



## TECHNICAL MEMORANDUM

**To:** David Skaleski, P.E.

**From:** Rachel Miller, P.E.  
Dawn Edgell, P.E.

**Date:** September 9, 2024

**Subject:** IDOT PTB 198-003  
Geotechnical Recommendations  
I-80 Temporary Soil Retention System

This design memorandum presents recommendations for the proposed temporary soil retention system along I-80 near the Wheeler Avenue bridge in Joliet, Illinois. The purpose of this memorandum is to provide design recommendations to design the retaining system. GSG has completed soil borings at this proposed location as part of the I-80 over Des Plaines River Bridge project: IDOT PTB 198-003.

### 1. INTRODUCTION

Based on information provided by WSP, a TSRS (temporary soil retention system) is required along westbound I-80 near the Wheeler Avenue bridge. The dimensions of the temporary retaining wall are currently unknown.

**Table 1** provides a list of the five (5) soil borings completed in this area that are being used for design of the temporary structure. The borings were completed within the I-80 median separating the eastbound and westbound lanes.

**Table 1 – Boring Information**

Boring	Northing	Easting	Ground Surface Elevation (ft)	Depth (ft)
TSRS-B-1	1764809.064	1047011.349	616.33	20.8*
TSRS-B-2	1764805.990	1046942.417	615.46	28.5**
TSRS-B-3	1764801.414	1046860.765	614.67	19.0*
TSRS-B-4	1764792.706	1046669.011	612.08	30.5**
TSRS-B-5	1764792.253	1046590.487	611.92	20.0*

\*borings were terminated upon reaching auger refusal on bedrock

\*\*includes a rock core

Copies of the soil boring logs are attached.

## 2. RECOMMENDATIONS

The surficial materials at each of the borings consisted of 2 inches of topsoil. The subsurface soil typically consisted of silty clay/silty clay loam fill materials to depths of about 2 to 3 feet (El. 613.3 to 609.1 feet). Below the fill, the borings encountered native, stiff to hard, brown and gray to gray silty clay to depths of 10.5 to 15.5 feet (El. 601.4 to 599.2 feet). The unconfined compressive strength of the native clay soils ranged from 1.5 to 5.0 tons per square foot (tsf). The silty clay soils were underlain by layers of medium dense to extremely dense sand, silt, and gravel to auger refusal on limestone bedrock at depths of 18 to 20.8 feet (El. 597.0 to 591.9 feet). The granular soils exhibited SPT N-values of 16 blows per foot (bpf) to 50 blows to drive the split spoon 3 inches.

Rock core samples were collected at two (2) of the soil boring locations. The bedrock cores generally consisted of brown and gray limestone, with slight to moderate weathering and high levels of fracturing. Photographs of the cores recovered and RQD values are included with each boring log in **Attachment 2**.

Water levels were checked in each boring to determine the general groundwater conditions present at the site and were measured while drilling and after each boring was completed. Groundwater was not encountered in the borings while drilling or immediately after drilling. It is assumed that the long-term groundwater is near or below the bedrock interface at depths of 18 to 20.8 feet (El. 597.0 to 591.9 feet). Water level readings were made in the boreholes at times and under conditions shown on the boring logs and stated in the text of this report. Long term observations in cased borings or piezometers would be necessary to more accurately evaluate the long-term groundwater conditions at the site. However, it should be noted that fluctuations in groundwater level may occur due to variations in rainfall, other climatic conditions, or other factors not evident at the time measurements were made and reported herein.

GSG determined the geotechnical parameters to be used for the project design based on the results of field and laboratory test data on individual boring logs as well as our experience. Unit weights, friction angles and shear strength parameters were estimated using standard penetration test (SPT) results for the cohesionless soils and in-situ and laboratory test results for cohesive soils. The SPT values were corrected for hammer efficiency and overburden pressure. Based on the field investigation data collected, generalized soil parameters for the soils for use in design are presented in **Tables 2a and 2b – Attachment 3**.



### A. Surcharge Load

Traffic and other surcharge loads should be included in the retaining design as necessary. A live load surcharge shall be applied where vehicular load is expected to act on the surface of the backfill within a distance equal to one-half the wall height behind the back face of the wall in accordance with AASHTO 3.11.6.4. The live load surcharge may be estimated as a uniform horizontal earth pressure due to an equivalent height ( $H_{eq}$ ) of soil. **Table 3** provides the equivalent heights of soils for vehicular loadings on retaining walls.

