	
564.63	2.50	1.80	8		17.8	27.6	959.5	959	0	0	528	60	
562.63	2.00	95		Hard Till	82.8	626.3	936.8	937	0	0	515	62	
560.13	2.50	79		Hard Till	73.5	520.8	2071.6	2072	0	0	1139	65	
557.63	2.50	240		Hard Till	637.3	1582.1	2708.9	2709	0	0	1490	67	
555.13	2.50	240		Hard Till	637.3	1582.1	2621.0	2621	0	0	1442	70	
552.63	2.50	130		Hard Till	189.2	857.0	2810.2	2810	0	0	1546	72	
550.13	2.50	130		Hard Till	189.2	857.0	4779.2	4779	0	0	2629	75	
547.63	2.50	400		Hard Till		2636.8							



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 1 SN 038-0226
 REFERENCE BORING ===== #1: SE Quad: S Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 624.96 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 610.20 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) === Scour
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 610.20 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1250 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 287.11 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 107.67 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.375" walls

Plugged Pile Perimeter===== 4.189 FT.

Plugged Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses			
Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
782 KIPS	343 KIPS	189 KIPS	58 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (TSF.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
609.63	0.57	1.70	8		3.9		26.9	27	0	0	15	15
607.13	2.50	1.50	5		15.8	23.0	38.1	38	0	0	21	18
604.63	2.50	1.20	5		13.4	18.4	51.5	51	0	0	28	20
602.13	2.50	1.20	6		13.4	18.4	71.0	71	0	0	39	23
599.63	2.50	1.60	6		16.5	24.5	87.5	88	0	0	48	25
597.13	2.50	1.60	5		16.5	24.5	123.9	124	0	0	68	28
594.63	2.50	2.90	12		24.5	44.4	176.0	176	0	0	97	30
592.13	2.50	4.70	14		34.1	72.0	199.3	199	0	0	110	33
589.63	2.50	4.00	13		31.1	61.3	248.8	249	0	0	137	35
587.13	2.50	5.20	14		34.1	79.6	221.6	222	0	0	122	38
584.63	2.50	1.20	6		13.4	18.4	233.5	233	0	0	128	40
582.13	2.50	1.10	5		12.6	16.8	247.6	248	0	0	136	43
579.63	2.50	1.20	5		13.4	18.4	267.1	267	0	0	147	45
577.13	2.50	1.60	6		16.5	24.5	274.4	274	0	0	151	48
574.63	2.50	1.00	4		11.6	15.3	287.6	288	0	0	158	50
572.13	2.50	1.10	5		12.6	16.8	303.2	303	0	0	167	53
569.63	2.50	1.30	5		14.3	19.9	325.1	325	0	0	179	55
567.13	2.50	1.80	6		17.8	27.6	343.0	343	0	0	189	58
564.63	2.50	1.80	8		17.8	27.6	959.5	959	0	0	528	60
562.63	2.00		95	Hard Till	82.8	626.3	936.8	937	0	0	515	62
560.13	2.50		79	Hard Till	73.5	520.8	2071.6	2072	0	0	1439	65
557.63	2.50		240	Hard Till	637.3	1582.1	2708.9	2709	0	0	1490	67
555.13	2.50		240	Hard Till	637.3	1582.1	2621.0	2621	0	0	1442	70
552.63	2.50		130	Hard Till	189.2	857.0	2810.2	2810	0	0	1546	72
550.13	2.50		130	Hard Till	189.2	857.0	4779.2	4779	0	0	2629	75
547.63	2.50		400	Hard Till		2636.8						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== Pier 2 SN 038-0226
 REFERENCE BORING ===== #2: NW Quad: N Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 625.00 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 610.20 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== Scour
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 610.20 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1250 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 287.11 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 107.67 KIPS

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.312" walls

Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
570 KIPS	270 KIPS	149 KIPS	58 FT.