**Table 3 - Equivalent Height of Soil for Vehicular Loading on Retaining Walls Parallel to Traffic**

Retaining Wall Height (ft)	H <sub>eq</sub> Distance from Wall Back face to Edge of Traffic	
	0 feet	1.0 feet or Further
5	5.0 feet	2.0 feet
10	3.5 feet	2.0 feet
≥20	2.0 feet	2.0 feet

Reference: AASHTO LRFD Table 3.11.6.4-2

### B. Drainage Recommendations

GSG does not anticipate significant groundwater related issues during construction activity; however, water may become perched in the fill soils or within confined granular layers. If rainwater run-off or perched water is accumulated at the base of excavation, the contractor should remove accumulated water using conventional sump pit and pump procedures and maintain a dry and stable excavation. The location of the sump should be determined by the contractor based on field conditions. During earthmoving activities at the site, grading should be performed to ensure that drainage is maintained throughout the construction period. Water should not be allowed to accumulate in the foundation area either during or after construction. Undercut and excavated areas should be sloped toward one corner to facilitate removal of any collected rainwater or surface run-off. Grades should be sloped away from the excavations to minimize runoff from entering.

### C. Construction Requirements

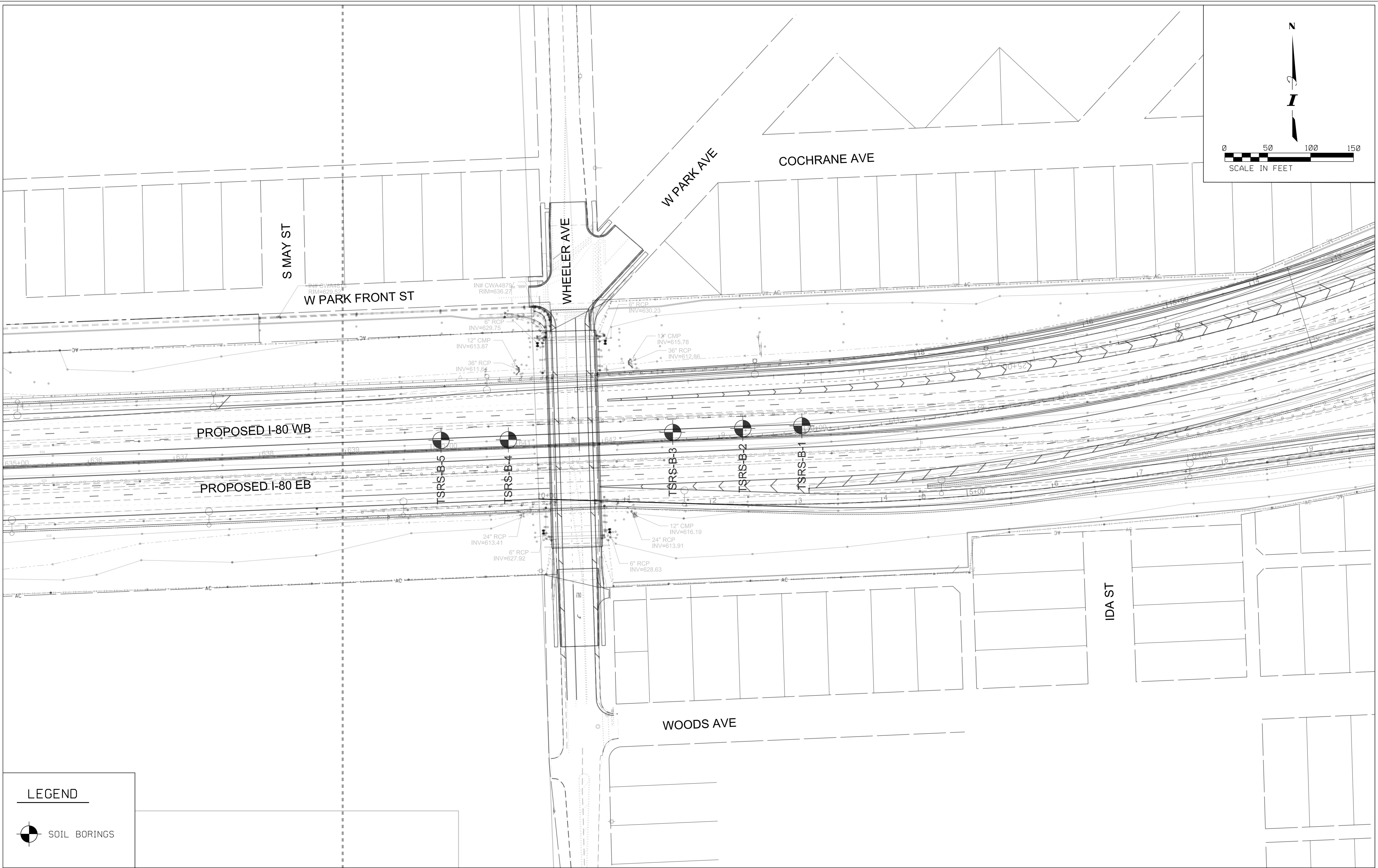
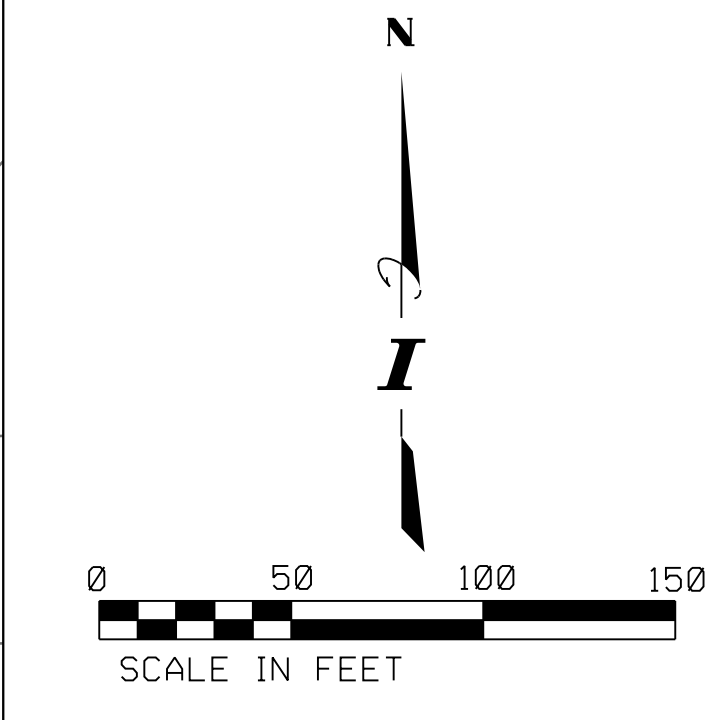
The temporary soil retention system should be designed in accordance with the IDOT Bridge Design Manual, Section 3.13.1, *Temporary Sheet Piling Design and Temporary Soil Retention Systems* and the IDOT Design Guide, Section 3.13.1, *Temporary Sheet Piling Design*. The design of the temporary soil retention system (TSRS) is the responsibility of the contractor. The contractor should submit the TSRS plans to the structural design team for review prior to commencing construction of the TSRS.



**Attachments:**

1. Soil Boring Location Plan
2. Soil Boring Logs
3. Tables 2a, 2b – Summary of Soil Parameters

**ATTACHMENT 1**  
**SOIL BORING LOCATION PLAN**



LEGEND



FILE NAME = \$FILEL\$  
PEN TABLE = \$PENTBL\$  
PLOT DATE = \$DATE\$  
SHEET SIZE = \$SHEETSIZE\$  
PLOT SCALE = \$SCALE\$  
USER NAME = \$USER\$



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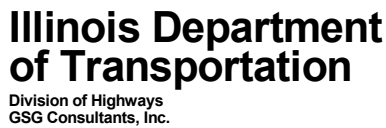
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PLOT SCALE	= \$SCALE\$	CHECKED	- DE
PLOT DATE	= \$DATE\$	DATE	- 08/19/2024

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

I-80 TSRS			
SOIL BORING LOCATION PLAN			
JOLIET, ILLINOIS			
SCALE: 1:50	SHEET 1	OF 1 SHEETS	STA. TO STA.

F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
		WILL	1	1
CONTRACT NO. PTB-198-003				
ILLINOIS FED. AID PROJECT				

**ATTACHMENT 2**  
**SOIL BORING LOGS**

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2 inches of Topsoil	616.16				Auger Refusal on Limestone Bedrock at 20.75 feet End of Boring			
Dark Brown, Moist		5						
FILL: SILTY CLAY, trace sand, trace gravel		5 5	1.5 P	18				
	613.33							
Very Stiff		4						
Brown and Gray, Moist		3	2.1	20				
SILTY CLAY, trace gravel (CL/ML)		4 -5	B				-25	
	610.83							
Stiff to Hard		3						
Gray, Moist		3 4	1.9 B	22				
SILTY CLAY, trace gravel (CL/ML)								
		3						
		3 5	2.1 B	15			-30	
		-10						
		4						
		4 7	4.0 B	19				
		3 4						
		8 -15	3.3 B	19		-35		
	600.83							
Medium Dense		5						
Gray, Moist		8		18				
SILT, trace gravel, trace sand (ML)		8						
	598.33							
Dense		3						
Brown, Dry		14		4				
SAND, medium to coarse grained, with gravel (SP)		31						
	596.33	-20				-40		





# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 7/31/24

ROUTE I-80 DESCRIPTION TSRS LOGGED BY DV

SECTION C-91-109-22 LOCATION SEC. 17, TWP. 35 N, RNG. 10 E,

COUNTY Will DRILLING RIG Diedrich D-70 ATV Latitude Longitude  
DRILLING METHOD HSA HAMMER TYPE Auto  
HAMMER EFF (%) 93

STRUCT. NO. Station	DEPTH H S	BLOW S Qu	UCS Qu	MOIST S T	Surface Water Elev. Stream Bed Elev.	N/A N/A	ft ft	DEPTH H S	BLOW S Qu	UCS Qu	MOIST S T
BORING NO. <u>TSRS-B-2</u> Station Offset	(ft)	(/6")	(tsf)	(%)	Groundwater Elev.: First Encounter Upon Completion After Hrs.	Dry N/A N/A	ft ft ft	(ft)	(/6")	(tsf)	(%)
Ground Surface Elev. <u>615.46</u> ft											
2 inches of Topsoil / 615.30					Brown and Gray						
Dark Brown, Moist		6			LIMESTONE, slightly weathered,						
FILL: SILTY CLAY LOAM, with		5		16	highly fractured, trace clay at 19.5,						
sand, trace gravel		6			22.5, and 26 feet, some vugs						
612.46					Run 1: 18.5' - 28.5'						
Stiff to Very Stiff					Recovery: 83.8%						
Gray, Moist		3			RQD: 6.7% (Very Poor)						
SILTY CLAY, trace gravel		3	1.9	22	(continued)						
(CL/ML)	-5	4	B					-25			
		4									
		4	2.7	14							
		4	B								
		3									
		5	2.8	17							
	-10	4	P		End of Boring		586.96				
		4									
		4	3.1	21							
		6	B								
		3									
		4	3.8	20							
	-15	6	B					-35			
599.96											
Very Dense		7									
Brown, Dry		23		4							
SAND, with gravel (SP)		32									
Auger Refusal on Limestone											
Bedrock at 18.5 feet		50/4									
596.96											
	-20							-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

I-80 TSRS  
Boring Number: TSRS-B-2  
Will County, IL



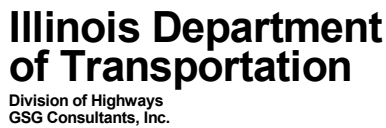
Boring No.	Run	Depth (ft)	Recovery (%)	RQD (%)	RQD Classification	Description
TSRS-B-2	1	18.5'-28.5'	83.8	6.7	Very Poor	Brown and Gray Limestone Slightly Weathered, Highly Fractured, Trace Clay at 19.5, 22.5, and 26 feet, Some Vugs

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Depth (ft)	Soil Description	Moisture (%)	Specific Gravity
0	Surface Soil		
1			
2			
3			
4			
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19	Bedrock		
20			
21			
22			
23			
24			
25			
26			
27			
28			
29			
30			
31			
32			
33			
34			
35			
36			
37			
38			
39			
40			

BBS, form 137 (Rev. 8-99)