BOT. OF LAYER (FT.)	LAYER THICK.	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
609.54	0.66	1.20	5		3.1	14.1	17.2	17	0	0	9	15
606.54	3.00	1.20	6		14.1	26.6		27	0	0	15	18
604.04	2.50	0.80	3		8.5	9.4	35.1	35	0	0	19	21
601.54	2.50	0.80	3		8.5	9.4	50.6	51	0	0	28	23
599.04	2.50	1.40	5		13.2	16.4	63.7	64	0	0	35	26
596.04	3.00	1.40	5		15.8	16.4	101.8	102	0	0	56	29
594.54	1.50	3.30	13		14.1	38.7	115.9	116	0	0	64	30
592.04	2.50	3.30	13		23.5	38.7	139.4	139	0	0	77	33
589.54	2.50	3.30	13		23.5	38.7	148.9	149	0	0	82	35
587.04	2.50	2.10	10		17.2	24.6	166.1	166	0	0	91	38
585.54	1.50	2.10	10		10.3	24.6	167.0	167	0	0	92	39
584.54	1.00	1.30	4		5.0	15.2	172.0	172	0	0	95	40
582.04	2.50	1.30	4		12.5	15.2	184.5	184	0	0	101	43
579.54	2.50	1.30	4		12.5	15.2	204.0	204	0	0	112	45
577.04	2.50	1.90	6		16.2	22.3	220.2	220	0	0	121	48
574.54	2.50	1.90	6		16.2	22.3	229.3	229	0	0	126	50
572.04	2.50	1.30	5		12.5	15.2	241.8	242	0	0	133	53
569.54	2.50	1.30	5		12.5	15.2	256.6	257	0	0	141	55
567.04	2.50	1.50	5		13.8	17.6	270.4	270	0	0	149	58
565.04	2.00	1.50	5		11.0	17.6	622.2	622	0	0	342	60
562.54	2.50	71		Hard Till	53.0	358.3	675.2	675	0	0	374	62
560.04	2.50	71		Hard Till	53.0	358.3	728.2	728	0	0	401	65
559.04	1.00	71		Hard Till	21.2	358.3	749.4	749	0	0	412	66
556.54	2.50	71		Hard Till	53.0	358.3	802.5	802	0	0	444	68
554.04	2.50	71		Hard Till	53.0	358.3	855.5	856	0	0	471	71
551.54	2.50	71		Hard Till	53.0	358.3	908.5	909	0	0	500	73
549.04	2.50	71		Hard Till	53.0	358.3	961.6	962	0	0	529	76
546.54	2.50	71		Hard Till	53.0	358.3	1014.6	1015	0	0	558	78
544.04	2.50	71		Hard Till	53.0	358.3	1067.6	1068	0	0	582	81
541.54	2.50	71		Hard Till	53.0	358.3	1120.7	1121	0	0	616	83
539.04	2.50	71		Hard Till	53.0	358.3	1173.7	1174	0	0	646	86
536.54	2.50	71		Hard Till		358.3						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE ===== Pier 2 SN 038-0226
 REFERENCE BORING ===== #2: NW Quad: N Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 625.00 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 610.20 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== Scour
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 610.20 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1250 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 287.11 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 107.67 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.312" walls

Pile Perimeter===== 4.189 FT.

Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
654 KIPS	312 KIPS	172 KIPS	58 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE	END BRG.	TOTAL RESIST. (KIPS)					
609.54	0.66	1.20	5		3.5	21.9		22	0	0	12	15
606.54	3.00	1.20	6		16.1	18.4	31.9	32	0	0	18	18
604.04	2.50	0.80	3		9.7	12.3	41.6	42	0	0	23	21
601.54	2.50	0.80	3		9.7	12.3	60.5	60	0	0	33	23
599.04	2.50	1.40	5		15.0	21.4	75.5	75	0	0	42	26
596.04	3.00	1.40	5		18.0	21.4	122.6	123	0	0	67	29
594.54	1.50	3.30	13		16.1	50.5	138.8	139	0	0	76	30
592.04	2.50	3.30	13		26.9	50.5	165.6	166	0	0	91	33
589.54	2.50	3.30	13		26.9	50.5	174.1	174	0	0	96	35
587.04	2.50	2.10	10		19.7	32.2	193.8	194	0	0	107	38
585.54	1.50	2.10	10		11.8	32.2	193.4	193	0	0	106	39
584.54	1.00	1.30	4		5.7	19.9	199.1	199	0	0	109	40
582.04	2.50	1.30	4		14.3	19.9	213.3	213	0	0	117	43
579.54	2.50	1.30	4		14.3	19.9	236.8	237	0	0	130	45
577.04	2.50	1.90	6		18.5	29.1	255.2	255	0	0	140	48
574.54	2.50	1.90	6		18.5	29.1	264.5	265	0	0	145	50
572.04	2.50	1.30	5		14.3	19.9	278.8	279	0	0	153	53
569.54	2.50	1.30	5		14.3	19.9	296.1	296	0	0	163	55
567.04	2.50	1.50	5		15.8	23.0	311.9	312	0	0	172	58
565.04	2.00	1.50	5		12.6	23.0	769.5	770	0	0	423	60
562.54	2.50	71		Hard Till	60.6	468.0	830.2	830	0	0	457	62
560.04	2.50	71		Hard Till	60.6	468.0	890.8	891	0	0	490	65
559.04	1.00	71		Hard Till	24.2	468.0	915.0	915	0	0	503	66
556.54	2.50	71		Hard Till	60.6	468.0	975.6	976	0	0	537	68
554.04	2.50	71		Hard Till	60.6	468.0	1036.2	1036	0	0	570	71
551.54	2.50	71		Hard Till	60.6	468.0	1096.8	1097	0	0	603	73
549.04	2.50	71		Hard Till	60.6	468.0	1157.4	1157	0	0	637	76
546.54	2.50	71		Hard Till	60.6	468.0	1218.1	1218	0	0	670	78
544.04	2.50	71		Hard Till	60.6	468.0	1278.7	1279	0	0	703	84
541.54	2.50	71		Hard Till	60.6	468.0	1339.3	1339	0	0	737	83
539.04	2.50	71		Hard Till	60.6	468.0	1399.9	1400	0	0	770	86
536.54	2.50	71		Hard Till		468.0						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE=====	Pier 2 SN 038-0226
REFERENCE BORING =====	#2: NW Quad: N Abut
LRFD or ASD or SEISMIC =====	LRFD
PILE CUTOFF ELEV. =====	625.00 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING =====	610.20 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====	Scour
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====	610.20 ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====	ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1250 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 287.11 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 107.67 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.375" walls

Plugged Pile Perimeter===== 4.189 FT.

Plugged Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
782 KIPS	770 KIPS	423 KIPS	60 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (TSF.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
609.54	0.66	1.20	5		3.5	21.9		22	0	0	12	15
606.54	3.00	1.20	6		16.1	31.9		32	0	0	18	18
604.04	2.50	0.80	3		9.7	12.3	41.6	42	0	0	23	21
601.54	2.50	0.80	3		9.7	12.3	60.5	60	0	0	33	23
599.04	2.50	1.40	5		15.0	21.4	75.5	75	0	0	42	26
596.04	3.00	1.40	5		18.0	21.4	122.6	123	0	0	67	29
594.54	1.50	3.30	13		16.1	50.5	138.8	139	0	0	76	30
592.04	2.50	3.30	13		26.9	50.5	165.6	166	0	0	91	33
589.54	2.50	3.30	13		26.9	50.5	174.1	174	0	0	96	35
587.04	2.50	2.10	10		19.7	32.2	193.8	194	0	0	107	38
585.54	1.50	2.10	10		11.8	32.2	193.4	193	0	0	106	39
584.54	1.00	1.30	4		5.7	19.9	199.1	199	0	0	109	40
582.04	2.50	1.30	4		14.3	19.9	213.3	213	0	0	117	43
579.54	2.50	1.30	4		14.3	19.9	236.8	237	0	0	130	45
577.04	2.50	1.90	6		18.5	29.1	255.2	255	0	0	140	48
574.54	2.50	1.90	6		18.5	29.1	264.5	265	0	0	145	50
572.04	2.50	1.30	5		14.3	19.9	278.8	279	0	0	153	53
569.54	2.50	1.30	5		14.3	19.9	296.1	296	0	0	163	55
567.04	2.50	1.50	5		15.8	23.0	311.9	312	0	0	172	58
565.04	2.00	1.50	5		12.6	23.0	769.5	770	0	0	423	60
562.54	2.50	71		Hard Till	60.6	468.0	830.2	830	0	0	457	62
560.04	2.50	71		Hard Till	60.6	468.0	890.8	891	0	0	490	65
559.04	1.00	71		Hard Till	24.2	468.0	915.0	915	0	0	503	66
556.54	2.50	71		Hard Till	60.6	468.0	975.6	976	0	0	537	68
554.04	2.50	71		Hard Till	60.6	468.0	1036.2	1036	0	0	570	71
551.54	2.50	71		Hard Till	60.6	468.0	1096.8	1097	0	0	603	73
549.04	2.50	71		Hard Till	60.6	468.0	1157.4	1157	0	0	637	76
546.54	2.50	71		Hard Till	60.6	468.0	1218.1	1218	0	0	670	78
544.04	2.50	71		Hard Till	60.6	468.0	1278.7	1279	0	0	703	81
541.54	2.50	71		Hard Till	60.6	468.0	1339.3	1339	0	0	737	83
539.04	2.50	71		Hard Till	60.6	468.0	1399.9	1400	0	0	770	86
536.54	2.50	71		Hard Till		468.0						