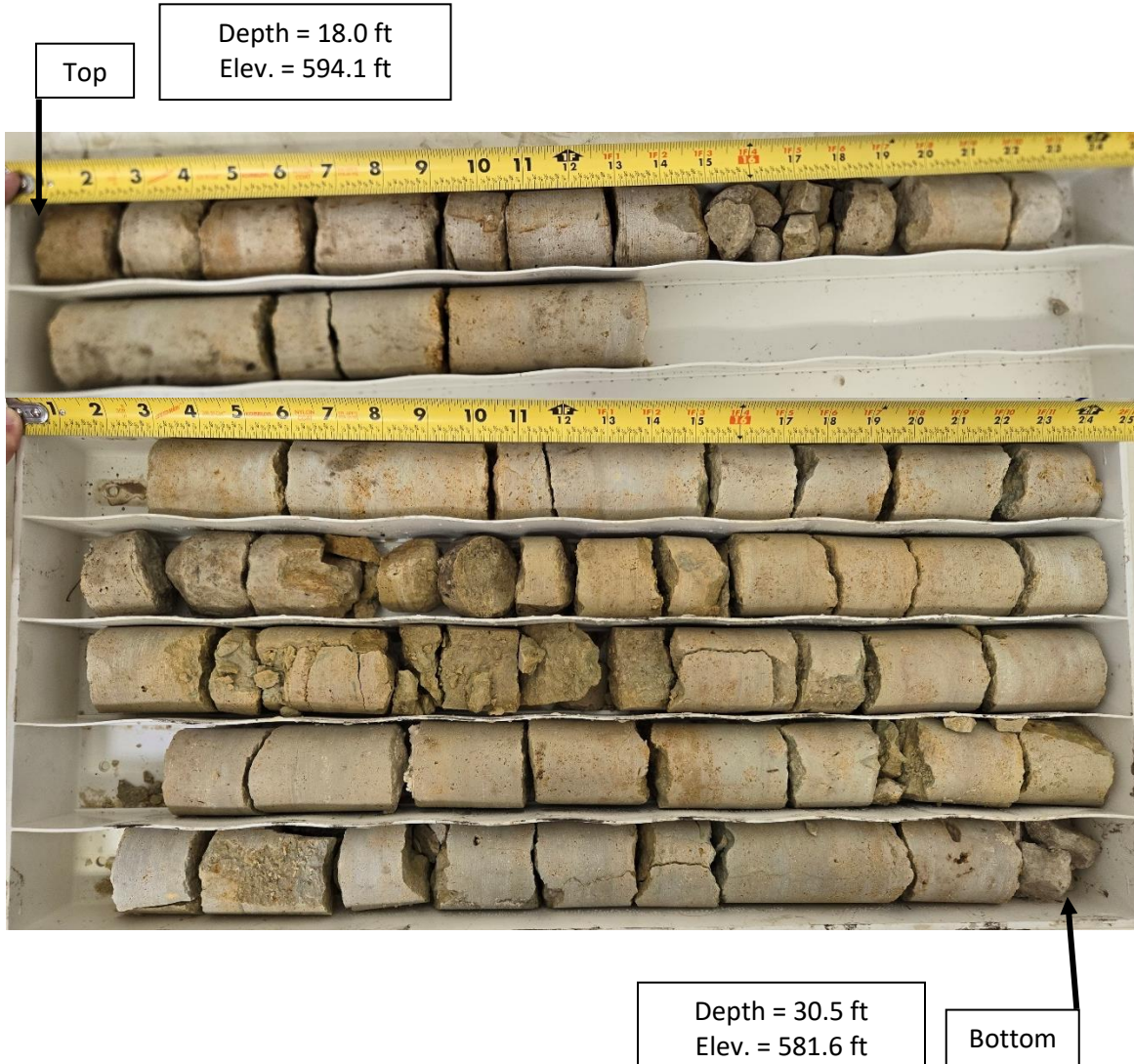
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**Date** 8/1/24

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BBS, form 137 (Rev. 8-99)

I-80 TSRS  
Boring Number: TSRS-B-4  
Will County, IL



Boring No.	Run	Depth (ft)	Recovery (%)	RQD (%)	RQD Classification	Description
TSRS-B-4	1	18.0'-30.5'	100	11.0	Very Poor	Brown and Gray Limestone Slightly to Moderately Weathered, Highly Fractured, Vertical Fractures at 24 and 30 feet, Trace Clay at 19.5 feet, Trace Vugs



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## SOIL BORING LOG

Page 1 of 1

Date 8/1/24

ROUTE I-80 DESCRIPTION  TSRS  LOGGED BY DV

SECTION C-91-109-22 LOCATION SEC. 17, TWP. 35 N, RNG. 10 E,

COUNTY Will DRILLING RIG Diedrich D-70 ATV Latitude  Longitude   
DRILLING METHOD HSA HAMMER TYPE Auto HAMMER EFF (%) 93

STRUCT. NO.   
Station

BORING NO. TSRS-B-5

Station

Offset

Ground Surface Elev. 611.92 ft

D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)
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Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	Dry	ft
Upon Completion	N/A	ft
After <u>    </u> Hrs.	N/A	ft