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== N Abut SN 038-0226
 REFERENCE BORING ===== #2: NW Quad: N Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 625.03 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 623.03 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 540 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 124.03 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 46.51 KIPS

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/ 312" walls

Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
570 KIPS	333 KIPS	183 KIPS	58 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
622.04	0.99	5	Medium Sand	1.7	7.4			7	0	0	4	3
620.54	1.50	4	Medium Sand	2.0	5.7	12.9		13	0	0	7	4
619.04	1.50	4	Medium Sand	2.0	9.2	35.0		35	0	0	19	6
616.54	2.50	2.50	6		19.3	29.3	54.4	54	0	0	30	8
614.54	2.00	2.50	9		15.5	29.3	58.1	58	0	0	32	10
612.04	2.50	1.50	8		13.8	17.6	68.4	68	0	0	38	13
609.54	2.50	1.20	5		11.8	14.1	80.1	80	0	0	44	15
606.54	3.00	1.20	6		14.1	14.1	89.5	90	0	0	49	18
604.04	2.50	0.80	3		8.5	9.4	98.0	98	0	0	54	21
601.54	2.50	0.80	3		8.5	9.4	113.5	114	0	0	62	23
599.04	2.50	1.40	5		13.2	16.4	126.7	127	0	0	70	26
596.04	3.00	1.40	5		15.8	16.4	164.7	165	0	0	91	29
594.54	1.50	3.30	13		14.1	38.7	178.8	179	0	0	98	30
592.04	2.50	3.30	13		23.5	38.7	202.3	202	0	0	111	33
589.54	2.50	3.30	13		23.5	38.7	211.8	212	0	0	116	35
587.04	2.50	2.10	10		17.2	24.6	229.0	229	0	0	126	38
585.54	1.50	2.10	10		10.3	24.6	230.0	230	0	0	126	39
584.54	1.00	1.30	4		5.0	15.2	235.0	235	0	0	129	40
582.04	2.50	1.30	4		12.5	15.2	247.4	247	0	0	136	43
579.54	2.50	1.30	4		12.5	15.2	266.9	267	0	0	147	45
577.04	2.50	1.90	6		16.2	22.3	283.1	283	0	0	156	48
574.54	2.50	1.90	6		16.2	22.3	292.2	292	0	0	161	50
572.04	2.50	1.30	5		12.5	15.2	304.7	305	0	0	168	53
569.54	2.50	1.30	5		12.5	15.2	319.5	320	0	0	176	55
567.04	2.50	1.50	5		13.8	17.6	333.3	333	0	0	183	58
565.04	2.00	1.50	5		11.0	17.6	685.1	685	0	0	377	60
562.54	2.50	71	Hard Till	53.0	358.3	738.1		738	0	0	406	62
560.04	2.50	71	Hard Till	53.0	358.3	791.2		791	0	0	435	65
559.04	1.00	71	Hard Till	21.2	358.3	812.4		812	0	0	447	66
556.54	2.50	71	Hard Till	53.0	358.3	865.4		865	0	0	476	68
554.04	2.50	71	Hard Till	53.0	358.3	918.4		918	0	0	505	71
551.54	2.50	71	Hard Till	53.0	358.3	971.5		971	0	0	534	73
549.04	2.50	71	Hard Till	53.0	358.3	1024.5		1025	0	0	563	76
546.54	2.50	71	Hard Till	53.0	358.3	1077.5		1078	0	0	593	78
544.04	2.50	71	Hard Till	53.0	358.3	1130.6		1131	0	0	622	81
541.54	2.50	71	Hard Till	53.0	358.3	1183.6		1184	0	0	651	83
539.04	2.50	71	Hard Till	53.0	358.3	1236.6		1237	0	0	680	86
536.54	2.50	71	Hard Till		358.3							