D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)
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2 inches of Topsoil	611.75				Auger Refusal on Limestone				
Stiff to Very Stiff					Bedrock at 20 feet				
Gray, Moist		4			End of Boring				
SILTY CLAY, trace gravel		4	2.3	18					
(CL/ML)		4	B						
		3							
		3	1.5	19					
	-5	5	B			-25			
		3							
		4	2.3	21					
		5	B						
		2							
		4	2.1	19					
	-10	7	B			-30			
	601.42								
Medium Dense									
Gray, Moist		4							
SILT, with clay, trace gravel, trace		8		20					
sand (ML)		7							
	598.42								
Very Dense to Extremely Dense		4							
Brown, Moist to Wet		22		18					
SAND, with gravel (SP)		34				-35			
	-15								
		25							
		50/3		5					
	593.92								
Stiff		19							
Brown and Gray, Moist		16	1.8	15					
SILTY CLAY, with sand, little		50/3	P						
gravel (CL/ML)									
	591.92	-20				-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

**ATTACHMENT 3**  
**SUMMARY OF SOIL PARAMETERS**

Table 2a: Summary of Soil Parameters – TSRS East (TSRS-B-1 through TSRS-B-3)

Depth ft (Elevation)	Soil Description	In situ Unit Weight $\gamma$ (pcf)	Undrained		Drained		Lateral Earth Pressure Long-term/Drained			Parameters for p-y Curve Method		
			Cohesion $c$ (psf)	Friction Angle $\phi$ (°)	Cohesion $c$ (psf)	Friction Angle $\phi$ (°)	Active Earth Pressure Coefficient ( $K_a$ )	Passive Earth Pressure Coefficient ( $K_p$ )	At Rest Earth Pressure Coefficient ( $K_o$ )	p-y Curve Type in LPile	Coefficient of Lateral Subgrade Modulus* (kpy, pci)	Horizontal Strain Factor ( $\epsilon_{50}$ )
0-2.5 (615.5-613)	Fill Dark Brown Silty Clay	136	1,600	0	160	25	0.41	2.46	0.58	Stiff Clay w/o Free Water	500	0.007
2.5-16.5 (613-599)	Brown and Gray to Gray Stiff to Hard Silty Clay	135	3,000	0	300	28	0.36	2.77	0.53	Stiff Clay w/o Free Water	1,000	0.005
16.5-19 (599-596.5)	Brown Dense to Very Dense Sand	142	0	42	0	42	0.20	5.04	0.33	Sand (Reese)	125	N/A
14.5-17 (601-598.5) <b>TSRS-B-1 only</b>	Gray Medium Dense Silt	128	0	34	0	34	0.28	3.53	0.44	Silt	90	N/A

\*The initial p-y modulus,  $E_{py}$ , varies linearly with depth. To obtain  $E_{py}$  use the equation  $E_{py} = k_{py} * z$ , where  $k_{py}$  is the subgrade modulus given in the table and  $z$  is the distance from the surface to the center point of the layer in inches.



Table 2b: Summary of Soil Parameters – TSRS West (TSRS-B-4, TSRS-B-5)

Depth ft (Elevation)	Soil Description	In situ Unit Weight $\gamma$ (pcf)	Undrained		Drained		Lateral Earth Pressure Long-term/Drained			Parameters for p-y Curve Method		
			Cohesion $c$ (psf)	Friction Angle $\phi$ (°)	Cohesion $c$ (psf)	Friction Angle $\phi$ (°)	Active Earth Pressure Coefficient ( $K_a$ )	Passive Earth Pressure Coefficient ( $K_p$ )	At Rest Earth Pressure Coefficient ( $K_o$ )	p-y Curve Type in LPile	Coefficient of Lateral Subgrade Modulus* (kpy, pci)	Horizontal Strain Factor ( $\epsilon_{50}$ )
0-11 (612-601)	Gray Stiff to Very Stiff Silty Clay	132	2,400	0	240	28	0.36	2.77	0.53	Stiff Clay w/o Free Water	1,000	0.005
11-13 (601-599)	Gray Medium Dense Silt	129	0	34	0	34	0.28	3.53	0.44	Silt	90	N/A
13-18 (599-594)	Brown Dense to Extremely Dense Sand	143	0	45	0	45	0.17	5.82	0.29	Sand (Reese)	225	N/A
0-3 (612-609) TSRS-B-4 only	Fill Dark Brown Silty Clay	130	1,000	0	100	25	0.41	2.46	0.58	Stiff Clay w/o Free Water	500	0.007
18-20 (594-592) TSRS-B-5 only	Brown and Gray Stiff Silty Clay	137	1,800	0	180	28	0.36	2.77	0.53	Stiff Clay w/o Free Water	500	0.007