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== N Abut SN 038-0226
 REFERENCE BORING ===== #2: NW Quad: N Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 625.03 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 623.03 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., OR DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 540 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 124.03 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 46.51 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.312" walls

Pile Perimeter===== 4.189 FT.
 Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
654 KIPS	384 KIPS	211 KIPS	58 FT.

BOT. OF LAYER (FT.)	LAYER THICK.	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
622.04	0.99	5	Medium Sand	1.9	9.4			9	0	0	5	3
620.54	1.50	4	Medium Sand	2.3	16.2			16	0	0	9	4
619.04	1.50	4	Medium Sand	2.3	44.8			45	0	0	25	6
616.54	2.50	6		22.1	38.3	66.9		67	0	0	37	8
614.54	2.00	9		17.7	38.3	69.3		69	0	0	38	10
612.04	2.50	8		15.8	23.0	80.4		80	0	0	44	13
609.54	2.50	5		13.4	18.4	93.9		94	0	0	52	15
606.54	3.00	6		16.1	18.4	103.8		104	0	0	57	18
604.04	2.50	3		9.7	12.3	113.5		114	0	0	62	21
601.54	2.50	3		9.7	12.3	132.4		132	0	0	73	23
599.04	2.50	5		15.0	21.4	147.4		147	0	0	81	26
596.04	3.00	5		18.0	21.4	194.6		195	0	0	107	29
594.54	1.50	13		16.1	50.5	210.7		211	0	0	116	30
592.04	2.50	13		26.9	50.5	237.6		238	0	0	131	33
589.54	2.50	13		26.9	50.5	246.1		246	0	0	135	35
587.04	2.10	10		19.7	32.2	265.8		266	0	0	146	38
585.54	2.10	10		11.8	32.2	265.3		265	0	0	146	39
584.54	1.00	4		5.7	19.9	271.0		271	0	0	149	40
582.04	2.50	4		14.3	19.9	285.3		285	0	0	157	43
579.54	2.50	4		14.3	19.9	308.7		309	0	0	170	45
577.04	2.50	6		18.5	29.1	327.2		327	0	0	180	48
574.54	2.50	6		18.5	29.1	336.5		336	0	0	185	50
572.04	2.50	5		14.3	19.9	350.7		351	0	0	193	53
569.54	2.50	5		14.3	19.9	368.0		368	0	0	202	55
567.04	2.50	5		15.8	23.0	383.8		384	0	0	211	58
565.04	2.00	5		12.6	23.0	841.5		844	0	0	463	60
562.54	2.50	71	Hard Till	60.6	468.0	902.1		902	0	0	496	62
560.04	2.50	71	Hard Till	60.6	468.0	962.7		963	0	0	529	65
559.04	1.00	71	Hard Till	24.2	468.0	986.9		987	0	0	543	66
556.54	2.50	71	Hard Till	60.6	468.0	1047.6		1048	0	0	576	68
554.04	2.50	71	Hard Till	60.6	468.0	1108.2		1108	0	0	609	71
551.54	2.50	71	Hard Till	60.6	468.0	1168.8		1169	0	0	643	73
549.04	2.50	71	Hard Till	60.6	468.0	1229.4		1229	0	0	676	76
546.54	2.50	71	Hard Till	60.6	468.0	1290.0		1290	0	0	709	78
544.04	2.50	71	Hard Till	60.6	468.0	1350.6		1351	0	0	743	81
541.54	2.50	71	Hard Till	60.6	468.0	1411.2		1411	0	0	776	83
539.04	2.50	71	Hard Till	60.6	468.0	1471.8		1472	0	0	809	86
536.54	2.50	71	Hard Till	468.0								



IDOT STATIC METHOD OF ESTIMATING PILE LENGTH

SUBSTRUCTURE===== N Abut SN 038-0226
 REFERENCE BORING ===== #2: NW Quad: N Abut
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 625.03 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 623.03 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 540 kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 34.83 ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 124.03 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 46.51 KIPS

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.375" walls

Plugged Pile Perimeter===== 4.189 FT.

Plugged Pile End Bearing Area===== 1.396 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
782 KIPS	384 KIPS	211 KIPS	58 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
				SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
622.04	0.99	5	Medium Sand	1.9	7.5	9.4	9	0	0	5	3
620.54	1.50	4	Medium Sand	2.3	12.0	16.2	16	0	0	9	4
619.04	1.50	4	Medium Sand	2.3	38.3	44.8	45	0	0	25	6
616.54	2.50	6		22.1	38.3	66.9	67	0	0	37	8
614.54	2.00	9		17.7	38.3	69.3	69	0	0	38	10
612.04	2.50	8		15.8	23.0	80.4	80	0	0	44	13
609.54	2.50	5		13.4	18.4	93.9	94	0	0	52	15
606.54	3.00	6		16.1	18.4	103.8	104	0	0	57	18
604.04	2.50	3		9.7	12.3	113.5	114	0	0	62	21
601.54	2.50	3		9.7	12.3	132.4	132	0	0	73	23
599.04	2.50	5		15.0	21.4	147.4	147	0	0	81	26
596.04	3.00	5		18.0	21.4	194.6	195	0	0	107	29
594.54	1.50	13		16.1	50.5	210.7	211	0	0	116	30
592.04	2.50	13		26.9	50.5	237.6	238	0	0	131	33
589.54	2.50	13		26.9	50.5	246.1	246	0	0	135	35
587.04	2.10	10		19.7	32.2	265.8	266	0	0	146	38
585.54	2.10	10		11.8	32.2	265.3	265	0	0	146	39
584.54	1.00	4		5.7	19.9	271.0	271	0	0	149	40
582.04	2.50	4		14.3	19.9	285.3	285	0	0	157	43
579.54	2.50	4		14.3	19.9	308.7	309	0	0	170	45
577.04	2.50	6		18.5	29.1	327.2	327	0	0	180	48
574.54	2.50	6		18.5	29.1	336.5	336	0	0	185	50
572.04	2.50	5		14.3	19.9	350.7	351	0	0	193	53
569.54	2.50	5		14.3	19.9	368.0	368	0	0	202	55
567.04	2.50	5		15.8	23.0	383.8	384	0	0	211	58
565.04	2.00	5		12.6	23.0	841.5	841	0	0	463	60
562.54	2.50	71	Hard Till	60.6	468.0	902.1	902	0	0	496	62
560.04	2.50	71	Hard Till	60.6	468.0	962.7	963	0	0	529	65
559.04	1.00	71	Hard Till	24.2	468.0	986.9	987	0	0	543	66
556.54	2.50	71	Hard Till	60.6	468.0	1047.6	1048	0	0	576	68
554.04	2.50	71	Hard Till	60.6	468.0	1108.2	1108	0	0	609	71
551.54	2.50	71	Hard Till	60.6	468.0	1168.8	1169	0	0	643	73
549.04	2.50	71	Hard Till	60.6	468.0	1229.4	1229	0	0	676	76
546.54	2.50	71	Hard Till	60.6	468.0	1290.0	1290	0	0	709	78
544.04	2.50	71	Hard Till	60.6	468.0	1350.6	1351	0	0	743	84
541.54	2.50	71	Hard Till	60.6	468.0	1411.2	1411	0	0	776	83
539.04	2.50	71	Hard Till	60.6	468.0	1471.8	1472	0	0	809	86
536.54	2.50	71	Hard Till	468.0							